



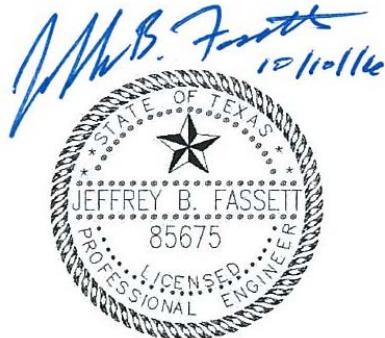
REPORT

SAFETY FACTOR ASSESSMENT REPORT

Oak Grove Steam Electric Station

Submitted To: Luminant
1601 Bryan Street
Dallas, TX 75201

Submitted By: Golder Associates Inc.
500 Century Plaza Drive, Suite 190
Houston, TX 77073 USA



Professional Engineering Firm
Registration Number F-2578

October 2016

Project No. 1648164





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LUMINANT



1.0 INTRODUCTION

1.1 Purpose

The “Disposal of Coal Combustion Residuals (CCR) from Electric Utilities rule” (40 Code of Federal Regulations (40 CFR) Part 257), effective October 19, 2015, requires that existing CCR surface impoundments meeting the requirements of §257.73(b) conduct safety factor assessments in accordance with §257.73(e). This letter provides the structural stability assessments and the safety factor assessments for the Oak Grove Steam Electric Station’s (OGSES’s) CCR Impoundments, identified as flue gas desulphurization (FGD) Ponds FGD-A, FGD-B, and FGD-C.

1.2 Site Background

The OGSES generates bottom ash, fly ash, boiler slag and flue gas desulfurization (FGD) sludge (gypsum) during electricity generation. The following surface impoundments, shown on Figure 1, are in operation at the OGSES:

- FGD-A Pond;
- FGD-B Pond; and
- FGD-C Pond.

1.3 Previous Slope Stability Evaluations

Golder performed previous evaluations on the FGD-A, and FGD-B ponds as part of the below reports submitted to Luminant:

- FGD-B Slope Stability Investigation Report (Revised), Luminant Oak Grove SES, Robertson County, Texas, dated June 2010
- FGD-A Slope Stability Evaluation Report, Luminant Oak Grove SES, Robertson County, Texas, dated March 2011
- Addendum To Slope Stability Investigation Reports Luminant Oak Grove SES, Robertson County, Texas, March 2014

These studies found the pond slopes to be adequately stable.

Construction of FGD-C Pond began on August 21, 2015. During the design of FGD-C Pond, Golder evaluated the stability of the embankments.

In this study, Golder has reviewed the previous analyses, modified the analyses where needed and added suitable cases to evaluate whether the ponds meet the required safety factors in §257.73(e)(1)(i)-(iv).



2.0 SUBSURFACE CONDITIONS

2.1 Regional Geology

The OGSES site is located in the Sandy Hills physiographic province of Texas. Ground elevations range from 400 to 425 feet MSL (mean sea level), and the topography is characterized by low rolling hills and shallow stream valleys (Espey, Huston & Associates, 1987). The regional terrain consists of a thick series of unconsolidated sediments consisting of sand, silt, clay, and lignite. The major geologic units are the tertiary age 'bedrock' strata and the quaternary age fluvial deposits. Eroded bedrock is overlain by alluvium and terraces along the valleys of larger streams. The approximate thickness of alluvium in the area of the site varies from 0 to 50 ft. The alluvium typically consists of sand, silt, silty clay and sandy clay and is not easily differentiated from the underlying bedrock strata in many instances.

2.2 Site Geology

2.2.1 Subsurface Investigations and Laboratory Testing

Information from previous subsurface investigations was used to characterize the subsurface site conditions. Golder conducted a subsurface investigation for the FGD-A pond in July 2008, prior to construction of the clay liner within the pond. Golder completed nine borings within the pond footprint with boring depths ranging from 16 to 28 feet below ground surface (bgs) (Golder, 2008). Golder also conducted a subsurface investigation for FGD-B pond in March 2010 (Golder, 2010). In December 2014, Golder completed another subsurface investigation including ten geotechnical boreholes and installation of 3 groundwater monitoring wells, to facilitate design and construction of the FGD-C pond. Appendix A includes the boring location maps and select, representative boring logs.

For each investigation, laboratory testing was performed on selected samples, in accordance with commonly accepted methods and practices. Undisturbed and disturbed soil samples were tested to determine water content, Atterberg limits, grain size distribution, and shear strength. Water content determination was performed in accordance with ASTM D2216; Atterberg limits were determined in accordance with ASTM D4318; and grain size distribution was performed in accordance with ASTM D422. Shear strength testing consisted of unconsolidated-undrained (UU) and consolidated-undrained (CU) triaxial compression tests in general accordance with ASTM D2850 and D4767, respectively. Laboratory test results are presented in Appendix B.

The findings from the above subsurface investigations were reviewed for their applicability to this study, and are summarized in the following sections.



2.2.2 Subsurface Site Conditions

2.2.2.1 FGD-A Pond

The soils encountered under the FGD-A Pond consist of lean clays, sandy clays, silty clays, sands, silty sands, clayey sands, and sandy silts. The near surface soils under the pond generally consist of fine-grained soils extending to depths ranging from approximately 6 feet to more than 19 feet below the pond bottom. Coarse-grained soils (i.e., sands) were generally encountered at depths greater than 6 feet below the pond bottom. Sands were encountered at shallower depths in the northwest portion of the pond than in the southeast portion of the pond.

Historical monitoring well measurements near the FGD-A Pond indicate that the groundwater level is between approximately 406 and 409 ft-msl.

2.2.2.2 FGD-B Pond

The soils encountered in the borings generally consisted of very stiff to hard clays and compact to very dense sands. The surficial soils were generally classified as very stiff to hard sandy (lean and fat) clay and ranged in thickness from 8 to 27 ft. The surficial clay stratum was underlain by layers of compact to very dense sand, clayey sand, silty sand, and/or very stiff to hard silty clay or clay.

Based on monitoring well measurements near FGD-B, the groundwater level ranges from approximately 405 to 410 ft-msl.

2.2.2.3 FGD-C Pond

Based on the results of the geotechnical investigations at this facility, soils in the footprint of the FGD-C Pond in general comprise the following:

- Laminated clays, silty clays and sandy clays having low horizontal and vertical hydraulic conductivity;
- Thinly bedded clays, clayey silts, and silty sands characterized by low to moderate horizontal permeability and low net vertical permeability; and
- Bedded sands, silty sands, clayey sands, and silts of moderate to relatively high horizontal and moderate vertical permeability.

Based on monitoring well measurements near FGD-C, the groundwater level ranges from approximately 410 ft-msl to 412 ft-msl.



3.0 STABILITY ANALYSIS - §257.73(e)

3.1 Safety Factor Assessment

According to the CCR rules, structural stability factors of safety need to be evaluated for the critical cross-section of each CCR facility under static and seismic loading for "Maximum Storage Pool" (2 feet of freeboard for this facility) and "Maximum Surcharge Pool" conditions. Liquefaction potential analysis is only necessary when soil sampling, construction documentation or anecdotal evidence from personnel with knowledge about the facility, indicates that soils of the embankment are susceptible to liquefaction.

Slope stability analyses were performed using a limit-equilibrium-based commercial computer program, Slide v7.0 by Rocscience. The analyses used a searching routine to identify the potential failure surface with minimum factor of safety for a given set of geometry, ground and groundwater conditions. The Spencer method of analysis was used in the analyses, while the Morgenstern-Price method was used for verification. The factors of safety of numerous potential failure surfaces were computed to establish minimum factors of safety. Circular failure surfaces were considered for all cases except for section B1-B1' (discussed later) that has a thin layer of silt, and hence, a block failure produces a lower factor of safety. Stability analyses were performed for "Maximum Storage Pool" (freeboard of 2 feet) and "Maximum Surcharge Pool" (no freeboard) conditions for both the interior and exterior slopes of the ponds. In addition, the interior slopes were analyzed while the pond is empty. For each case, respective slopes were analyzed for both static and seismic loading conditions.

3.2 Cross-Sections Analyzed

After considering multiple cross-sections a critical cross-section was identified for each pond and used for the stability analysis. The critical cross-section was determined considering the geometry of the slopes, soil profile, phreatic surface and loading conditions. More than one cross-section was used when required. For example, the critical section for the interior slopes of FGD-B is located to the east bordering pond FGD-A. However, since FGD-A adjoins FGD-B here, the critical section for exterior slopes of FGD-B are not located on this section. Hence, another section is analyzed on the west side of FGD-B to evaluate the exterior slopes. The critical cross-sections analyzed – A-A', B-B', B1-B1', C-C' – for each pond are shown in Figure 2.

3.3 Material Properties

Based on the previous subsurface investigations, appropriate material properties were selected for use in the stability analysis. Table 1, Table 2, Table 3, and Table 4 summarize the material properties used in the stability analysis.

Espey, Huston & Associates, 1987 present boreholes drilled on the embankment of FGD-A composed of structural fill. The borings on the embankment crest and the slopes show high pocket penetrometer values



of 4.5 tons/ft² or above, indicating considerably hard clays. Also, we reviewed the Atterberg limits on samples collected from fill at the FGD-C pond. Based on these, a conservative value of shear strength was assumed for the structural fill as shown in the below tables.

Table 1: Soil Properties for Section A-A'

Soil Material	Description	Moist Unit Weight (lb/ft ³)	Saturated Unit Weight (lb/ft ³)	Drained Soil Properties	
				Cohesion, c' (lb/ft ²)	Friction Angle, ϕ' (°)
I	Sandy Clay	127	132	270	26
II	Silty Clay/ Clay	127	132	0	26
III	Clayey Sand	127	132	0	32

Table 2: Soil Properties for Section B-B'

Soil Material	Description	Moist Unit Weight (lb/ft ³)	Saturated Unit Weight (lb/ft ³)	Drained Soil Properties	
				Cohesion, c' (lb/ft ²)	Friction Angle, ϕ' (°)
I	Clay/ Silty Clay/ Sandy Clay	127	132	270	26
II	Sandy Silt	127	132	0	26
III	Sand/ Silty Sand	127	132	0	36
	Structural Fill	127	132	270	26

**Table 3: Soil Properties for Section B1-B1'**

Soil Material	Description	Moist Unit Weight (lb/ft ³)	Saturated Unit Weight (lb/ft ³)	Drained Soil Properties	
				Cohesion, c' (lb/ft ²)	Friction Angle, φ' (°)
I	Clay/ Silty Clay/ Sandy Clay	127	132	270	26
II	Sand/ Silty Sand	127	132	0	36
	Structural Fill	127	132	270	26

Table 4: Soil Properties for Section C-C'

Soil Material	Description	Moist Unit Weight (lb/ft ³)	Saturated Unit Weight (lb/ft ³)	Drained Soil Properties	
				Cohesion, c' (lb/ft ²)	Friction Angle, φ' (°)
I	New Fill - compacted onsite low to moderate plasticity clay soils	125	n/a	200	26
II	Existing Fill - stiff to very stiff clays	125	n/a	150	24
III	Very stiff Silty Clay	127	132	270	26
IV	Very dense Silty Sand	120	130	n/a	34

3.4 Phreatic Surface

For the stability analysis, the location of the phreatic surface within the FGD-A Pond embankment was conservatively assumed to correspond to the water level in the pond and to the ground surface of the exterior slope of the embankment. The only exception to this is Case 5a and 5b for FGD-B, where the phreatic surface from the adjoining FGD-A embankment was assumed to slope at approximately 3H:1V.

FGD-B and FGD-C Ponds are both lined with a composite geomembrane/clay liner; therefore, no phreatic surface is expected to develop within the embankments. The groundwater level below the FGD-B Pond was conservatively assumed to be at 410 ft-msl. The groundwater level near the cross-section analyzed for FGD-C Pond was assumed to be at 410 ft-msl, which is representative of the eastern portion of the pond.



Note that the phreatic surface elevations were conservatively assumed for stability analysis purposes -- they do not represent the elevation of the uppermost aquifer.

3.5 Seismic Loading

Based on the "US Seismic Hazard 2014 Map" prepared by the United States Geologic Survey (USGS) and the "2008 Interactive Deaggregations" (USGS), the peak ground acceleration (PGA) for a 2% probability of exceedance in 50 years (return period of 2,475 years) is 0.06g for the site location (including amplification factors for site soil conditions). Hence, a horizontal seismic load coefficient of 0.06g was used in the pseudostatic analysis.

3.6 Liquefaction Potential

Soil liquefaction describes a phenomenon whereby a saturated or partially saturated soil substantially loses strength and stiffness in response to an applied stress, usually earthquake shaking or other sudden change in stress condition, causing it to behave like a liquid. The phenomenon is most often observed in saturated, loose (low density or uncompacted), sandy soils. The embankment soils of ponds FGD-A, FGD-B, and FGD-C are all composed of clayey materials with significant fines content. The immediate foundation materials are also composed of soils containing a significant portion of fines, and are as well considerable dense. The subsurface investigations performed at each of the ponds do not indicate any soils in the embankment or its foundation, which are susceptible to liquefaction. Hence, failure of the pond slopes due to liquefaction is considered unlikely for the CCR surface impoundments at the OGSES.

3.7 Stability Analysis Results

Slope stability analyses were performed for long-term conditions for each of the critical cross-sections considered under static and seismic loading conditions. Both interior and exterior slopes were analyzed for "Maximum Storage Pool" (2 feet of freeboard) and "Maximum Surcharge Pool" (no freeboard) conditions. The interior slopes were analyzed for the condition where the pond is empty. The results of the slope stability analyses cases are presented in Table 5, Table 6, and Table 7 for ponds FGD-A, FGD-B, and FGD-C, respectively. The corresponding analysis outputs can be found in Appendix C. The results indicate that the pond slopes are sufficiently stable under all considered loading scenarios.

Table 5: Slope Stability Analysis Results – FGD-A

Cross-Section	Case #	Slope Location	Pond Pool Level	Loading Condition	Req'd Safety Factor ⁽¹⁾	Calculated Safety Factor
A-A'	1a	Exterior	Storage	Static	1.50	1.89
	1b			Pseudostatic	1.00	1.61
	2a		Surcharge	Static	1.40	1.84
	2b			Pseudostatic	1.00	1.56



Cross-Section	Case #	Slope Location	Pond Pool Level	Loading Condition	Req'd Safety Factor ⁽¹⁾	Calculated Safety Factor
	3a	Interior	Storage	Static	1.50	4.72
	3b			Pseudostatic	1.00	3.58
	4a		Surcharge	Static	1.40	5.20
	4b			Pseudostatic	1.00	3.90
	5a		Empty	Static	1.50	2.15
	5b			Pseudostatic	1.00	1.77

Note: (1) Required safety factors per §257.73(e)(i)-(iii)

Table 6: Slope Stability Analysis Results – FGD-B

Cross-Section	Case #	Slope Location	Pond level	Loading Condition	Req'd Safety Factor ⁽¹⁾	Calculated Safety Factor
B-B'	1a	Exterior	Storage	Static	1.50	2.43
	1b			Pseudostatic	1.00	2.07
	2a		Surcharge	Static	1.40	2.43
	2b			Pseudostatic	1.00	2.07
B1-B1'	3a	Interior	Storage	Static	1.50	1.51
	3b			Pseudostatic	1.00	1.20
	4a		Surcharge	Static	1.40	1.55
	4b			Pseudostatic	1.00	1.25
	5a		Empty	Static	1.50	2.20
	5b			Pseudostatic	1.00	1.79

Note: (1) Required safety factors per §257.73(e)(i)-(iii)

Table 7: Slope Stability Analysis Results – FGD-C

Cross-Section	Case #	Slope Location	Pond Pool level	Loading Condition	Req'd Safety Factor ⁽¹⁾	Calculated Safety Factor
C-C'	1a	Exterior	Storage	Static	1.50	2.06
	1b			Pseudostatic	1.00	1.72
	2a		Surcharge	Static	1.40	2.06
	2b			Pseudostatic	1.00	1.72
	3a	Interior	Storage	Static	1.50	5.53
	3b			Pseudostatic	1.00	4.04
	4a		Surcharge	Static	1.40	6.19
	4b			Pseudostatic	1.00	4.44
	5a		Empty	Static	1.50	2.16
	5b			Pseudostatic	1.00	1.80

Note: (1) Required safety factors per §257.73(e)(i)-(iii)



4.0 CONCLUSION

Based on our review of the information provided by Luminant, on information prepared by Golder Associates Inc., and on our analyses, the calculated factors of safety through the critical cross sections in the surface impoundments exceed the values listed in §257.73(e)(1)(i)-(iv).

Golder appreciates the opportunity to assist Luminant with this project. If you have any questions, or require further assistance from Golder, please contact the undersigned at (281) 821-6868.

GOLDER ASSOCIATES INC.

A handwritten signature in black ink.

Varenya Kumar
Staff Engineer

VK-JBF

A handwritten signature in blue ink.

Jeffrey B. Fassett, PE
Associate Geotechnical Engineer



5.0 CERTIFICATION

I hereby certify that this report has been prepared in general accordance with normally accepted civil engineering practices and in accordance with the requirements of 40 CFR §257.73(e).



Jeffrey B. Fassett, PE
Golder Associates Inc.
Firm Registration Number F-2578

LUMINANT



6.0 REFERENCES

Espey, Huston & Associates, Inc., 1987, Hydrogeologic Assessment of Proposed Surface Impoundment Areas, Twin Oak SES, Robertson County, Texas.

Golder Associates Inc. 2008, Data Report - Oak Grove SES, FGD Pond Subsurface Investigation, Robertson County, Texas.

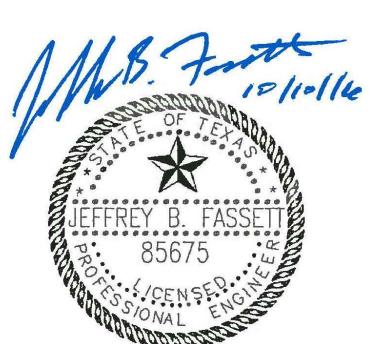
Golder Associates Inc. 2010, FGD-B Slope Stability Investigation Report (Revised), Luminant Oak Grove SES, Robertson County, Texas.

Golder Associates Inc. 2011, FGD-A Slope Stability Evaluation Report, Luminant Oak Grove SES, Robertson County, Texas.

Golder Associates Inc. 2014, Addendum to Slope Stability Investigation Reports, Luminant Oak Grove SES, Robertson County, Texas.



REFERENCE(S)
AERIAL PHOTO SOURCED FROM GOOGLE EARTH PRO DATED 2016



Professional Engineering Firm
Registration Number F-2578

0 400 800
1" = 800' FEET

CLIENT
LUMINANT POWER
OAK GROVE



CONSULTANT	YYYY-MM-DD	2016-09-29
DESIGNED	VK	
PREPARED	TNB	
REVIEWED	MX	
APPROVED	JBF	

PROJECT
2016 COAL COMBUSTION RESIDUALS
ENGINEERING SERVICES

TITLE
GENERAL SITE MAP

PROJECT NO.
1648164

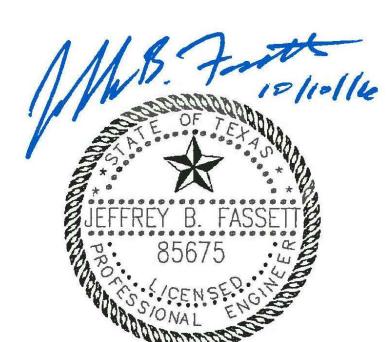
REV.
A



LEGEND

- - - FGD POND GRADE BREAK LINES
- FGD POND MAJOR CONTOUR
- FGD POND MINOR CONTOUR

REFERENCE(S)
AERIAL PHOTO SOURCED FROM GOOGLE EARTH PRO DATED 2016



Professional Engineering Firm
Registration Number F-2578

0 150 300
1" = 300' FEET

CLIENT
LUMINANT POWER
OAK GROVE

CONSULTANT



YYYY-MM-DD	2016-09-29
DESIGNED	VK
PREPARED	TNB
REVIEWED	MX
APPROVED	JBF

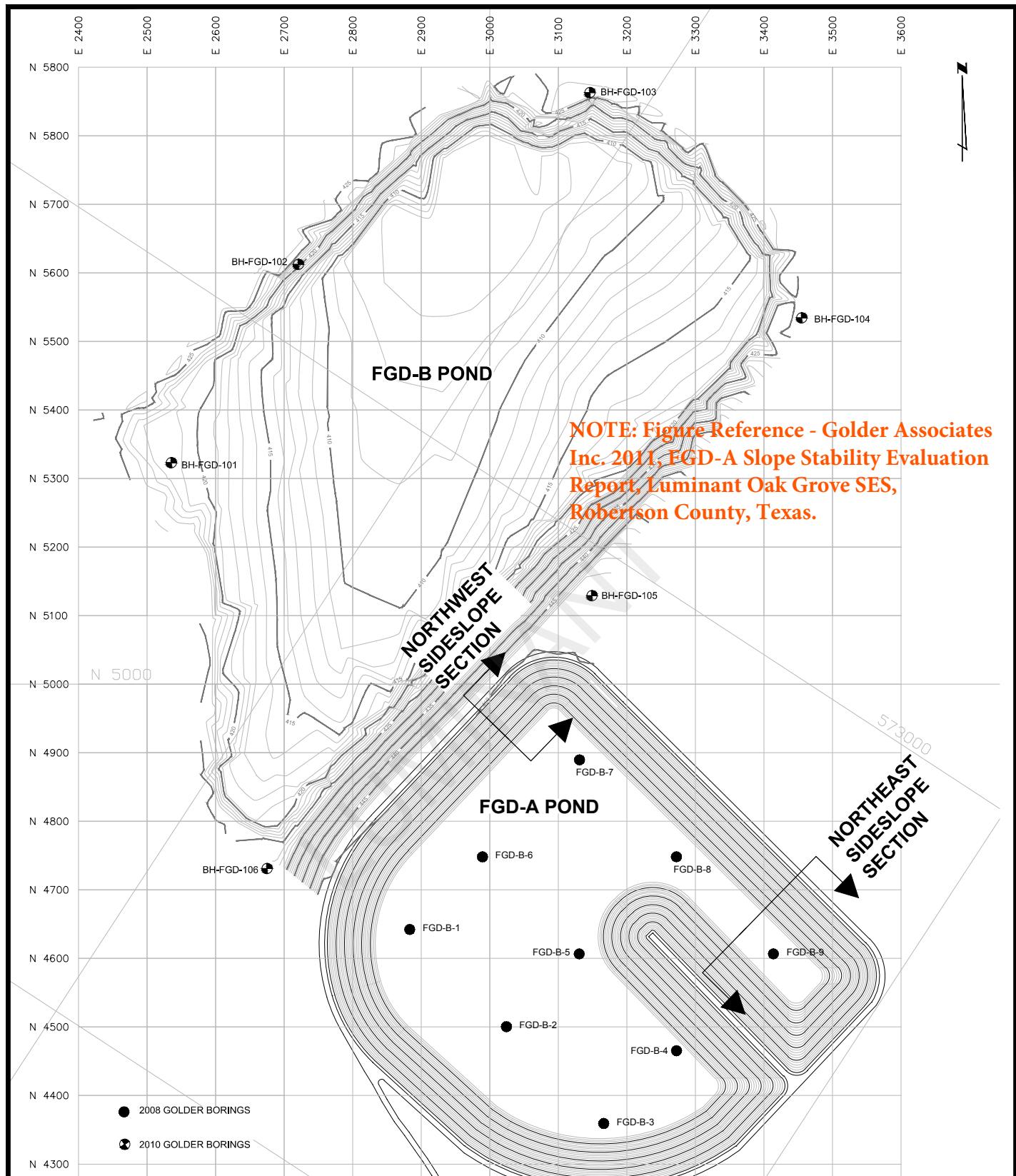
PROJECT
2016 COAL COMBUSTION RESIDUALS
ENGINEERING SERVICES

TITLE
CROSS-SECTIONS FOR SLOPE STABILITY ANALYSIS

PROJECT NO.
1648164

REV.
A

APPENDIX A
BORING LOCATION MAPS & BORING LOGS



TITLE

EXISTING BORING LOCATION PLAN

PROJECT

**FGD-A-POND SLOPE STABILITY ANALYSIS
LUMINANT OAK GROVE SES
ROBERTSON COUNTY, TEXAS**

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DATE
MARCH 2011

FIGURE NUMBER

CHECKED

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SCALE
AS SHOWN

REVIEWED

PCM

JOB NO.
113-94790

FILE NO.

DWG NO.

11394790A003

3

RECORD OF BOREHOLE FGD-B-7

SHEET 1 OF 2
DATUM: LOCAL

PROJECT: OAK GROVE SES
LOCATION: FRANKLIN, TEXAS

BORING STARTED: 17-Jul-2008
BORING FINISHED: 17-Jul-2008

DRILLING EQUIPMENT: MOBILE B-57 BUGGY
DRILLING OPERATOR: Lewis Environmental Drilling

NORTHING (ft): 4889.56
EASTING (ft): 3130.96
ELEVATION (ft): 422.24

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES	UNDRAINED SHEAR STRENGTH Cu	ROCK QUALITY DESIGNATION (RQD) %	WATER CONTENT PERCENT	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS	
		DESCRIPTION	STRATA PLOT							
				ELEV. DEPTH (ft)	NUMBER	TYPE	BLOWS/0.5 FT	PL	W	LL
0		GROUND SURFACE Stiff to very stiff, reddish brown, sandy CLAY, damp	422.2 0.0		4 7 8 N15	SB				
2		dark brown at 1.5'		2.0		SH				
4		Very stiff, reddish brown and yellowish brown, CLAY, trace sand, damp								
6		Dense, reddish brown to brown, SAND, with clay, damp	6.0		7 10 13 N23	SB				
8	Hollow Stem Auger	light brown, sandy clay layer at 8.0' reddish brown at 8.5'			12 22 24 N46	SB				
10		dense to very dense at 10.0'			12 17 21 N38	SB				
12		light brown at 12.0'			11 14 17 N31	SB				
14		clayey at 14'			17 30 28 N58	SB				
16		moist at 16.0'			17 17 22 N39	SB				
18					10 14 18 N32	SB				
20		light gray at 19.0'			12 24 26 N50	SB				

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RECORD OF BOREHOLE FGD-B-7

SHEET 2 OF 2
DATUM: LOCAL

PROJECT: OAK GROVE SES
LOCATION: FRANKLIN, TEXAS

BORING STARTED: 17-Jul-2008
BORING FINISHED: 17-Jul-2008

DRILLING EQUIPMENT: MOBILE B-57 BUGGY
DRILLING OPERATOR: Lewis Environmental Drilling

NORTHING (ft): 4889.56
EASTING (ft): 3130.96
ELEVATION (ft): 422.24

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE			SAMPLES	UNDRAINED SHEAR STRENGTH Cu CU - ● P.P. - ◊ Field Vane Shear ■ UU - □ TORV - ▲ UCS - *400 800 1200 1600	ROCK QUALITY DESIGNATION (RQD) % ★ 20 40 60 80	WATER CONTENT PERCENT PL ━ GW ━ LL 20 40 60 80	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION		STRATA PLOT						
		ELEV. DEPTH (ft)	NUMBER	TYPE						
<i>— CONTINUED FROM PREVIOUS PAGE —</i>										
20	Hollow Stem Auger		20.0							
22			22.0		11	SB	12 24 24 N48			
TOTAL DEPTH AT 22.0'										
24										
26										
28										
30										
32										
34										
36										
38										
40										

RECORD OF BOREHOLE FGD-B-8

SHEET 1 OF 2
DATUM: LOCAL

PROJECT: OAK GROVE SES
LOCATION: FRANKLIN, TEXAS

BORING STARTED: 17-Jul-2008
BORING FINISHED: 17-Jul-2008

DRILLING EQUIPMENT: MOBILE B-57 BUGGY
DRILLING OPERATOR: Lewis Environmental Drilling

NORTHING (ft): 4748.26
EASTING (ft): 3272.19
ELEVATION (ft): 426.97

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES	UNDRAINED SHEAR STRENGTH				ROCK QUALITY DESIGNATION				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS	
		DESCRIPTION	STRATA PLOT		ELEV. DEPTH (ft)	NUMBER	TYPE	BLOWS/0.5 FT	Cu	20	40	60	80		
0		GROUND SURFACE Stiff to very stiff, reddish brown, CLAY, with sand, damp	427.0 0.0						CU - ● P.P. - ⊕ Field Vane Shear ■	20	40	60	80		
2		silty at 1.5'							UU - ◊ TORV. - ▲ UCS - *	400	800	1200	1600		
4															
6		Stiff to very stiff, light brown and yellowish brown, silty CLAY, trace sand, damp	6.0												
8		very stiff, brown with mottled yellowish brown at 8'													
10	Hollow Stem Auger	reddish brown at 10.0'													
12															
14		dark brown at 14.5'													
16															
18															
20		Hard, reddish brown, sandy CLAY, damp	19.0		10 9 8 7 6 5 4	SB SB SH SB SB SB	SB SH SB SB SB SB	3 4 5 N10	8 17 19 N36	20	40	60	80		

- CONTINUED NEXT PAGE -

RECORD OF BOREHOLE FGD-B-8

SHEET 2 OF 2

DATUM: LOCAL

PROJECT: OAK GROVE SES
LOCATION: FRANKLIN, TEXAS

BORING STARTED: 17-Jul-2008
BORING FINISHED: 17-Jul-2008

DRILLING EQUIPMENT: MOBILE B-57 BUGGY
DRILLING OPERATOR: Lewis Environmental Drilling

NORTHING (ft): 4748.26
EASTING (ft): 3272.19
ELEVATION (ft): 426.97

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES	UNDRAINED SHEAR STRENGTH Cu CU - ● P.P. - ○ Field Vane Shear ■ UU - □ TORV. ▲ UCS - *	ROCK QUALITY DESIGNATION (RQD) % ★ 20 40 60 80	WATER CONTENT PERCENT PL ━━ W ━━ LL 20 40 60 80	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT						
<i>-- CONTINUED FROM PREVIOUS PAGE --</i>									
20		Compact to dense, brown, clayey SAND, moist		20.0					
22	Hollow Stem Auger	light brown at 21.5'			7 17 24 N41				sieve
24					4 7 10 N17				
26		Firm, gray, CLAY		25.5			O		
		TOTAL DEPTH 26'		26.0	14 19 24 N43				
28									
30									
32									
34									
36									
38									
40									

RECORD OF BOREHOLE FGD-B-9

SHEET 1 OF 2
DATUM: LOCAL

PROJECT: OAK GROVE SES
LOCATION: FRANKLIN, TEXAS

BORING STARTED: 17-Jul-2008
BORING FINISHED: 17-Jul-2008

DRILLING EQUIPMENT: MOBILE B-57 BUGGY
DRILLING OPERATOR: Lewis Environmental Drilling

NORTHING (ft): 4606.63
EASTING (ft): 3413.66
ELEVATION (ft): 427.99

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES	UNDRAINED SHEAR STRENGTH Cu				ROCK QUALITY DESIGNATION (RQD) % ★				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS			
		DESCRIPTION	STRATA PLOT		ELEV. DEPTH (ft)	NUMBER	TYPE	BLOWS/0.5 FT	400	800	1200	1600	20	40	60	80	
0		GROUND SURFACE Firm to stiff, yellowish brown and brown, CLAY, with sand, damp			428.0 0.0	-											
2		mottled reddish brown and light gray at 3.0'															
4		Stiff to very stiff, brown with occasional yellow brown seams, silty CLAY, damp			4.0												
8																	
8																	
10	Hollow Stem Auger	dark brown with occasional streaks of reddish brown at 10.0'															
12																	
14																	
16		Hard, light gray with occasional yellowish brown and brown, CLAY, trace sand, moist			16.0	8	7	6	5	4	3	2	1				
18						SB	SB	SH	SB	SB	SB	SB	SB				
20						10	9										

— CONTINUED NEXT PAGE —

RECORD OF BOREHOLE FGD-B-9

SHEET 2 OF 2
DATUM: LOCAL

PROJECT: OAK GROVE SES
LOCATION: FRANKLIN, TEXAS

BORING STARTED: 17-Jul-2008
BORING FINISHED: 17-Jul-2008

DRILLING EQUIPMENT: MOBILE B-57 BUGGY
DRILLING OPERATOR: Lewis Environmental Drilling

NORTHING (ft): 4606.63
EASTING (ft): 3413.66
ELEVATION (ft): 427.99

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE			SAMPLES	UNDRAINED SHEAR STRENGTH Cu CU - ● P.P. - Ⓛ Field Vane Shear ■ UU - Ⓛ TORV. ▲ UCS - *	ROCK QUALITY DESIGNATION (RQD) % ★ 20 40 60 80	WATER CONTENT PERCENT PL ── GW ── LL 20 40 60 80	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE	BLOWS/0.5 FT			
<i>— CONTINUED FROM PREVIOUS PAGE —</i>										
20		Hard, dark brown with occasional reddish brown, sandy CLAY, moist		20.0						
22	Hollow Stem Auger	gray with occasional reddish brown at 23'			12	SB	5 18 28 N46			
24		TOTAL DEPTH 24.0'		24.0			18 29 33 N62			
26										
28										
30										
32										
34										
36										
38										
40										

RECORD OF BOREHOLE BH-FGD-105

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

SHEET 1 OF 2
DATUM: GEODETIC
NORTHING (ft): 5129
EASTING (ft): 3149
ELEVATION (ft): 449

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE			SAMPLES	RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)	WATER CONTENT PERCENT	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE	BLOWS/0.5 FT	PL	W	LL
0		Grass		449.0						
		Very stiff, mottled dark brown, sandy fat CLAY (CH), trace organics, damp			44	SH		37		
		hard, light brown at 2.0'			45	SH		33		
		dark brown at 4.0'			46	SH		30		
		light brown at 6.0'			47	SH		50		
		mottled, trace lignite at 13.0'			48	SH		67		
		very stiff, dark gray at 18.0'			49	SH		30		
		hard, dark brown at 23.0'			50	SH		37		
		Very stiff, mottled dark gray to brown, silty CLAY (CL-ML), few sand, moist		28.0	51	SH		37		
		— CONTINUED NEXT PAGE —			52	SH		50		

RECORD OF BOREHOLE BH-FGD-105

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5129
EASTING (ft): 3149
ELEVATION (ft): 449

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			UNDRAINED SHEAR STRENGTH Cu (psf)	RECOVERY %	WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE			BLOWS/0.5 FT	PL	W	LL		
-- CONTINUED FROM PREVIOUS PAGE --														
30				30.0										
				33.0										
				33.8	53	SH		50						
35		Stiff, black, sandy SILT (ML), trace clay, some organics, some wood fragments, moist Stiff, dark brown, fat CLAY (CH), trace organics, trace sand, moist												
				38.0	54	SS	50/6° N>50	56						
40		Very dense, light brown, fine, poorly-graded SAND (SP), trace clay, damp												
				43.0	55	SS	24 34 38 N72	67						
45		Very dense, light brown, fine, poorly-graded SAND (SP-SM), with silt, moist												
				48.0	56	SS	22 26 50/5° N>50	83						
50		Very dense, grayish brown, silty SAND (SM), trace clay, moist BORING TERMINATED AT 50.0'		50.0										
55														
60														

RECORD OF BOREHOLE BH-FGD-101

SHEET 1 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 25-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5323
EASTING (ft): 2535
ELEVATION (ft): 421

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)				WATER CONTENT PERCENT	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS			
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		BLOWS/0.5 FT	CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000			
0		Cleared ground Very stiff, mottled, sandy lean CLAY (CL), damp		421.0											○		
		hard, mottled reddish brown at 2.0'			88	SH									○		
		trace silt at 4.0'			89	SH									○		
5		very stiff, reddish brown and light gray, some silt at 6.0'			90	SH									○		
		Dense, grayish brown, SAND (SP-SM), with silt, damp		8.0	91	SH									○		
10					92	SH									○		
		Very stiff, grayish brown, clayey fine SAND (SC), with some silt, layered gray and light brown at 13.5'		13.0	93	SH									○		
15					94	SS									○		
		Very dense, light brown, fine, poorly-graded SAND (SP), damp		18.0	95	SS									○		
20					96	SS									○		
		little clay at 23.0'													○		
25															○		
		dense, wet at 28.0'													○		
30		BORING TERMINATED AT 30.0'															
		--- CONTINUED NEXT PAGE ---															

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/27/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

27 03/24/2010

RECORD OF BOREHOLE BH-FGD-101

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 25-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5323
EASTING (ft): 2535
ELEVATION (ft): 421

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)					WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL		
30	---	--- CONTINUED FROM PREVIOUS PAGE ---		30.0														
35																		
40																		
45																		
50																		
55																		
60																		

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/27/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-102

SHEET 1 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5612
EASTING (ft): 2721
ELEVATION (ft): 421

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)				WATER CONTENT PERCENT	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■ UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000			
0		Grass		421.0											
		Hard, mottled light brown, sandy lean CLAY (CL), damp			79	SH									
		very stiff, brown at 2.0'			80	SH									
5		hard at 4.0'			81	SH									
		light gray, moist at 6.0'			82	SH									
		very stiff at 8.0'			83	SH									
10		little silt at 13.0'			84	SH									
		Stiff, light to dark gray, silty fat CLAY (CH), trace sand, moist		18.0	85	SH									
20		Stiff, gray, sandy lean CLAY (CL), trace silt, moist		23.0	86	SH									
25		Very dense, light brown, fine, poorly-graded SAND (SP-SM), with clay, wet BORING TERMINATED AT 30.0'		28.0	87	SS N72	2 7 34 38								
30		-- CONTINUED NEXT PAGE --													

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-102

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5612
EASTING (ft): 2721
ELEVATION (ft): 421

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)					WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL		
30	---	--- CONTINUED FROM PREVIOUS PAGE ---		30.0														
35																		
40																		
45																		
50																		
55																		
60																		

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-103

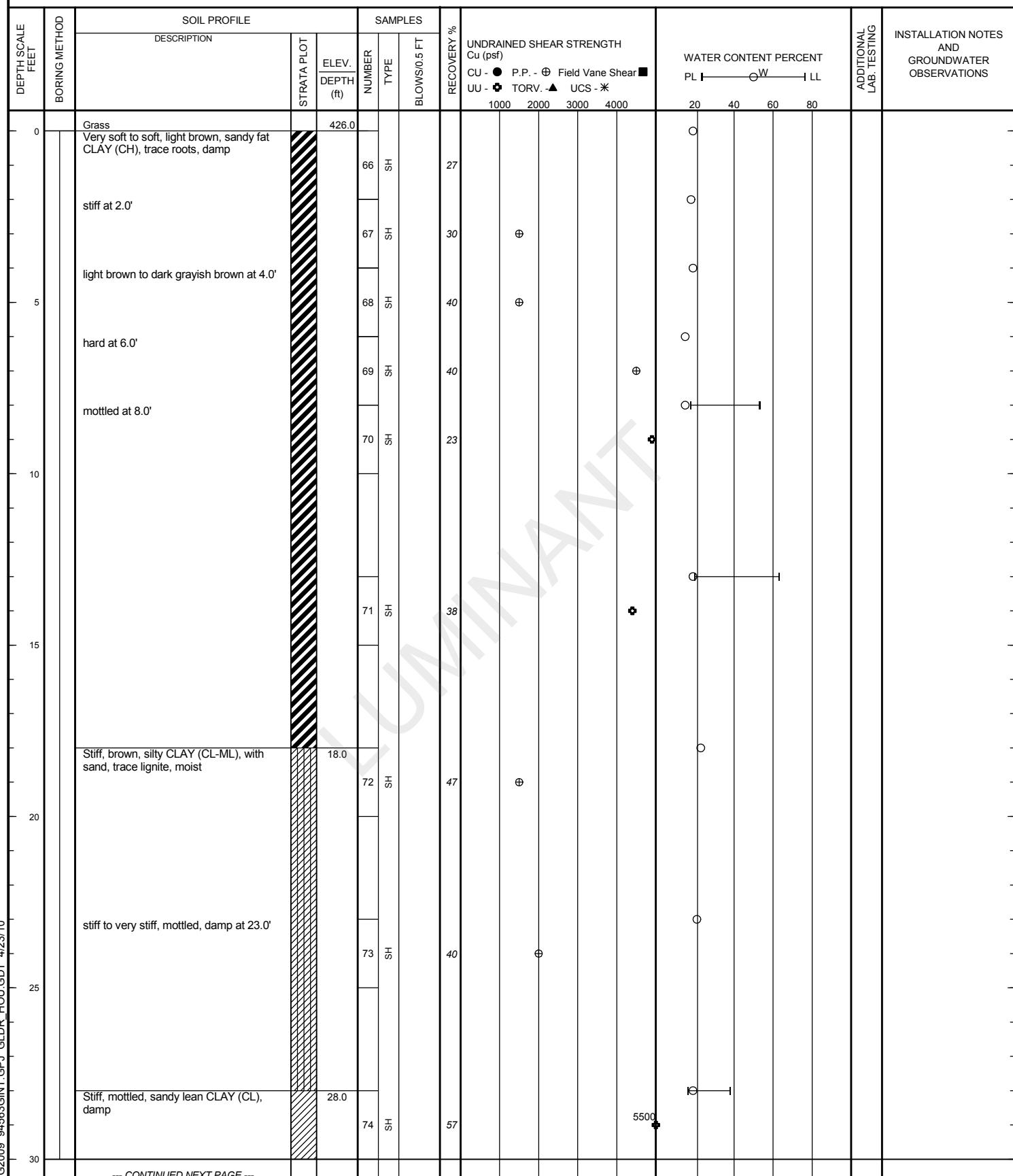
SHEET 1 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5863
EASTING (ft): 3146
ELEVATION (ft): 426



HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-103

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5863
EASTING (ft): 3146
ELEVATION (ft): 426

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)				WATER CONTENT PERCENT PL W LL	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■ UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000			
30		--- CONTINUED FROM PREVIOUS PAGE ---		30.0											
33		Compact, light gray, SILT (ML), with sand, wet		33.0											
33.7		Firm, light gray and brown, silty SAND (SM), wet		33.7	75	SH									
38.0		Very stiff, mottled light gray, lean CLAY (CL), trace lignite, trace sand, wet		38.0	76	SH									
43.0'		hard at 43.0'			77	SH									
48.0'		interbedded with sand layers at 48.0'			78	SH									
50.0		BORING TERMINATED AT 50.0'		50.0											

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

32° 03/24/2010

RECORD OF BOREHOLE BH-FGD-104

SHEET 1 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5534
EASTING (ft): 3455
ELEVATION (ft): 425

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)				WATER CONTENT PERCENT	ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS			
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL	
0		Grass		425.0													
		Very stiff, light brown to dark brown, sandy lean CLAY (CL), damp			57	SH											
		hard, light brown at 2.0'			58	SH											
5		mottled to dark brown, trace silt at 4.0'			59	SH											
		grayish brown at 6.0'			60	SH											
		very stiff, moist at 13.0'			61	SH											
10					62	SH											
15		hard, damp at 18.0'		18.5	63	SH											
		Very dense, grayish brown, medium to fine, silty clayey SAND (SC/SM), trace organic			64	SS											
20					65	SS											
		Compact, light brown and gray, poorly-graded SAND (SP-SM), with silt, wet		23.0	5 9 14 N23	67											▼
25					66												
		Dense, fine, silty SAND (SM), trace clay		28.0	11 12 19 N31	67											22' 03/24/2010
30		---															

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/27/10

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LOGGED: DM

CHECKED: PCM

DEPTH SCALE
1 inch to 3.8 feet

RECORD OF BOREHOLE BH-FGD-104

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5534
EASTING (ft): 3455
ELEVATION (ft): 425

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)					WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL		
30		-- CONTINUED FROM PREVIOUS PAGE --		30.0														
		BORING TERMINATED AT 30.0'																
35																		
40																		
45																		
50																		
55																		
60																		

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/27/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-105

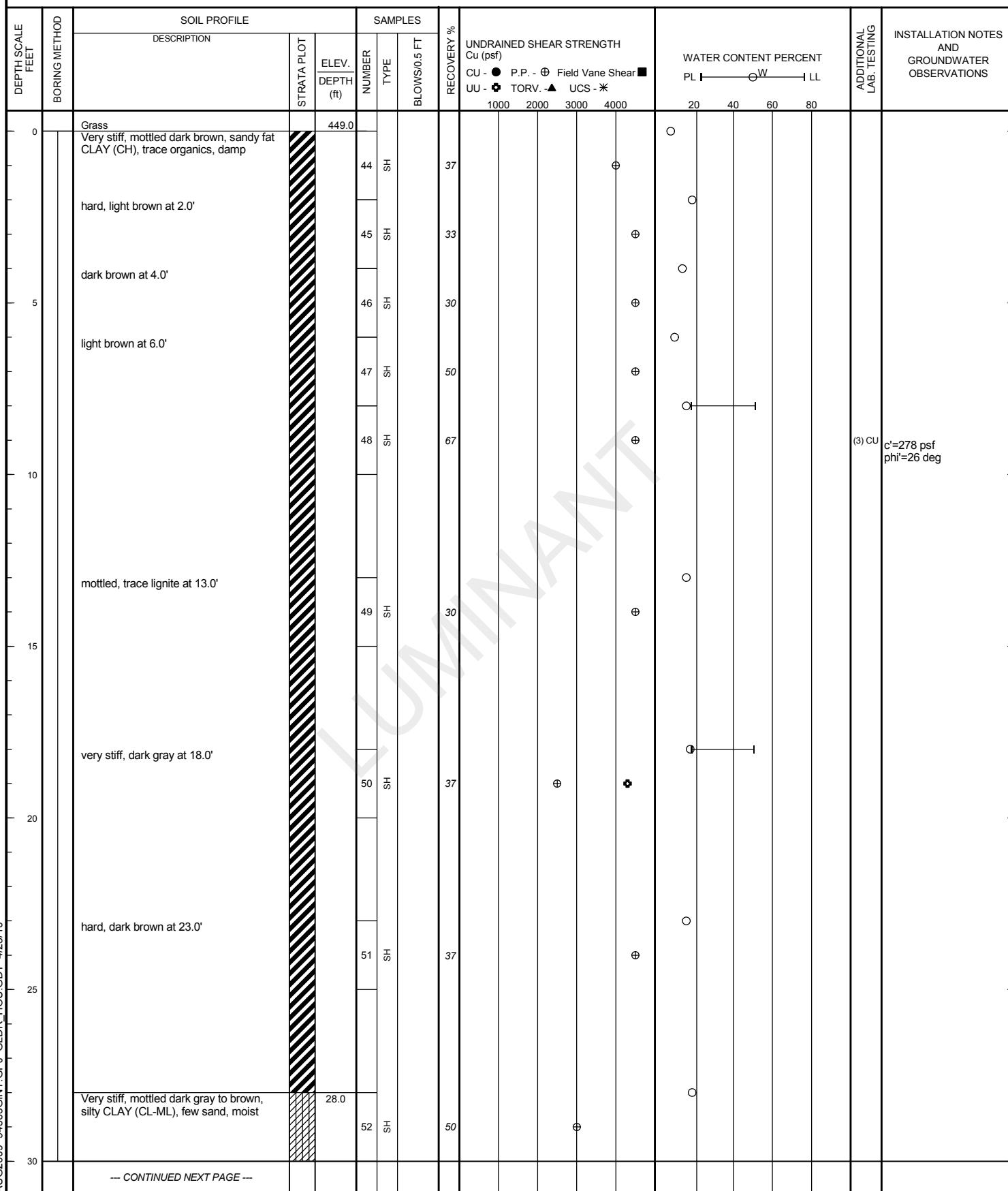
SHEET 1 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5129
EASTING (ft): 3149
ELEVATION (ft): 449



HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

--- CONTINUED NEXT PAGE ---

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-105

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 24-Mar-2010
BORING FINISHED: 24-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 5129
EASTING (ft): 3149
ELEVATION (ft): 449

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)				WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL	
30		--- CONTINUED FROM PREVIOUS PAGE ---		30.0													
33.0		Stiff, black, sandy SILT (ML), trace clay, some organics, some wood fragments, moist		33.0													
33.8		Stiff, dark brown, fat CLAY (CH), trace organics, trace sand, moist		33.8	53	SI	50										
38.0		Very dense, light brown, fine, poorly-graded SAND (SP), trace clay, damp		38.0	54	SS	56										
43.0		Very dense, light brown, fine, poorly-graded SAND (SP-SM), with silt, moist		43.0	55	SS	67										
48.0		Very dense, grayish brown, silty SAND (SM), trace clay, moist		48.0	56	SS	83										
50.0		BORING TERMINATED AT 50.0'		50.0													

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-106

SHEET 1 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 23-Mar-2010
BORING FINISHED: 23-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 4731
EASTING (ft): 2675
ELEVATION (ft): 425

DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)					WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL		
0		Grass Stiff, mottled dark gray, sandy lean CLAY (CL), trace silt, damp		425.0		SH	37		⊕					20	40	60	80	
2		light brown to dark brown at 2.0'			97	SH	37											
4		hard, brownish red, moist at 4.0'			98	SH	40											
6		damp at 6.0'			99	SH	33											
8		mottled brownish red at 8.0'			100	SH	33											
10		mottled gray, little silt at 13.0'			101	SH	40											
12					102	SH	37											
14					103	SH	43											
16					104	SH	43											
18					105	SS	7 10 17 N27											
20							61											
22																		
24																		
26		Compact, light gray, fine silty SAND (SM), moist		23.0														
28		wet at 28.0'																
30		---																

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

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DEPTH SCALE

1 inch to 3.8 feet



LOGGED: DM

CHECKED: PCM

RECORD OF BOREHOLE BH-FGD-106

SHEET 2 OF 2
DATUM: GEODETIC

PROJECT: Luminant Pond Stability Geotechnical
Investigation
LOCATION: Oak Grove, Texas

BORING STARTED: 23-Mar-2010
BORING FINISHED: 23-Mar-2010

DRILLING EQUIPMENT: Buggy Mounted Rig
DRILLING OPERATOR: Van & Sons

NORTHING (ft): 4731
EASTING (ft): 2675
ELEVATION (ft): 425

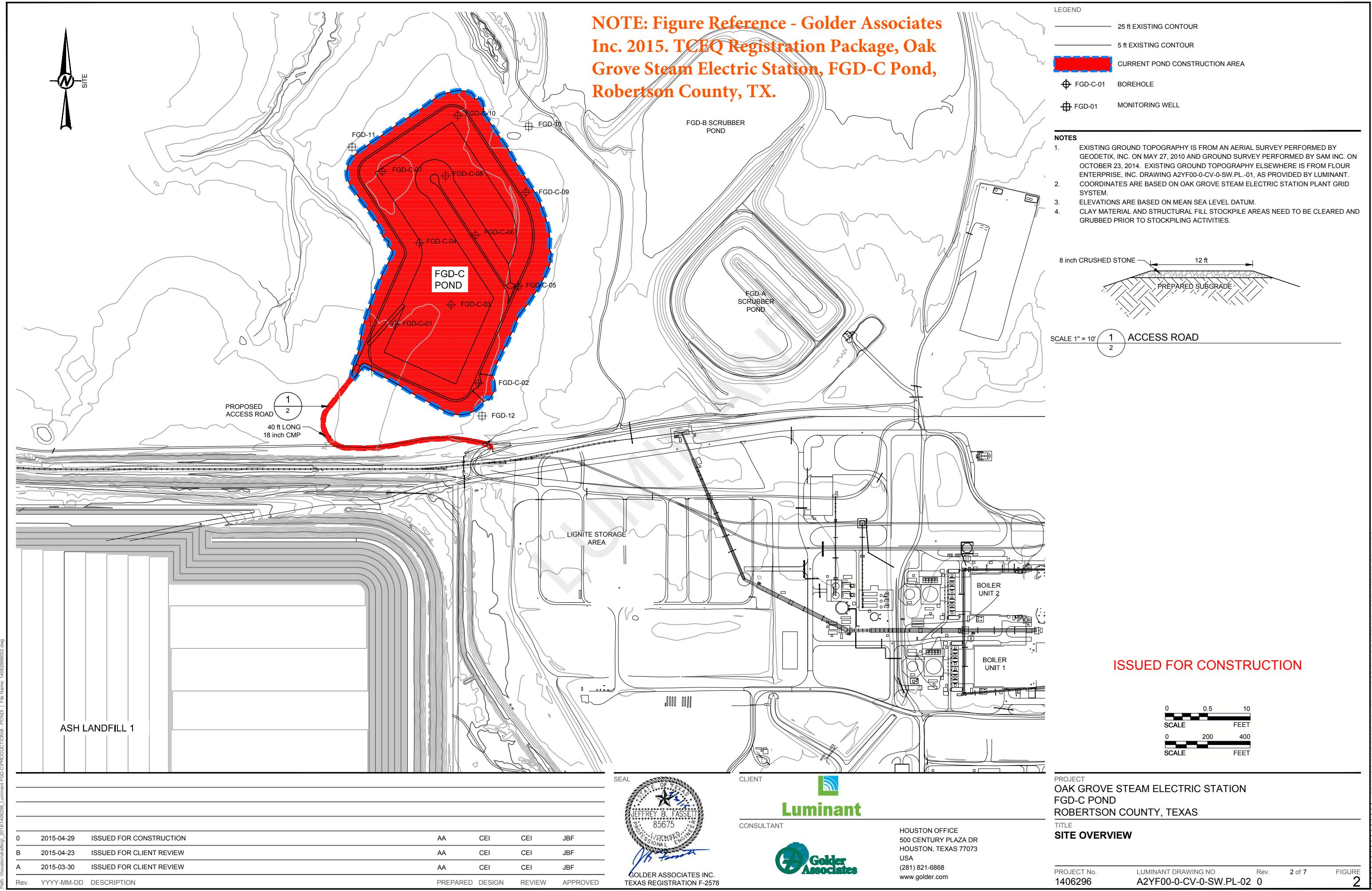
DEPTH SCALE FEET	BORING METHOD	SOIL PROFILE		SAMPLES			RECOVERY %	UNDRAINED SHEAR STRENGTH Cu (psf)					WATER CONTENT PERCENT				ADDITIONAL LAB. TESTING	INSTALLATION NOTES AND GROUNDWATER OBSERVATIONS
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (ft)	NUMBER	TYPE		CU - ● P.P. - ⊕ Field Vane Shear ■	UU - ✕ TORV. ▲ UCS - *	1000	2000	3000	4000	PL	W	LL		
30		-- CONTINUED FROM PREVIOUS PAGE --		30.0														
		BORING TERMINATED AT 30.0'																
35																		
40																		
45																		
50																		
55																		
60																		

HOU SOIL AUG2009 94563GINT GPJ GLDR HOU GDT 4/23/10

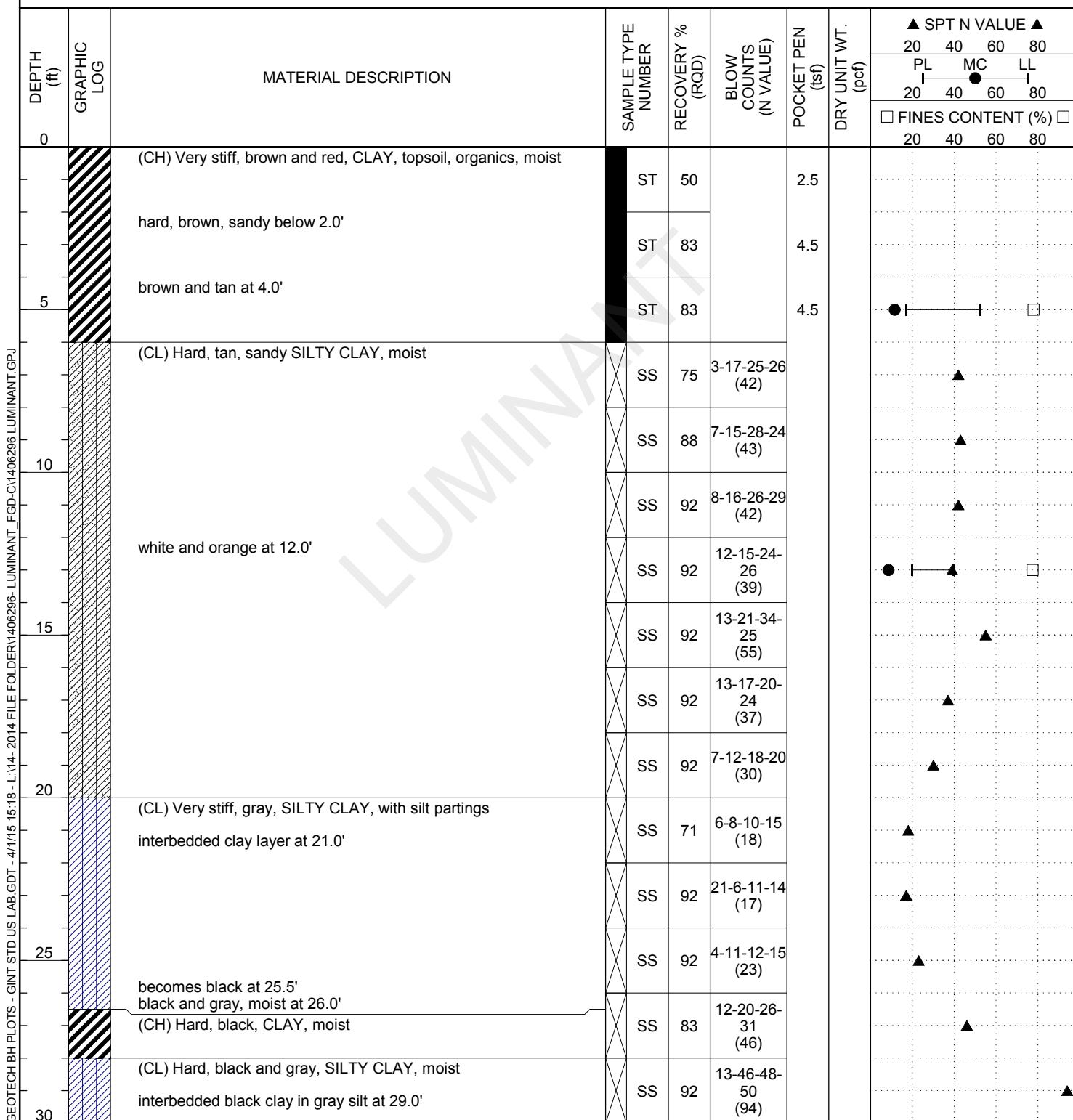
DEPTH SCALE
1 inch to 3.8 feet



LOGGED: DM
CHECKED: PCM



CLIENT	Luminant Power	PROJECT NAME	Luminant
PROJECT NUMBER	1406296	PROJECT LOCATION	Oak Grove SES
DATE STARTED	11/25/14	COMPLETED	11/25/14
DRILLING CONTRACTOR	Envirotech	GROUND ELEVATION 444.5 ft HOLE SIZE 6 inches	
DRILLING METHOD	Auger	GROUND WATER LEVELS:	
LOGGED BY	DMW	AT TIME OF DRILLING	
CHECKED BY	AQ	AT END OF DRILLING	
NOTES			





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BOREHOLE FGD-C-01

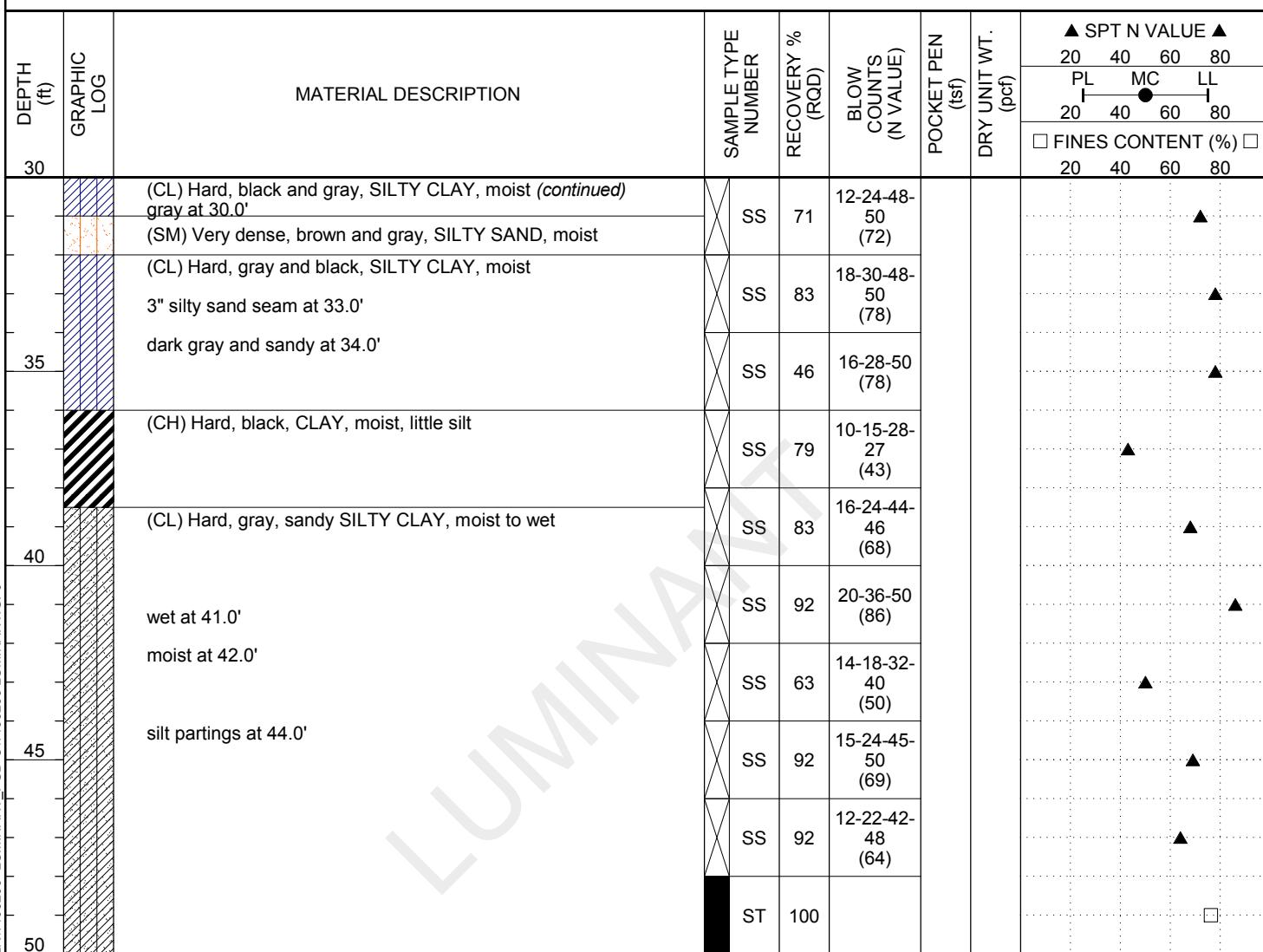
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES





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BOREHOLE FGD-C-02

PAGE 1 OF 2

CLIENT Luminant Power

PROJECT NUMBER 1406296

DATE STARTED 11/17/14 COMPLETED 11/17/14

DRILLING CONTRACTOR Envirotech

DRILLING METHOD Auger

LOGGED BY DMW CHECKED BY AQ

NOTES _____

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES

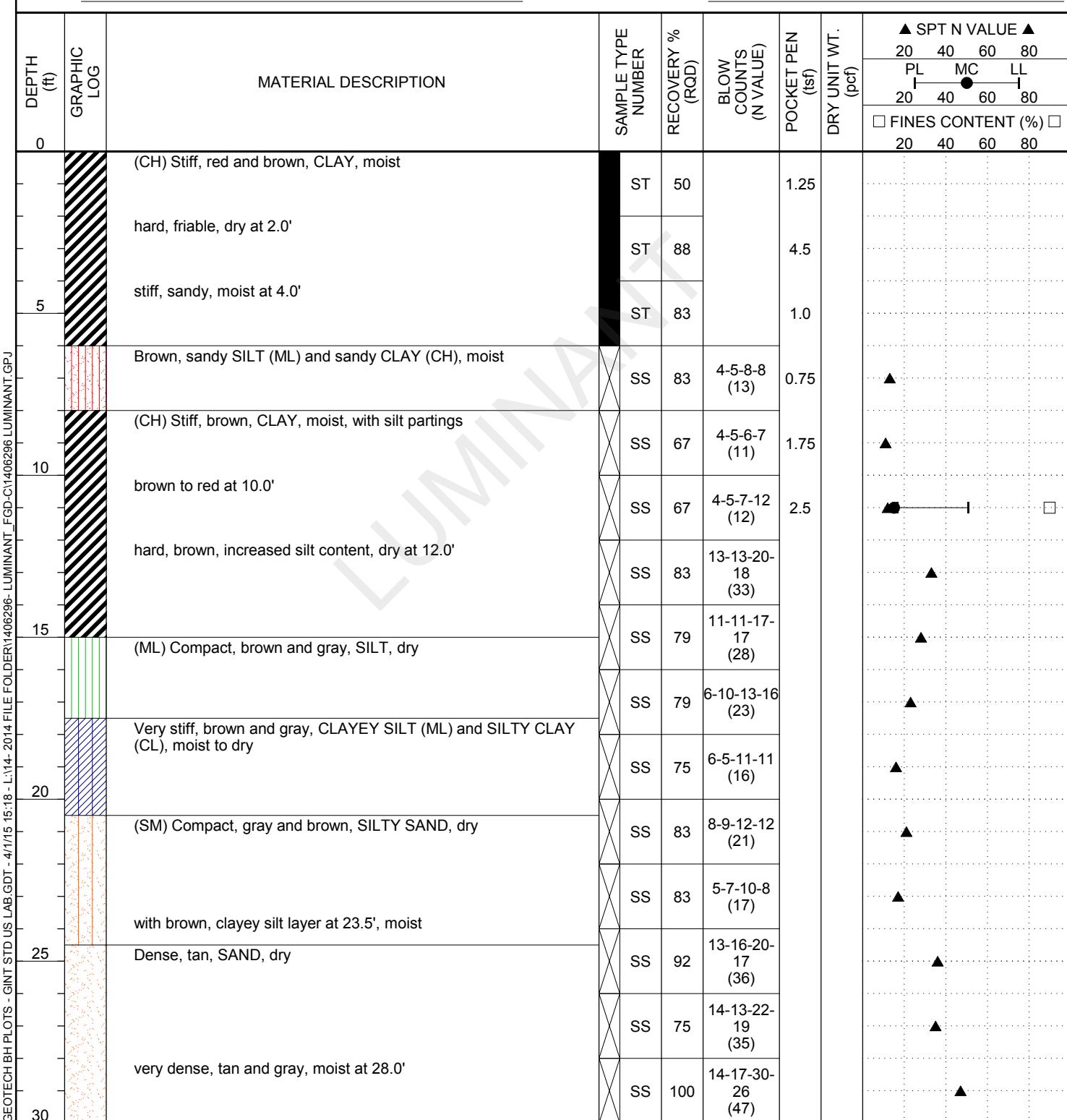
GROUND ELEVATION _____ HOLE SIZE 6 inches

GROUND WATER LEVELS:

AT TIME OF DRILLING 35 35 ft bgs

AT END OF DRILLING _____

AFTER DRILLING _____

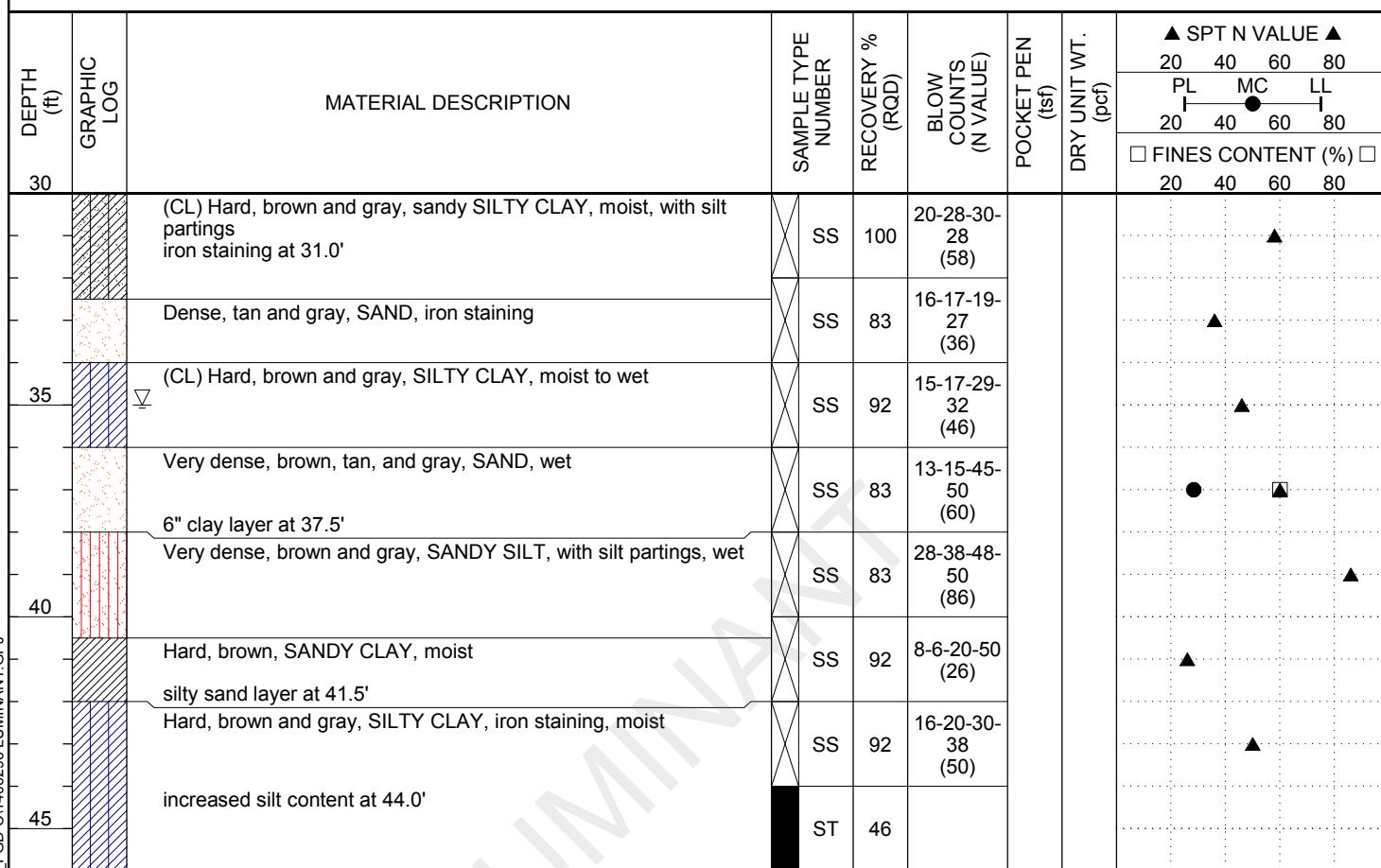


CLIENT Luminant Power

PROJECT NUMBER 1406296

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES



Bottom of borehole at 46.0 feet.



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BOREHOLE FGD-C-03

PAGE 1 OF 2

CLIENT Luminant Power

PROJECT NUMBER 1406296

DATE STARTED 11/24/14 COMPLETED 11/25/14

DRILLING CONTRACTOR Envirotech

DRILLING METHOD Auger

LOGGED BY DMW CHECKED BY AQ

NOTES

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES

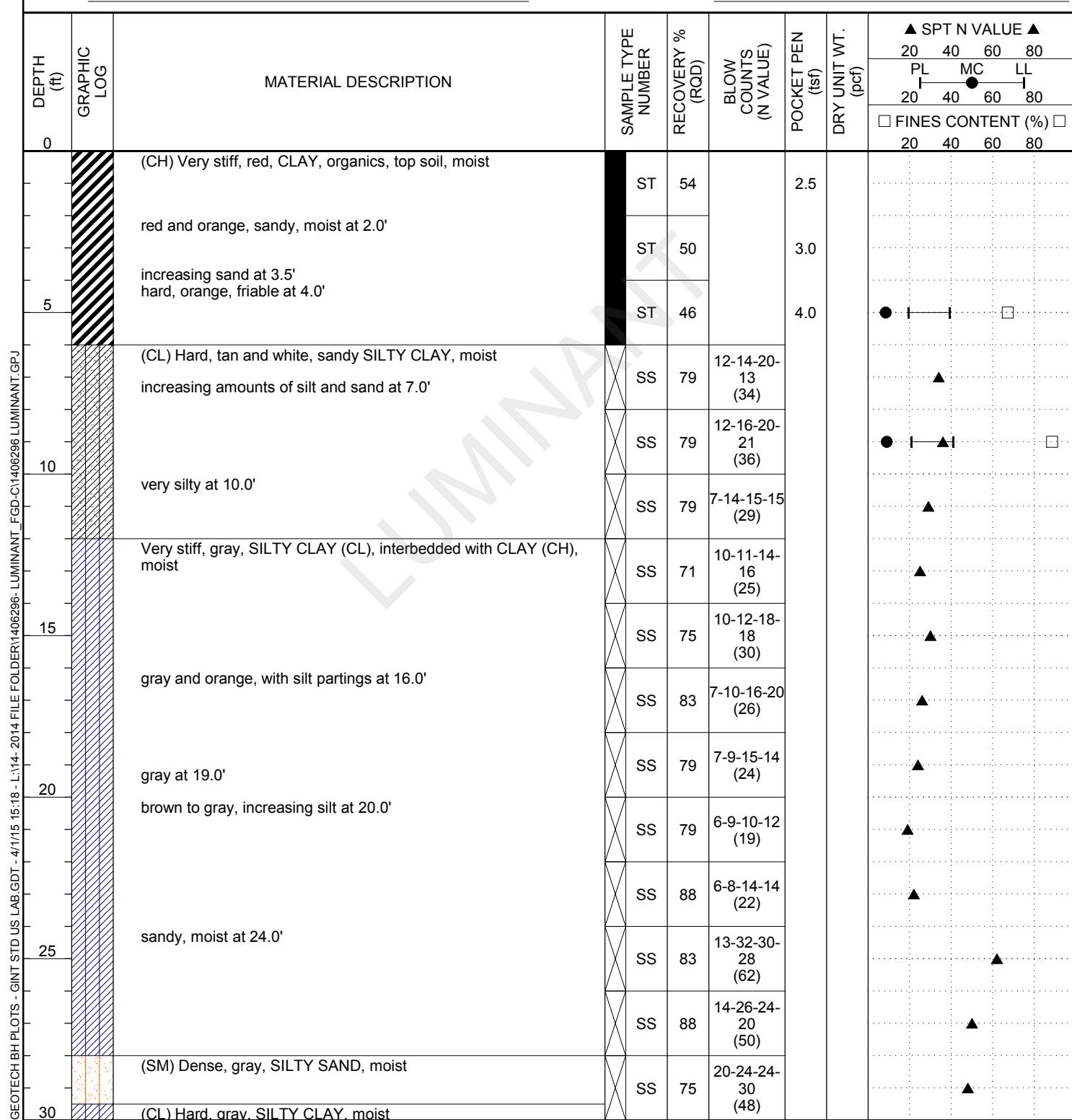
GROUND ELEVATION 443.7 ft HOLE SIZE 6 inches

GROUND WATER LEVELS:

AT TIME OF DRILLING

AT END OF DRILLING

AFTER DRILLING





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BOREHOLE FGD-C-03

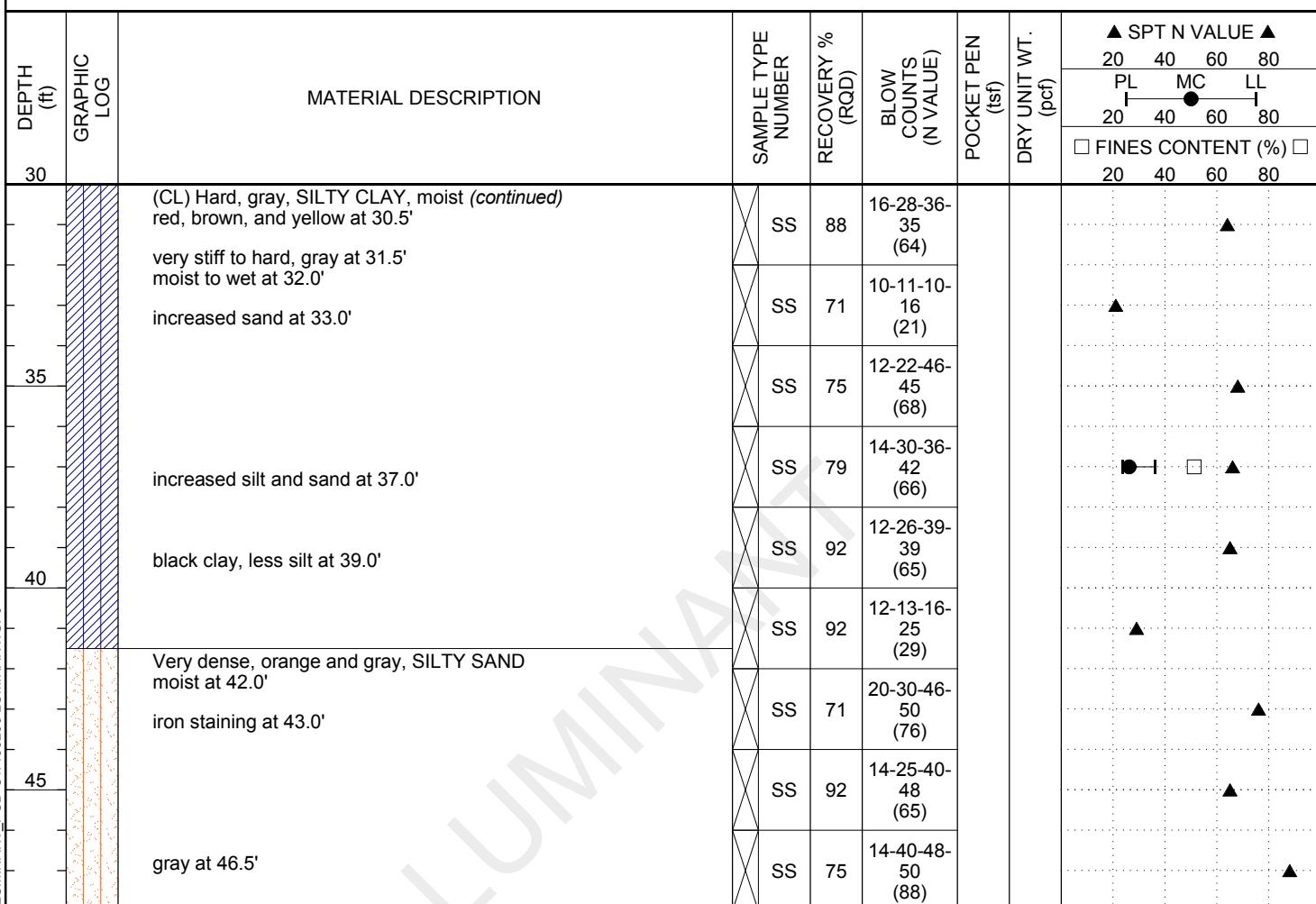
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

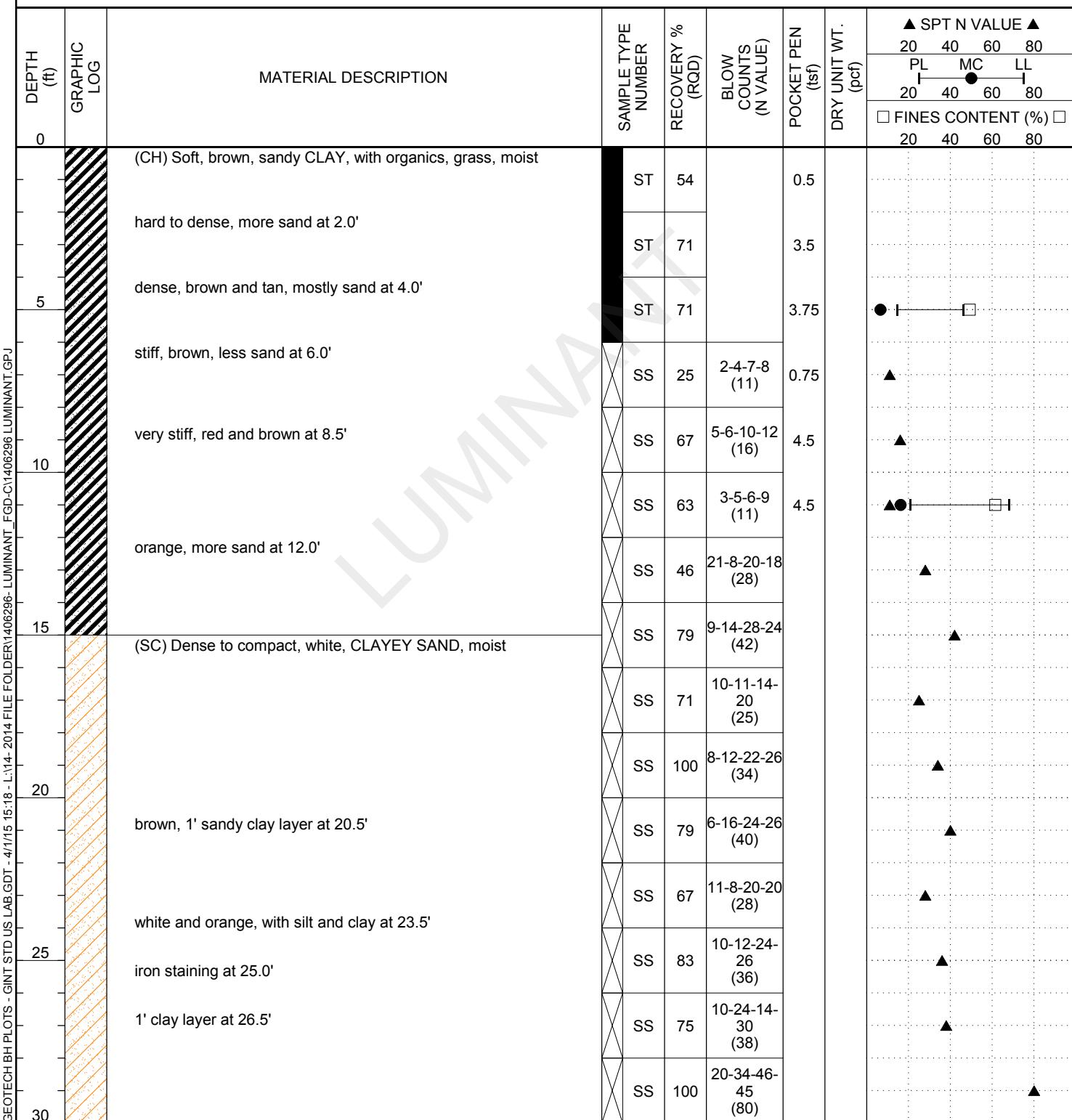
PROJECT LOCATION Oak Grove SES



Bottom of borehole at 48.0 feet.

CLIENT Luminant Power
PROJECT NUMBER 1406296
DATE STARTED 11/20/14 **COMPLETED** 11/20/14
DRILLING CONTRACTOR Envirotech
DRILLING METHOD Auger
LOGGED BY DMW **CHECKED BY** AQ
NOTES

PROJECT NAME Luminant
PROJECT LOCATION Oak Grove SES
GROUND ELEVATION _____ **HOLE SIZE** 6 inches
GROUND WATER LEVELS:
 AT TIME OF DRILLING 42 42 ft bgs
AT END OF DRILLING _____
AFTER DRILLING _____





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BOREHOLE FGD-C-04

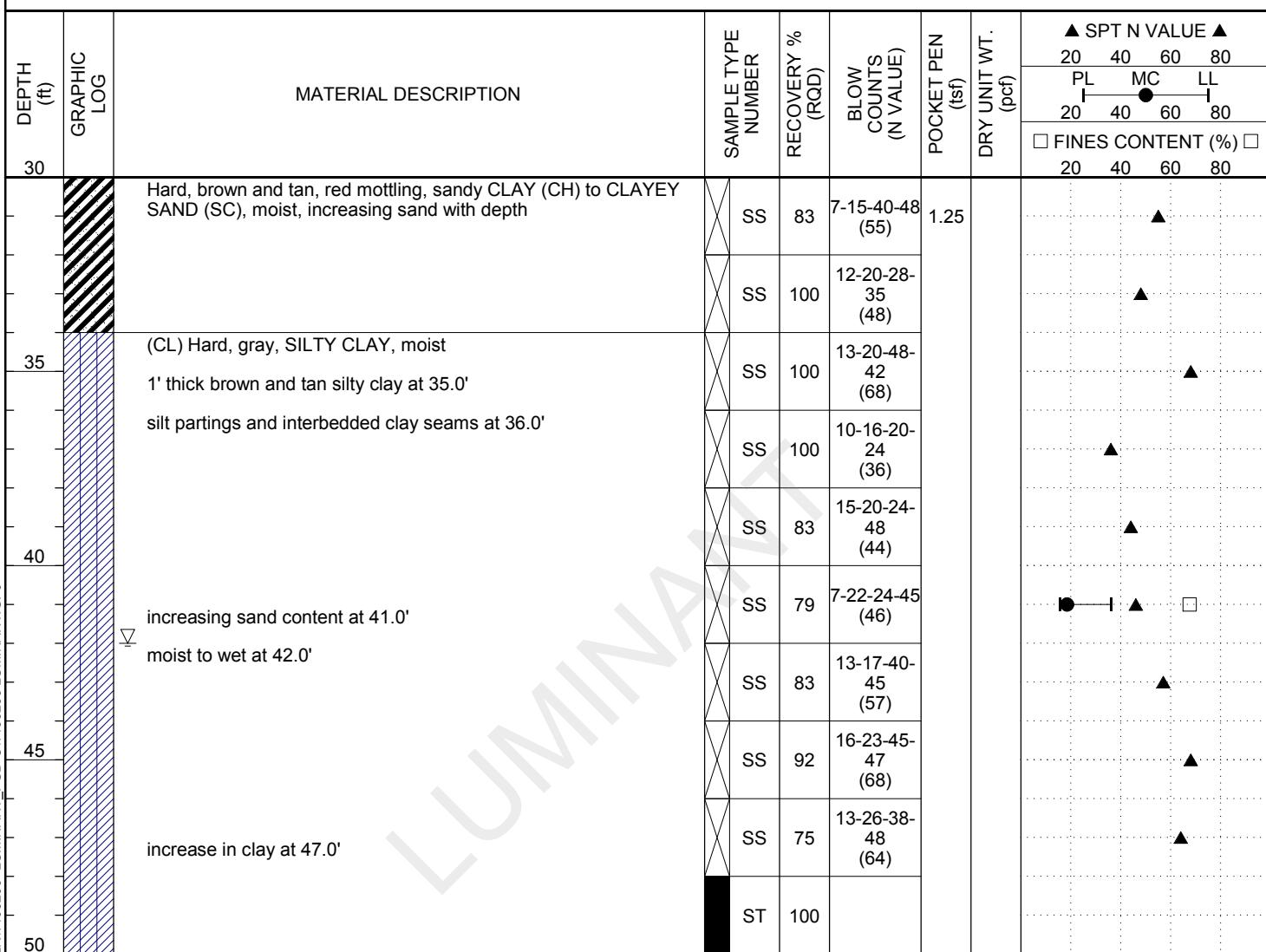
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES





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BOREHOLE FGD-C-05

PAGE 1 OF 2

CLIENT Luminant Power

PROJECT NUMBER 1406296

DATE STARTED 11/18/14 COMPLETED 11/18/14

DRILLING CONTRACTOR Envirotech

DRILLING METHOD Auger

LOGGED BY DMW CHECKED BY AQ

NOTES

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES

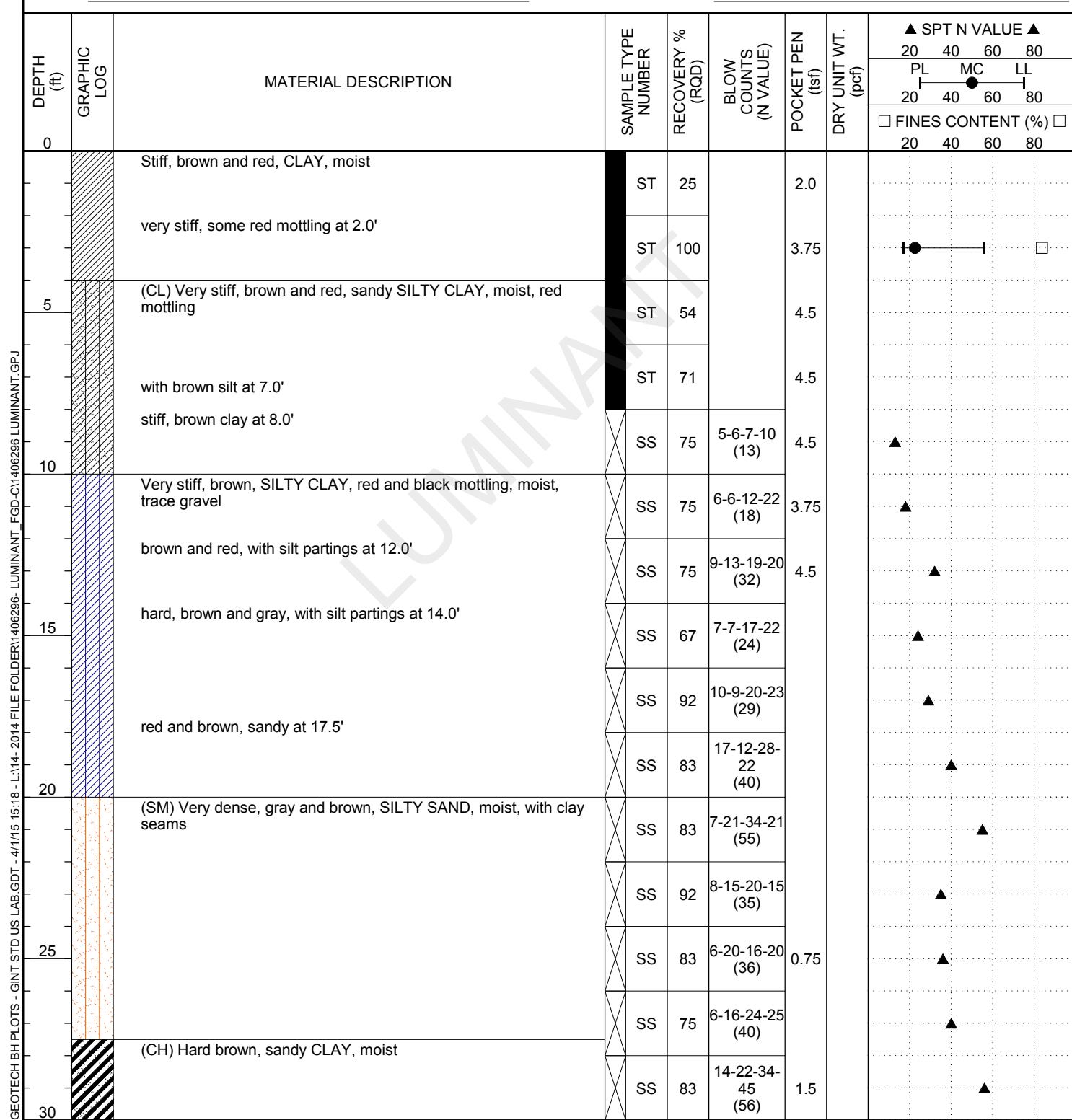
GROUND ELEVATION 440.3 ft HOLE SIZE 6 inches

GROUND WATER LEVELS:

▽ AT TIME OF DRILLING 34 34.0 ft bgs

AT END OF DRILLING

AFTER DRILLING



(Continued Next Page)



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BOREHOLE FGD-C-05

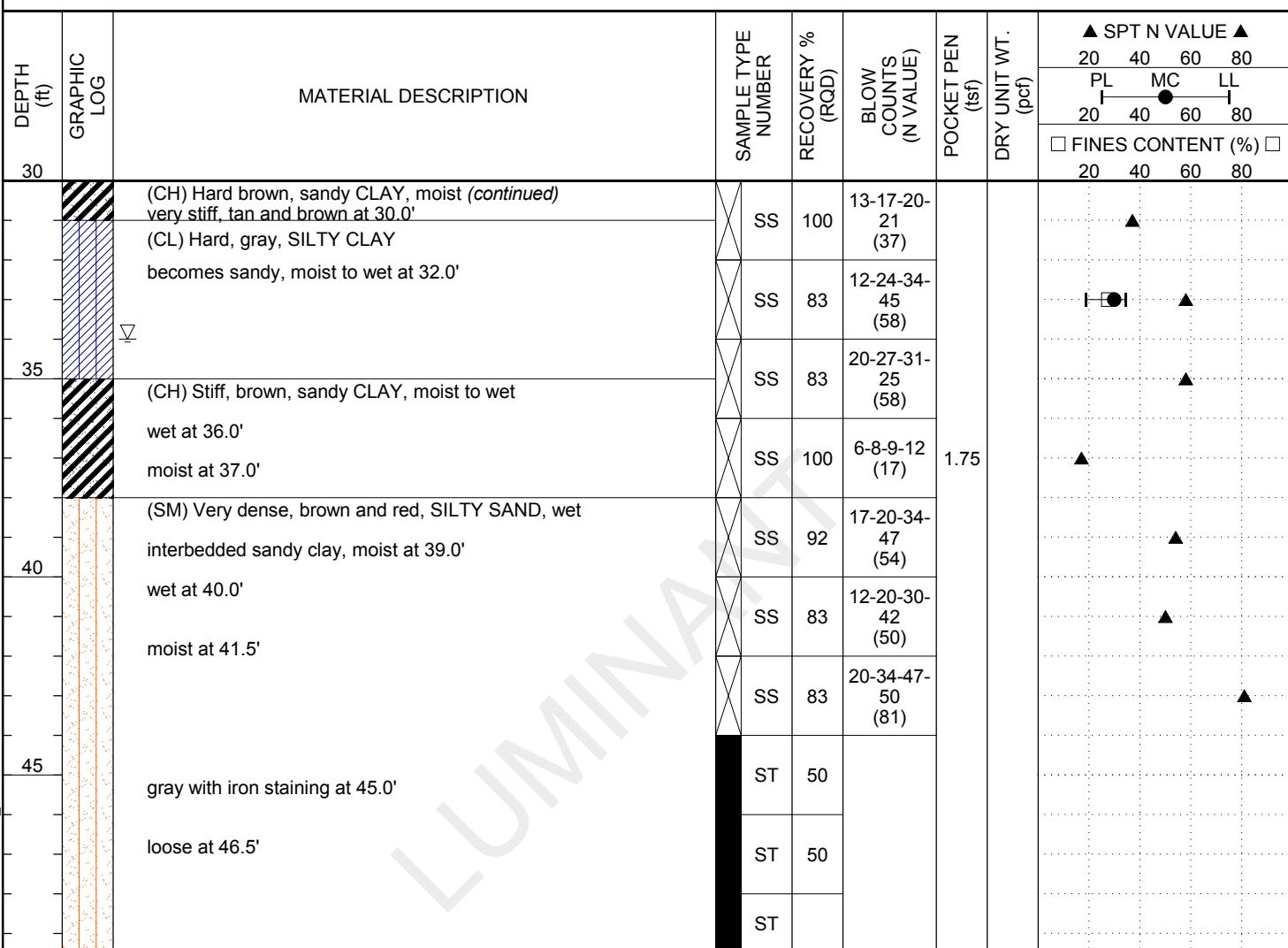
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

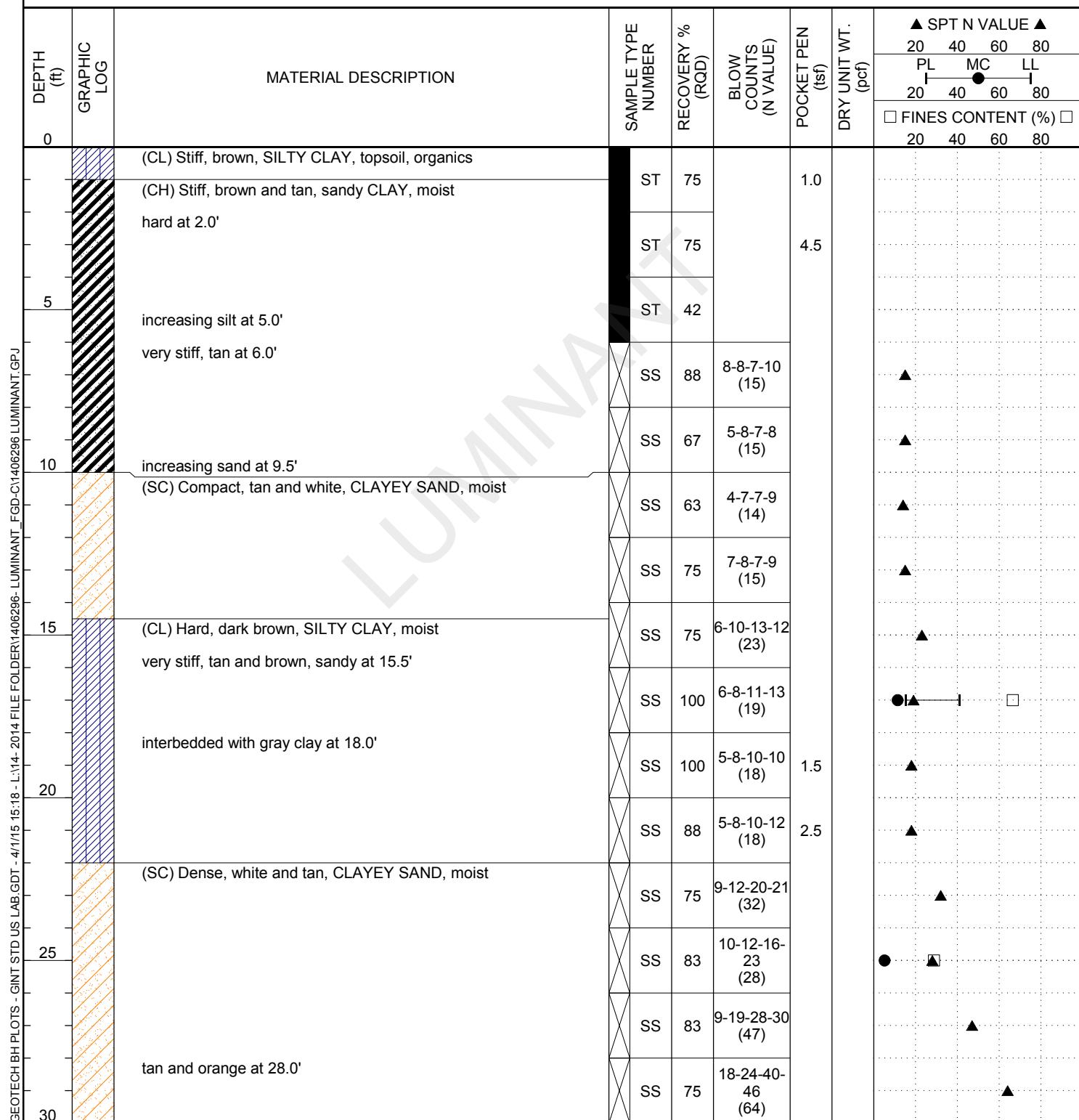
PROJECT LOCATION Oak Grove SES



Bottom of borehole at 49.5 feet.

CLIENT Luminant Power
PROJECT NUMBER 1406296
DATE STARTED 11/24/14 **COMPLETED** 11/24/14
DRILLING CONTRACTOR Envirotech
DRILLING METHOD Auger
LOGGED BY DMW **CHECKED BY** AQ
NOTES

PROJECT NAME Luminant
PROJECT LOCATION Oak Grove SES
GROUND ELEVATION 450.9 ft **HOLE SIZE** 6 inches
GROUND WATER LEVELS:
AT TIME OF DRILLING
AT END OF DRILLING
AFTER DRILLING

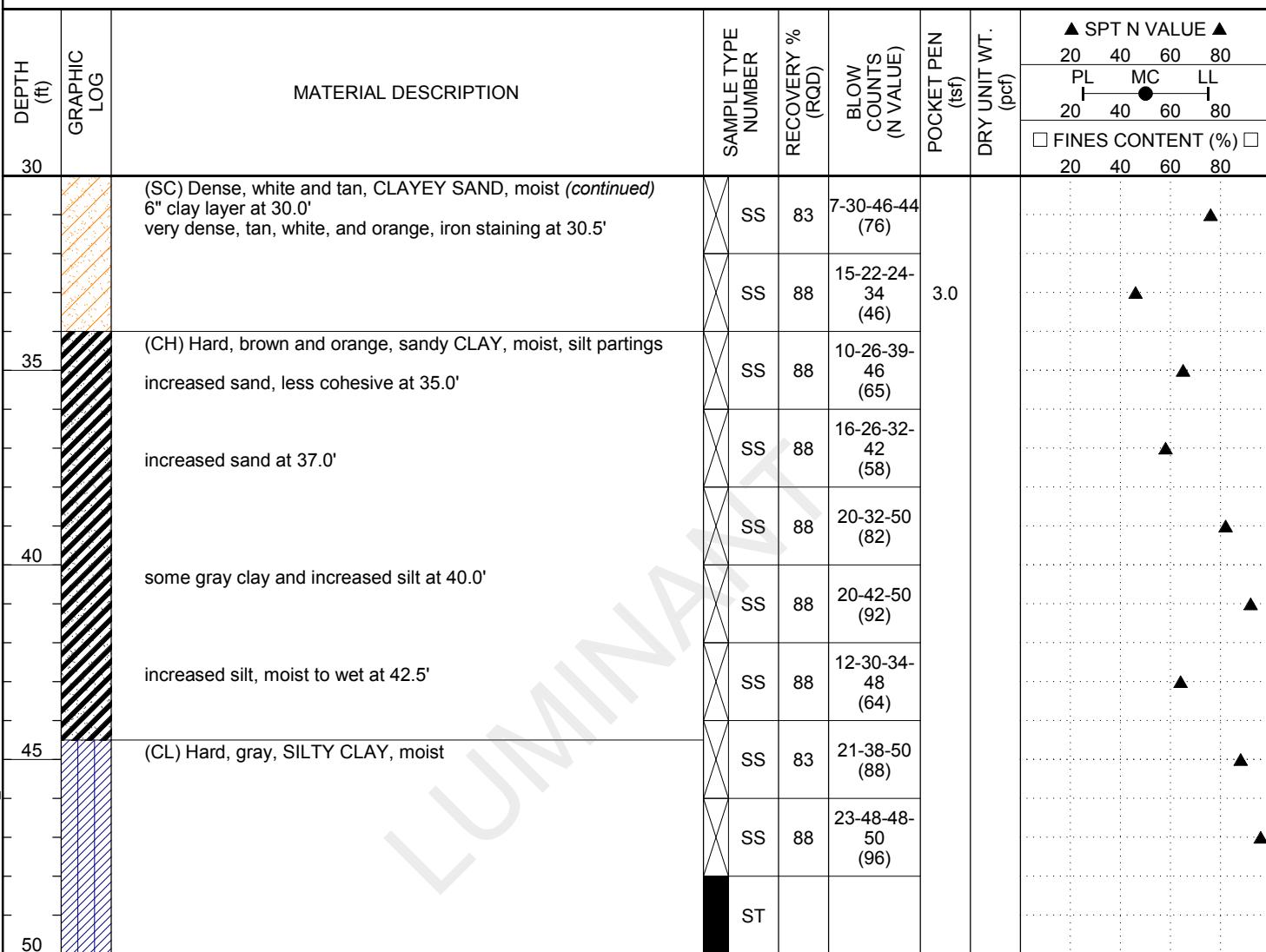


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CLIENT Luminant Power

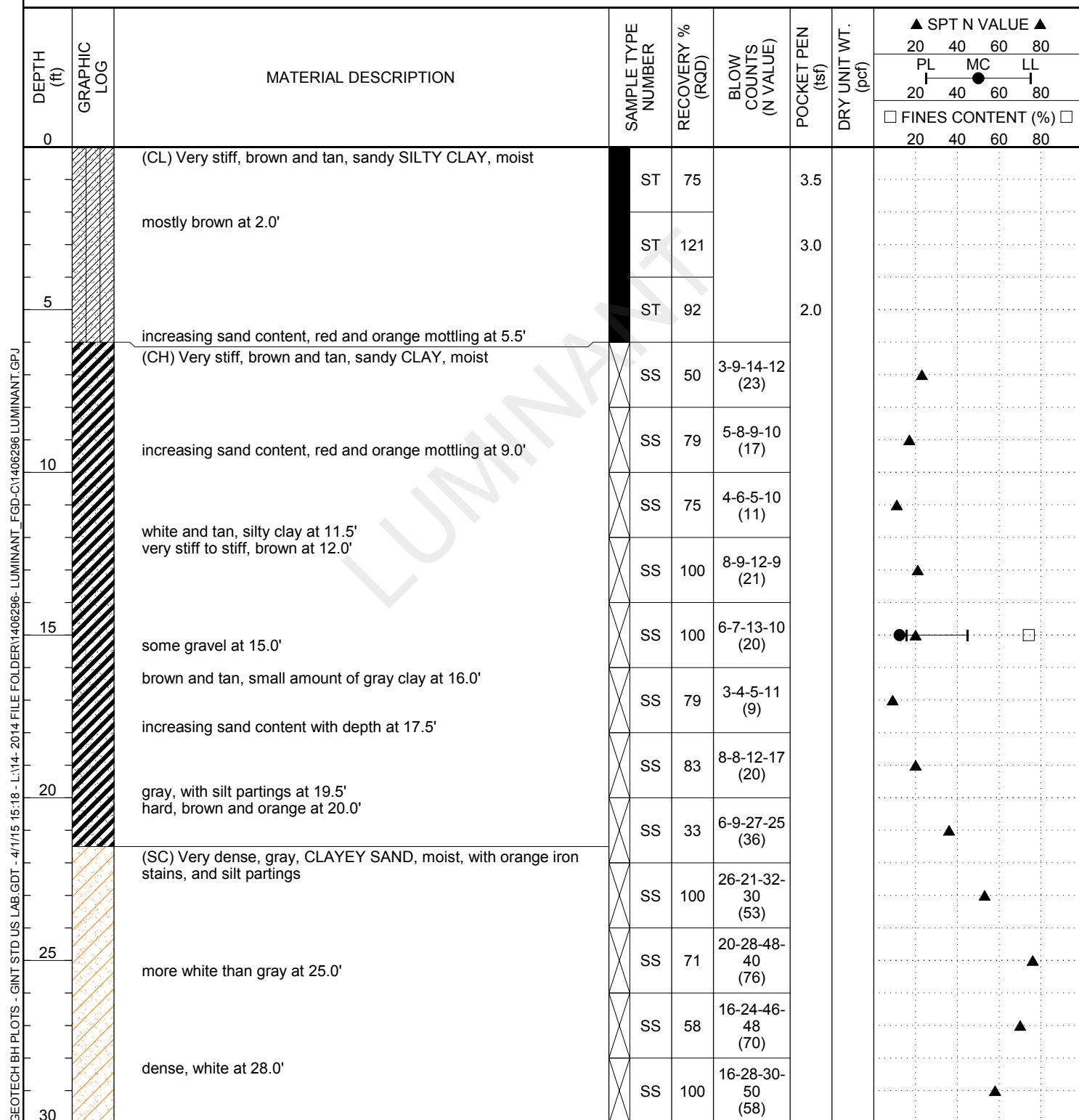
PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES


CLIENT Luminant Power
PROJECT NUMBER 1406296
DATE STARTED 11/20/14 **COMPLETED** 11/21/14
DRILLING CONTRACTOR Envirotech
DRILLING METHOD Auger
LOGGED BY DMW **CHECKED BY** AQ
NOTES

PROJECT NAME Luminant
PROJECT LOCATION Oak Grove SES
GROUND ELEVATION 449.7 ft **HOLE SIZE** 6 inches
GROUND WATER LEVELS:
AT TIME OF DRILLING
AT END OF DRILLING
AFTER DRILLING





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BOREHOLE FGD-C-07

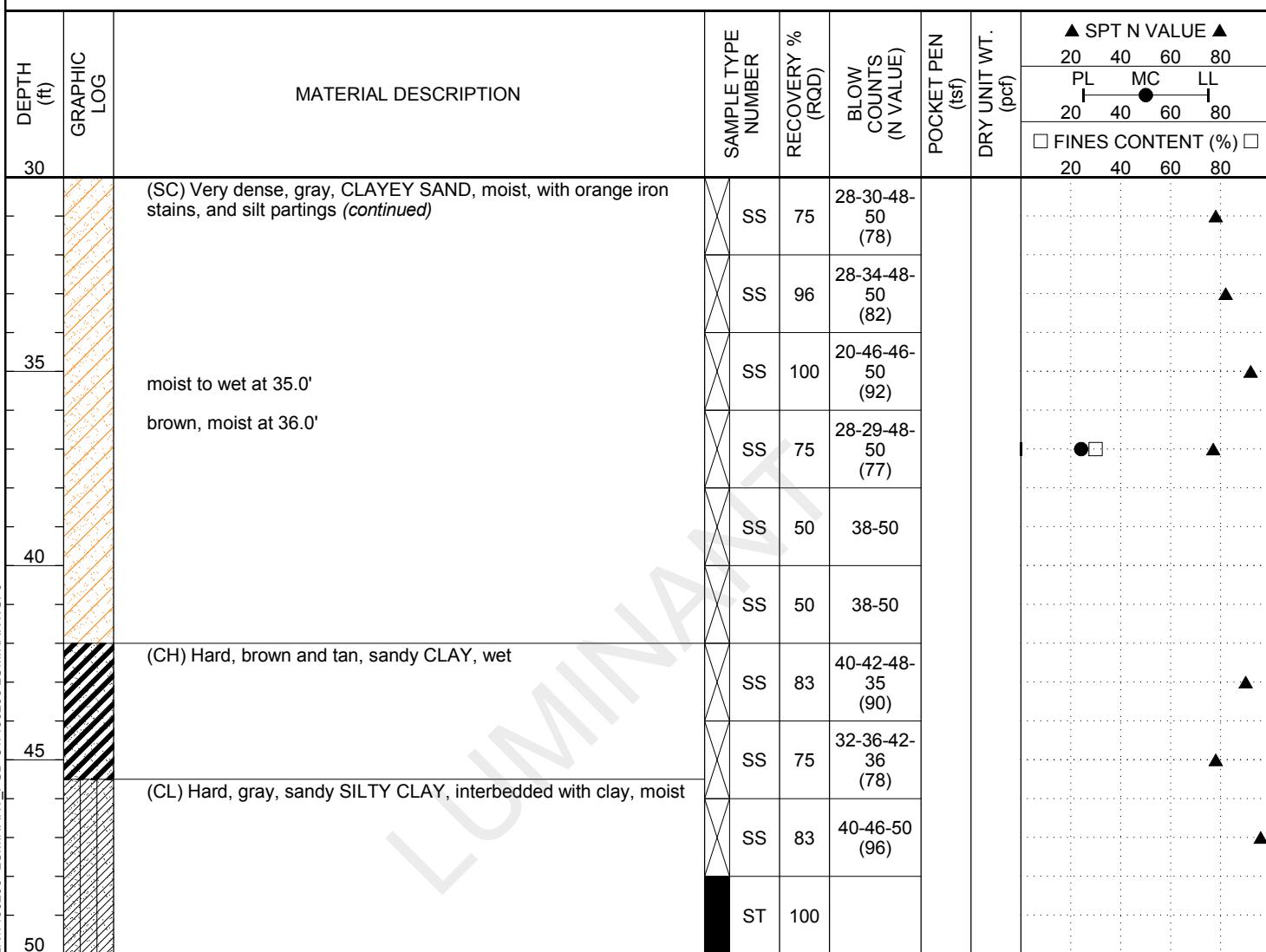
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES



Bottom of borehole at 50.0 feet.



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BOREHOLE FGD-C-08

PAGE 1 OF 2

CLIENT Luminant Power

PROJECT NUMBER 1406296

DATE STARTED 11/19/14 COMPLETED 11/19/14

DRILLING CONTRACTOR Envirotech

DRILLING METHOD Auger

LOGGED BY DMW CHECKED BY AQ

NOTES

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES

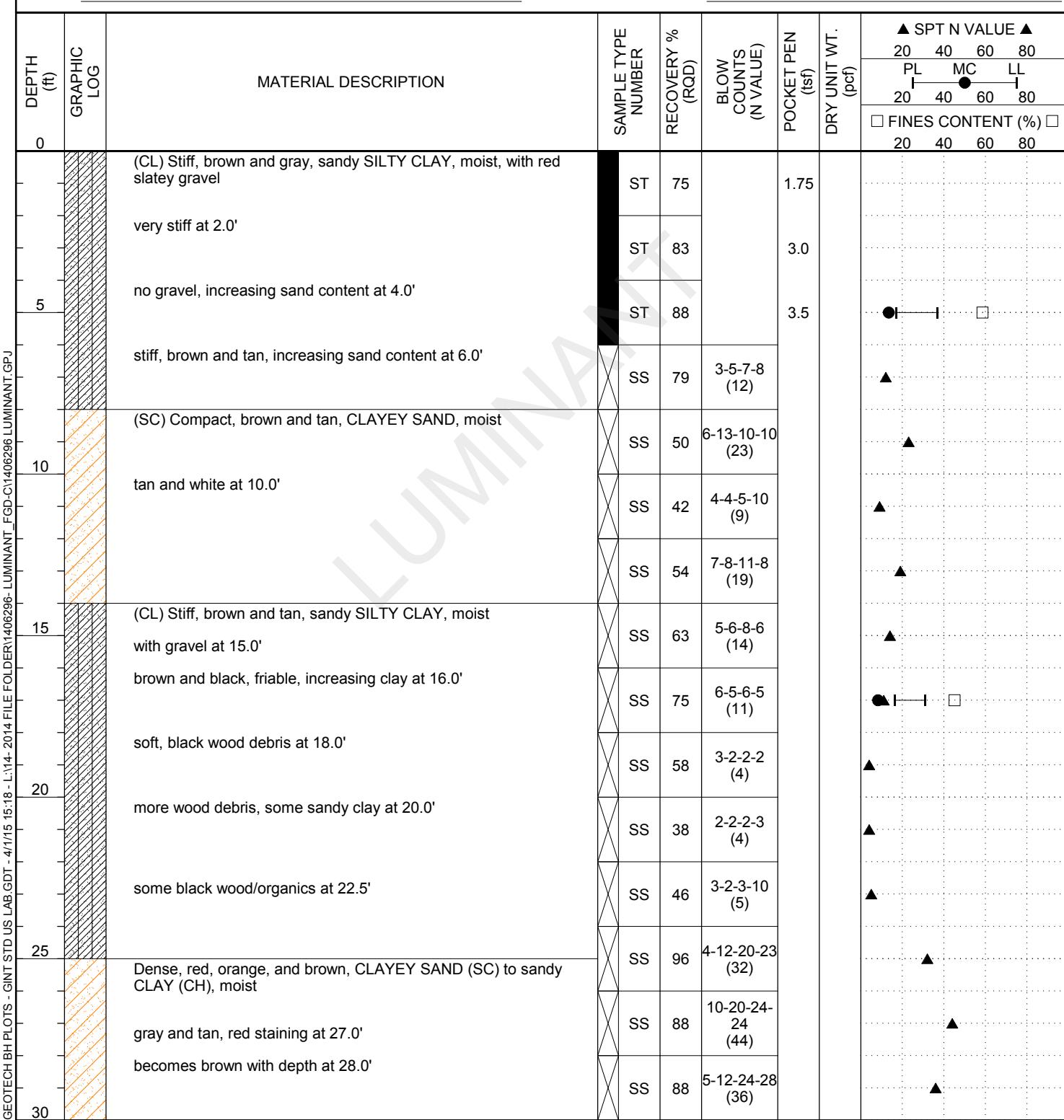
GROUND ELEVATION 448.7 ft HOLE SIZE 6 inches

GROUND WATER LEVELS:

AT TIME OF DRILLING

AT END OF DRILLING

AFTER DRILLING





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BOREHOLE FGD-C-08

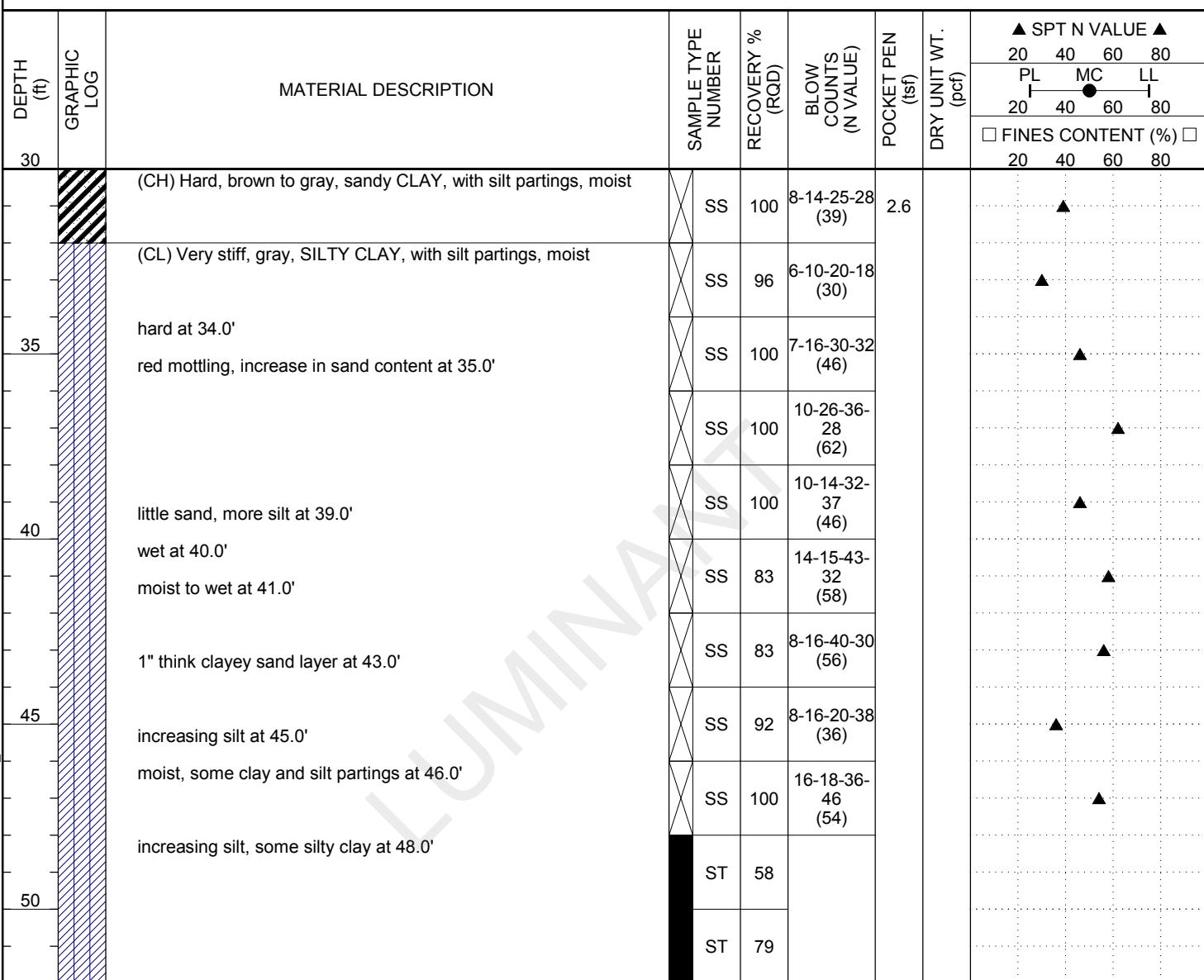
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NUMBER 1406296

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES



CLIENT Luminant Power

PROJECT NUMBER 1406296

DATE STARTED 11/18/14 **COMPLETED** 11/19/14

DRILLING CONTRACTOR Envirotech

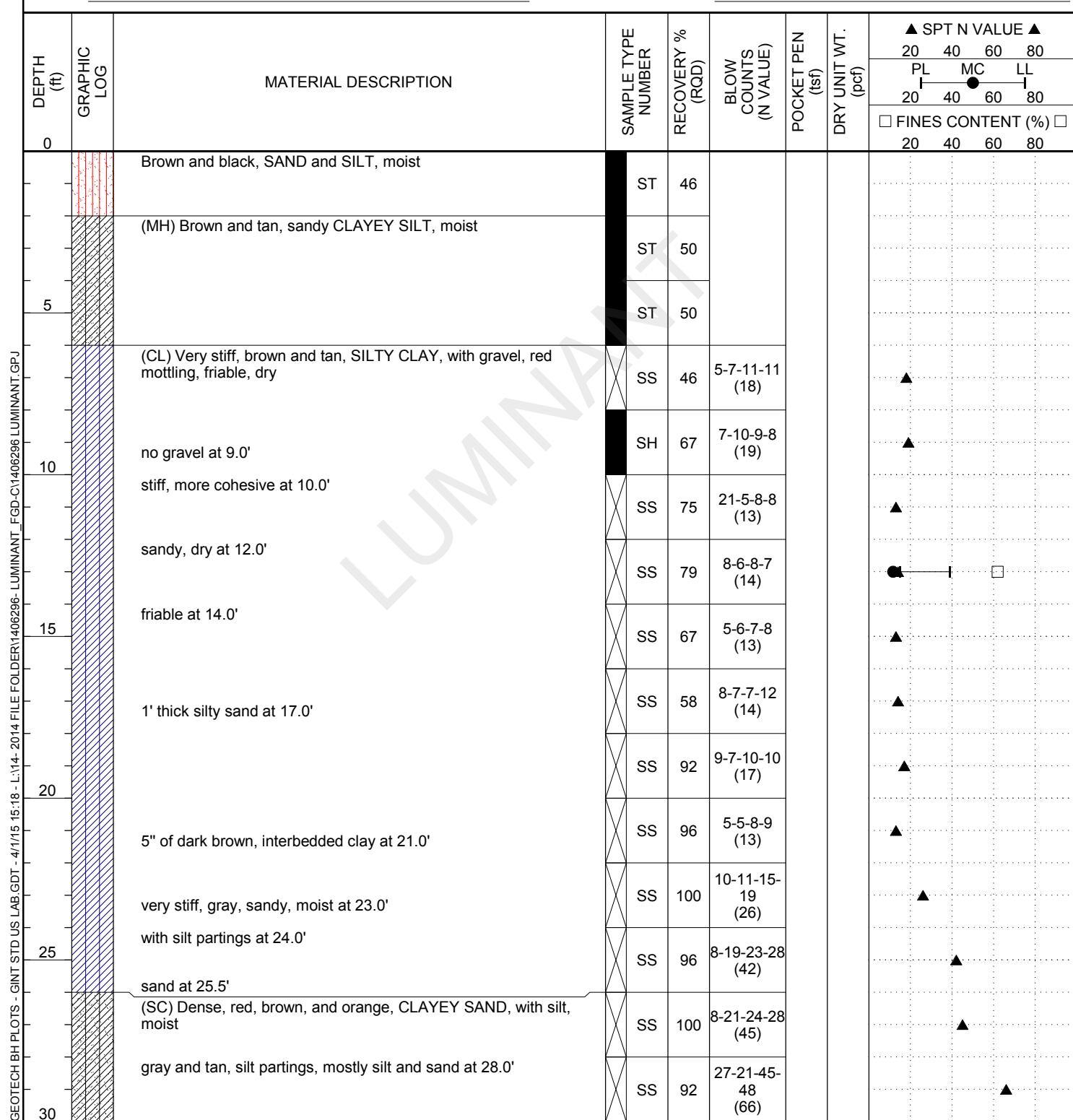
DRILLING METHOD Auger

LOGGED BY DMW **CHECKED BY** AQ

NOTES
PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES

GROUND ELEVATION 445 ft **HOLE SIZE** 6 inches

GROUND WATER LEVELS:
AT TIME OF DRILLING
AT END OF DRILLING
AFTER DRILLING


(Continued Next Page)

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN (tsf)	▲ SPT N VALUE ▲			
							PL	MC	LL	DRY UNIT WT. (pcf)
30		(CL) Hard, brown and tan, SILTY CLAY, moist 6" silty sand layer at 31.5' brown and gray, iron staining at 32.0' increasing silt and sand at 33.0'	SS	92	9-20-46-50 (66)					
35		gray, with silt partings, moist at 36.0' with interbedded brown, silty clay at 37.0'	SS	83	13-28-48- 32 (76)					
40		moist to wet at 39.0' moist at 40.0'	SS	100	14-26-46- 48 (72)					
45		with silt partings at 42.0'	SS	92	20-32-48- 50 (80)					
50		with interbedded gray, clay at 45.0' brown, sandy at 46.0' with interbedded gray clay at 47.0'	SS	92	18-22-33- 43 (55)					
55		(CH) Very stiff, brown and gray, sandy CLAY, moist gray, with silt partings at 52.0'	ST	42	24-34-46- 30 (80)					
55		stiff, increasing sand with depth at 56.0'	ST	67	26-32-38- 34 (70)					
60		Stiff, gray, SILTY CLAY with black mudstone or slate at 59.0'	ST	100	13-40-48- 50 (88)					
60		Bottom of borehole at 60.0 feet.	ST	75	14-39-44- 48 (83)					
60			ST	67	3.5					
60			ST	50	3.5					
60			ST	100	3.5					
60			ST	100	4.0					
60			ST	75	1.75					
60			ST	67	1.75					



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BOREHOLE FGD-C-10

PAGE 1 OF 2

CLIENT Luminant Power

PROJECT NUMBER 1406296

DATE STARTED 11/19/14 COMPLETED 11/20/14

DRILLING CONTRACTOR Envirotech

DRILLING METHOD Auger

LOGGED BY DMW CHECKED BY _____

NOTES _____

PROJECT NAME Luminant

PROJECT LOCATION Oak Grove SES

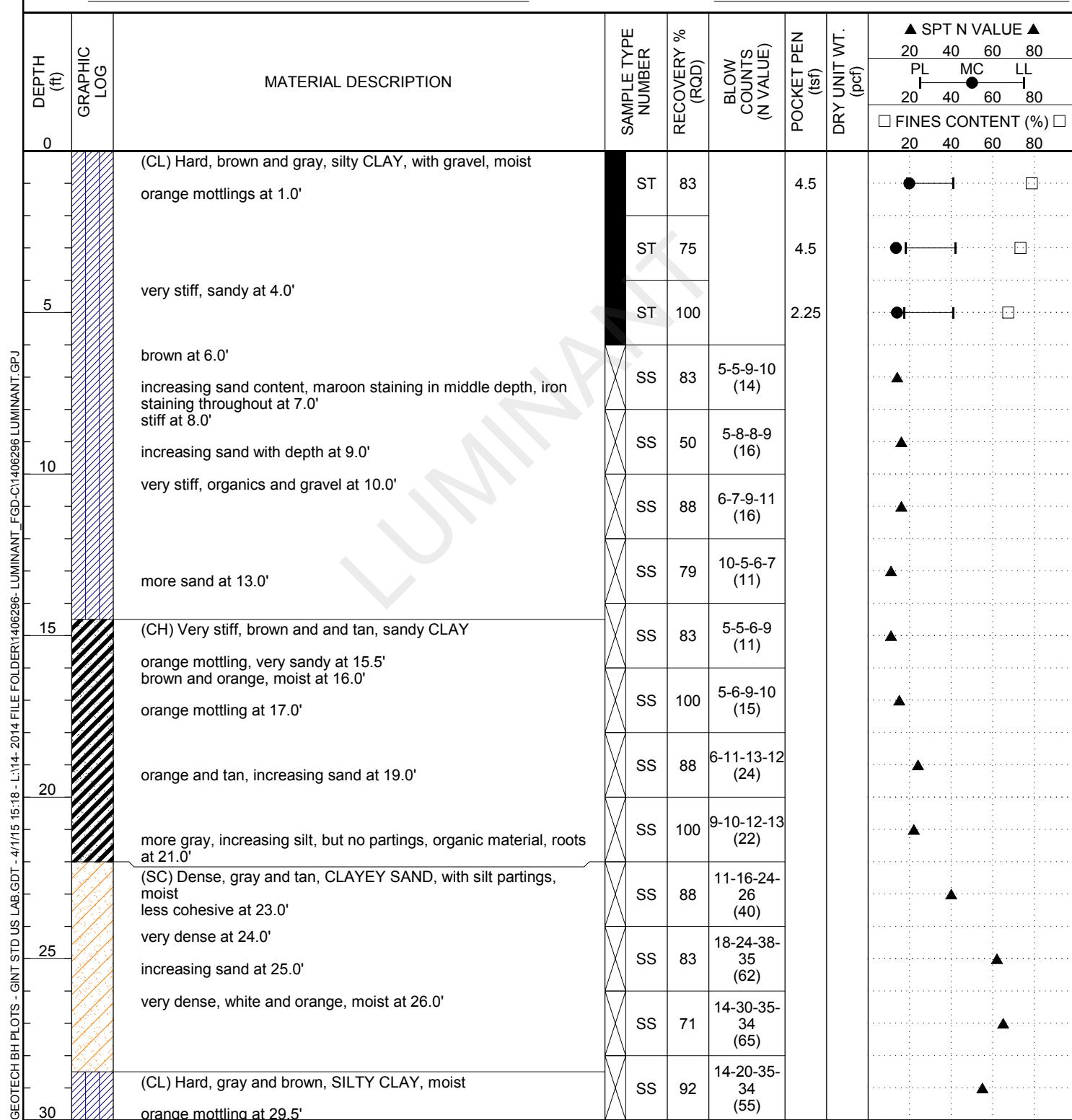
GROUND ELEVATION 445 ft HOLE SIZE 6 inches

GROUND WATER LEVELS:

AT TIME OF DRILLING

AT END OF DRILLING

AFTER DRILLING



(Continued Next Page)



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BOREHOLE FGD-C-10

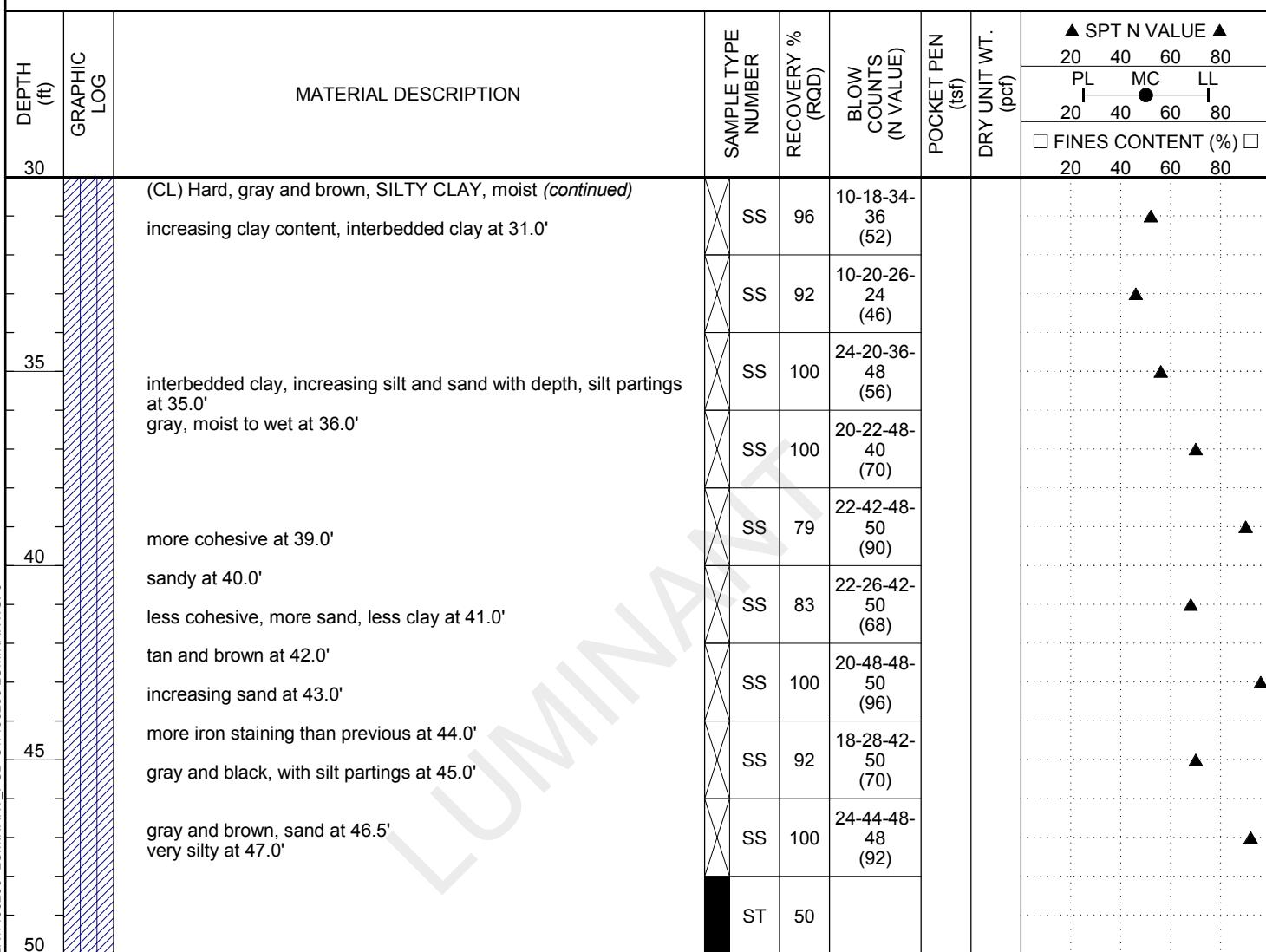
PAGE 2 OF 2

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES



Bottom of borehole at 50.0 feet.

APPENDIX B
LABORATORY TEST RESULTS

SUMMARY OF SOIL DATA AND LABORATORY TEST RESULTS

Borehole Number	Sample Number	Sample		Sample Type	SPT N Value (blows/1 ft)	Moisture Content (%)	Soil Description	Atterberg Limits					Particle Size Analysis				Dry Unit wt (pcf)	Moist Unit wt (pcf)	CU Triaxial		UU Triaxial		Consolidation				Organic Content (%)
		Depth Interval (ft-bgs)	Elevation of Top (ft)					LL	PL	PI	LI	USCS	Gravel (%)	Sand (%)	Silt (%)	Clay (%)			c' (psf)	phi' (deg)	UU - c _u (psf)	Confining Pressure (psf)	Type	C _c	C _r	σ _p (psf)	
BH-FGD-101	88	0.0-2.0		SH	18.2	Very stiff, mottled, sandy lean CLAY (CL), damp																					
BH-FGD-101	89	2.0-4.0		SH	11.9	hard, mottled reddish brown at 2.0'																					
BH-FGD-101	90	4.0-6.0		SH	18.4	trace silt at 4.0'																					
BH-FGD-101	91	6.0-8.0		SH	13.6	very stiff, reddish brown and light gray, some silt at 6.0'																					
BH-FGD-101	92	8.0-10.0		SH	18.4	Dense, grayish brown, SAND (SP-SM), with silt, damp																					
BH-FGD-101	93	13.0-15.5		SH	27.0	Very stiff, grayish brown, clayey fine SAND (SC), with some silt, layered																					
BH-FGD-101		-				gray and light brown at 13.5'																					
BH-FGD-101	94	18.0-20.0		SS	50	25.5	Very dense, light brown, fine, poorly-graded SAND (SP), damp																				
BH-FGD-101	95	23.0-25.0		SS	50	27.6	little clay at 23.0'																				
BH-FGD-101	96	28.0-30.0		SS	35	28.7	dense, wet at 28.0'																				
BH-FGD-101		-					BORING TERMINATED AT 30.0'																				



Project: Luminant Pond Stability Geotechnical Investigation
Location: Oak Grove, Texas

SUMMARY OF SOIL DATA AND LABORATORY TEST RESULTS

Sample				Sample Type	SPT N Value (blows/1 ft)	Moisture Content (%)	Soil Description	Atterberg Limits					Particle Size Analysis				Dry Unit wt (pcf)	Moist Unit wt (pcf)	CU Triaxial		UU Triaxial		Consolidation				Organic Content (%)
Borehole Number	Sample Number	Depth Interval (ft-bgs)	Elevation of Top (ft)					LL	PL	PI	LI	USCS	Gravel (%)	Sand (%)	Silt (%)	Clay (%)			c' (psf)	phi' (deg)	UU - c _u (psf)	Confining Pressure (psf)	Type	C _c	C _r	σ _p (psf)	
BH-FGD-102	79	0.0-2.0		SH	20.1	Hard, mottled light brown, sandy lean CLAY (CL), damp																					
BH-FGD-102	80	2.0-4.0		SH	8.3	very stiff, brown at 2.0'																					
BH-FGD-102	81	4.0-6.0		SH	14.1	hard at 4.0'																					
BH-FGD-102	82	6.0-8.0		SH	17.9	light gray, moist at 6.0'																					
BH-FGD-102	83	8.0-10.0		SH	20.0	very stiff at 8.0'																					
BH-FGD-102	89	13.0-15.0		SH	20.7	little silt at 13.0'																					
BH-FGD-102	85	18.0-20.0		SH	25.1	Stiff, light to dark gray, silty fat CLAY (CH), trace sand, moist	54	22	32	0.08																	
BH-FGD-102	86	23.0-25.0		SH	23.3	Stiff, gray, sandy lean CLAY (CL), trace silt, moist																					
BH-FGD-102	87	28.0-30.0		SS	72	26.7 Very dense, light brown, fine, poorly-graded SAND (SP-SM), with clay, wet							0.0	75.2	24.8												
BH-FGD-102		-				BORING TERMINATED AT 30.0'																					



Project: Luminant Pond Stability Geotechnical Investigation
Location: Oak Grove, Texas

SUMMARY OF SOIL DATA AND LABORATORY TEST RESULTS

Borehole Number	Sample Number	Sample		Sample Type	SPT N Value (blows/1 ft)	Moisture Content (%)	Soil Description	Atterberg Limits					Particle Size Analysis				Dry Unit wt (pcf)	Moist Unit wt (pcf)	CU Triaxial		UU Triaxial		Consolidation				Organic Content (%)
		Depth Interval (ft-bgs)	Elevation of Top (ft)					LL	PL	PI	LI	USCS	Gravel (%)	Sand (%)	Silt (%)	Clay (%)			c' (psf)	phi' (deg)	UU - c _u (psf)	Confining Pressure (psf)	Type	C _c	C _r	σ _p (psf)	
BH-FGD-103	66	0.0-2.0		SH	18.9	Very soft to soft, light brown, sandy fat CLAY (CH), trace roots, damp																					
BH-FGD-103	67	2.0-4.0		SH	18.3	stiff at 2.0'																					
BH-FGD-103	68	4.0-6.0		SH	18.8	light brown to dark grayish brown at 4.0'																					
BH-FGD-103	69	6.0-8.0		SH	14.9	hard at 6.0'																					
BH-FGD-103	70	8.0-10.0		SH	15.0	mottled at 8.0'		53	18	36	-0.08						109.6	126.0			4900	1123					
BH-FGD-103	71	13.0-15.0		SH	19.0			63	20	43	-0.02						105.0	125.0			4400	1541					
BH-FGD-103	72	18.0-20.0		SH	22.5	Stiff, brown, silty CLAY (CL-ML), with sand, trace lignite, moist																					
BH-FGD-103	73	23.0-25.0		SH	20.6	stiff to very stiff, mottled, damp at 23.0'																					
BH-FGD-103	74	28.0-30.0		SH	19.0	Stiff, mottled, sandy lean CLAY (CL), damp		38	16	22	0.12						111.6	132.8			5500	3571					
BH-FGD-103		-																									
BH-FGD-103	75	33.0-34.5		SH	16	21.3	Compact, light gray, SILT (ML), with sand, wet							0.0	39.7	60.3											
BH-FGD-103		-					Firm, light gray and brown, silty SAND (SM), wet																				
BH-FGD-103	76	38.0-40.0		SH	16.0	Very stiff, mottled light gray, lean CLAY (CL), trace lignite, trace sand, wet		35	16	20	0.02						111.8	129.7			3200	4435					
BH-FGD-103	77	43.0-45.0		SH	25.7	hard at 43.0'																					
BH-FGD-103	78	48.0-50.0		SH	23.6	interbedded with sand layers at 48.0'																					
BH-FGD-103		-				BORING TERMINATED AT 50.0'																					

SUMMARY OF SOIL DATA AND LABORATORY TEST RESULTS

Borehole Number	Sample Number	Sample		Sample Type	SPT N Value (blows/1 ft)	Moisture Content (%)	Soil Description	Atterberg Limits					Particle Size Analysis				Dry Unit wt (pcf)	Moist Unit wt (pcf)	CU Triaxial		UU Triaxial		Consolidation				Organic Content (%)
		Depth Interval (ft-bgs)	Elevation of Top (ft)					LL	PL	PI	LI	USCS	Gravel (%)	Sand (%)	Silt (%)	Clay (%)			c' (psf)	phi' (deg)	UU - c _u (psf)	Confining Pressure (psf)	Type	C _c	C _r	σ _p (psf)	
BH-FGD-104	57	0.0-2.0		SH	14.7	Very stiff, light brown to dark brown, sandy lean CLAY (CL), damp																					
BH-FGD-104	58	2.0-4.0		SH	21.0	hard, light brown at 2.0'																					
BH-FGD-104	59	4.0-6.0		SH	17.6	mottled to dark brown, trace silt at 4.0'																					
BH-FGD-104	60	6.0-8.0		SH	13.3	grayish brown at 6.0'																					
BH-FGD-104	61	8.0-10.0		SH	15.6																						
BH-FGD-104	62	13.0-15.0		SH	18.6	very stiff, moist at 13.0'																					
BH-FGD-104	63	18.0-20.0		SH	15.2	hard, damp at 18.0'																					
BH-FGD-104	-					Very dense, grayish brown, medium to fine, silty clayey SAND (SC/SM), trace organic																					
BH-FGD-104	64	23.0-24.5		SS	23	23.4	Compact, light brown and gray, poorly-graded SAND (SP-SM), with silt, wet						0.0	83.8	16.2												
BH-FGD-104	65	28.0-30.0		SS	31	23.7	Fine, silty SAND (SM), trace clay																				
BH-FGD-104	-					BORING TERMINATED AT 30.0'																					



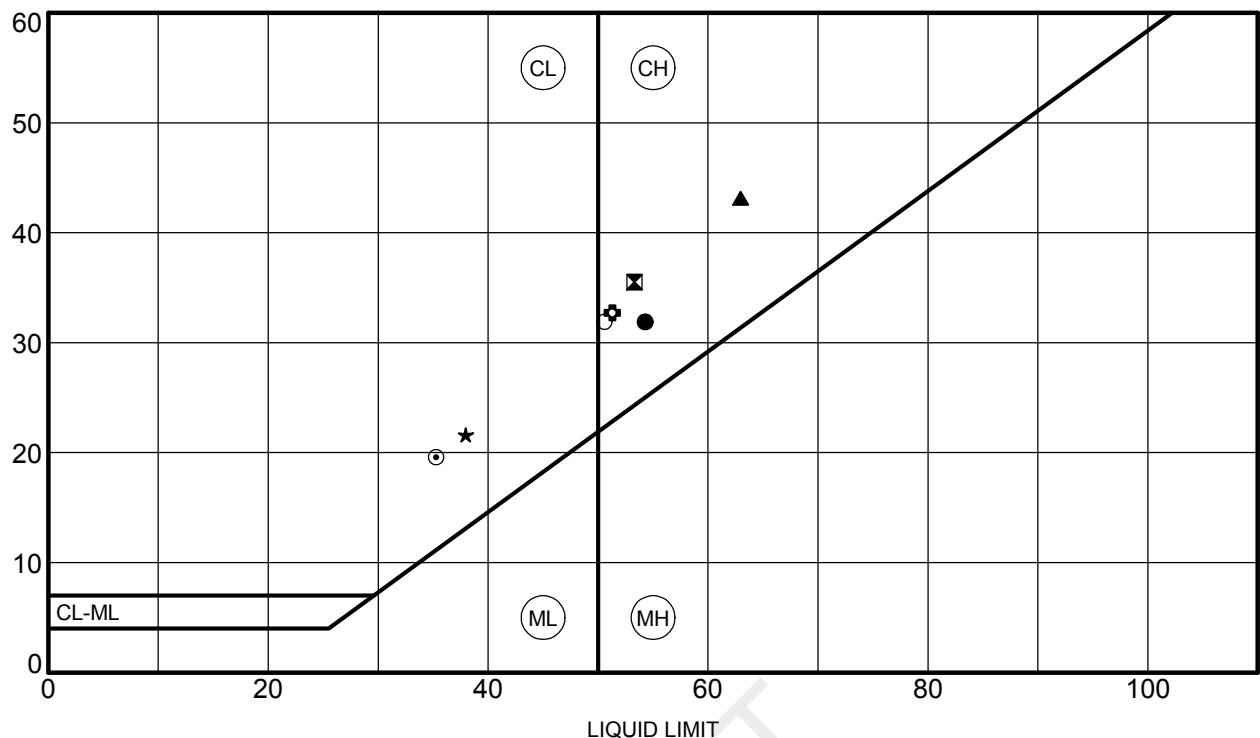
Project: Luminant Pond Stability Geotechnical Investigation
Location: Oak Grove, Texas

SUMMARY OF SOIL DATA AND LABORATORY TEST RESULTS

Borehole Number	Sample Number	Sample		Sample Type	SPT N Value (blows/1 ft)	Moisture Content (%)	Soil Description	Atterberg Limits					Particle Size Analysis				Dry Unit wt (pcf)	Moist Unit wt (pcf)	CU Triaxial		UU Triaxial		Consolidation				Organic Content (%)
		Depth Interval (ft-bgs)	Elevation of Top (ft)					LL	PL	PI	LI	USCS	Gravel (%)	Sand (%)	Silt (%)	Clay (%)			c' (psf)	phi' (deg)	UU - c _u (psf)	Confining Pressure (psf)	Type	C _c	C _r	σ _p (psf)	
BH-FGD-105	44	0.0-2.0		SH	8.3	Very stiff, mottled dark brown, sandy fat CLAY (CH), trace organics, damp																					
BH-FGD-105	45	2.0-4.0		SH	19.3	hard, light brown at 2.0'																					
BH-FGD-105	46	4.0-6.0		SH	13.5	dark brown at 4.0'																					
BH-FGD-105	47	6.0-8.0		SH	10.3	light brown at 6.0'																					
BH-FGD-105	48	8.0-10.0		SH	16.3			51	19	33	-0.07	CH	0.0	12.3	87.7			278	26								
BH-FGD-105	49	13.0-15.0		SH	16.0	mottled, trace lignite at 13.0'																					
BH-FGD-105	50	18.0-20.0		SH	18.0	very stiff, dark gray at 18.0'		51	19	32	-0.02						107.9	127.3			4300	2434					
BH-FGD-105	51	23.0-25.0		SH	15.9	hard, dark brown at 23.0'																					
BH-FGD-105	52	28.0-30.0		SH	18.9	Very stiff, mottled dark gray to brown, silty CLAY (CL-ML), few sand, moist																					
BH-FGD-105		-																									
BH-FGD-105	53	33.0-35.0		SH	22.3	Stiff, black, sandy SILT (ML), trace clay, some organics, some wood fragments, moist																					
BH-FGD-105		-				Stiff, dark brown, fat CLAY (CH), trace organics, trace sand, moist																					
BH-FGD-105	54	38.0-39.5		SS	50	12.5	Very dense, light brown, fine, poorly-graded SAND (SP), trace clay, damp							1.2	62.0	36.8											
BH-FGD-105	55	43.0-45.0		SS	72	23.6	Very dense, light brown, fine, poorly-graded SAND (SP-SM), with silt, moist							0.0	78.8	21.2											
BH-FGD-105	56	48.0-50.0		SS	50	26.4	Very dense, grayish brown, silty SAND (SM), trace clay, moist							0.0	74.6	25.4											
BH-FGD-105		-				BORING TERMINATED AT 50.0'																					

SUMMARY OF SOIL DATA AND LABORATORY TEST RESULTS

Borehole Number	Sample Number	Sample		Sample Type	SPT N Value (blows/ 1 ft)	Moisture Content (%)	Soil Description	Atterberg Limits					Particle Size Analysis				Dry Unit wt (pcf)	Moist Unit wt (pcf)	CU Triaxial		UU Triaxial		Consolidation				Organic Content (%)
		Depth Interval (ft-bgs)	Elevation of Top (ft)					LL	PL	PI	LI	USCS	Gravel (%)	Sand (%)	Silt (%)	Clay (%)			c' (psf)	phi' (deg)	UU - c _u (psf)	Confining Pressure (psf)	Type	C _c	C _r	σ _p (psf)	
BH-FGD-106	97	0.0-2.0		SH	21.3	Stiff, mottled dark gray, sandy lean CLAY (CL), trace silt, damp																					
BH-FGD-106	98	2.0-4.0		SH	23.8	light brown to dark brown at 2.0'																					
BH-FGD-106	99	4.0-6.0		SH	18.8	hard, brownish red, moist at 4.0'																					
BH-FGD-106	100	6.0-8.0		SH	13.1	damp at 6.0'																					
BH-FGD-106	101	8.0-10.0		SH	17.8	mottled brownish red at 8.0'																					
BH-FGD-106	102	13.0-15.0		SH	17.4	mottled gray, little silt at 13.0'																					
BH-FGD-106	103	18.0-20.0		SH	16.7																						
BH-FGD-106	104	23.0-25.0		SH	22.8	Compact, light gray, fine silty SAND (SM), moist							0.0	64.6	35.4												
BH-FGD-106	105	28.0-30.0		SS	27	28.0 wet at 28.0'																					
BH-FGD-106		-				BORING TERMINATED AT 30.0'																					

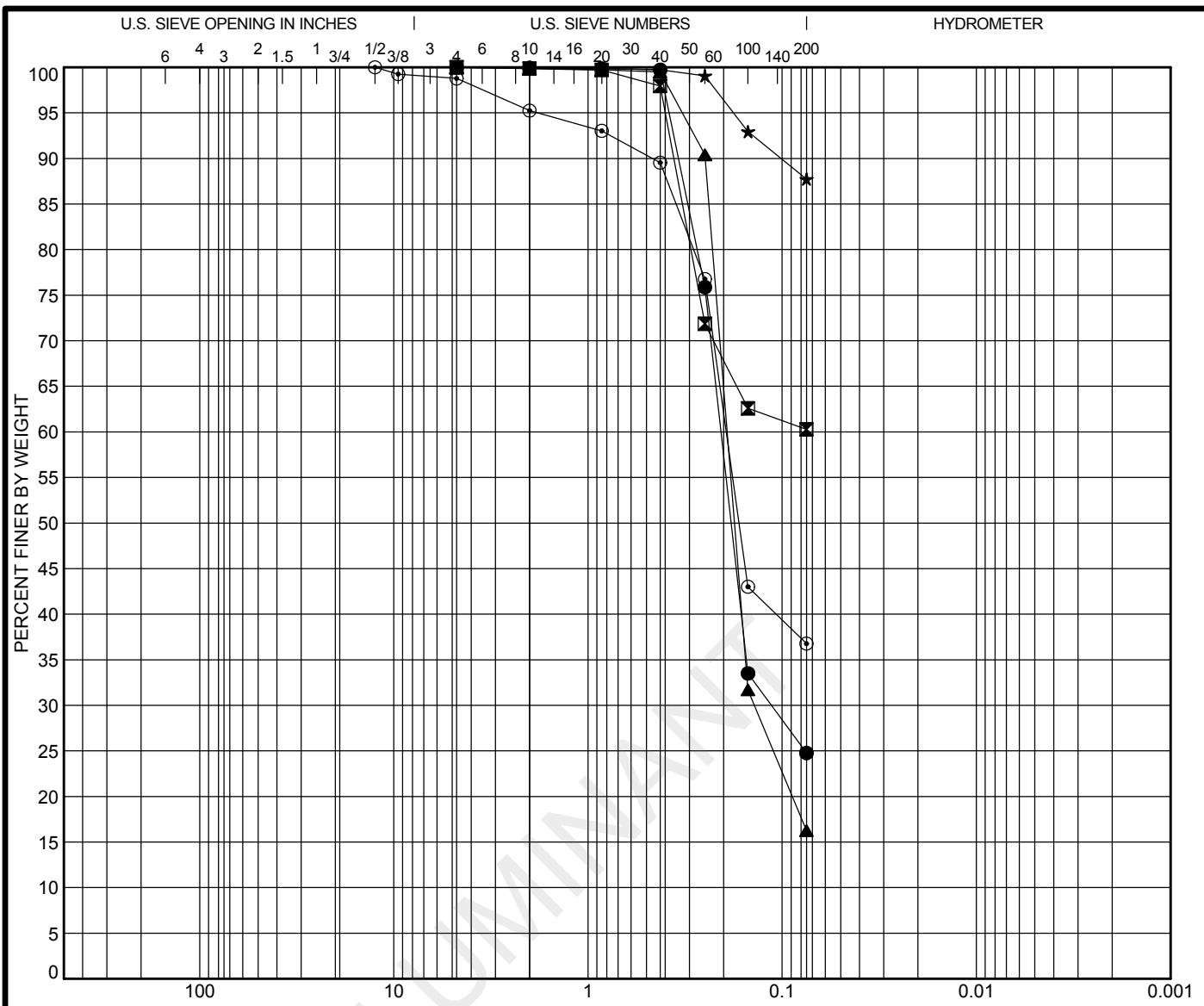


CAN ATTERBERG LIMITS 94563GINT.GPJ GLDR LDN.GDT 4/23/10



ATTERBERG LIMITS' RESULTS

Project: Luminant Pond Stability Geotechnical Investigation
Location: Oak Grove, Texas



COBBLES	GRAVEL		SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine				

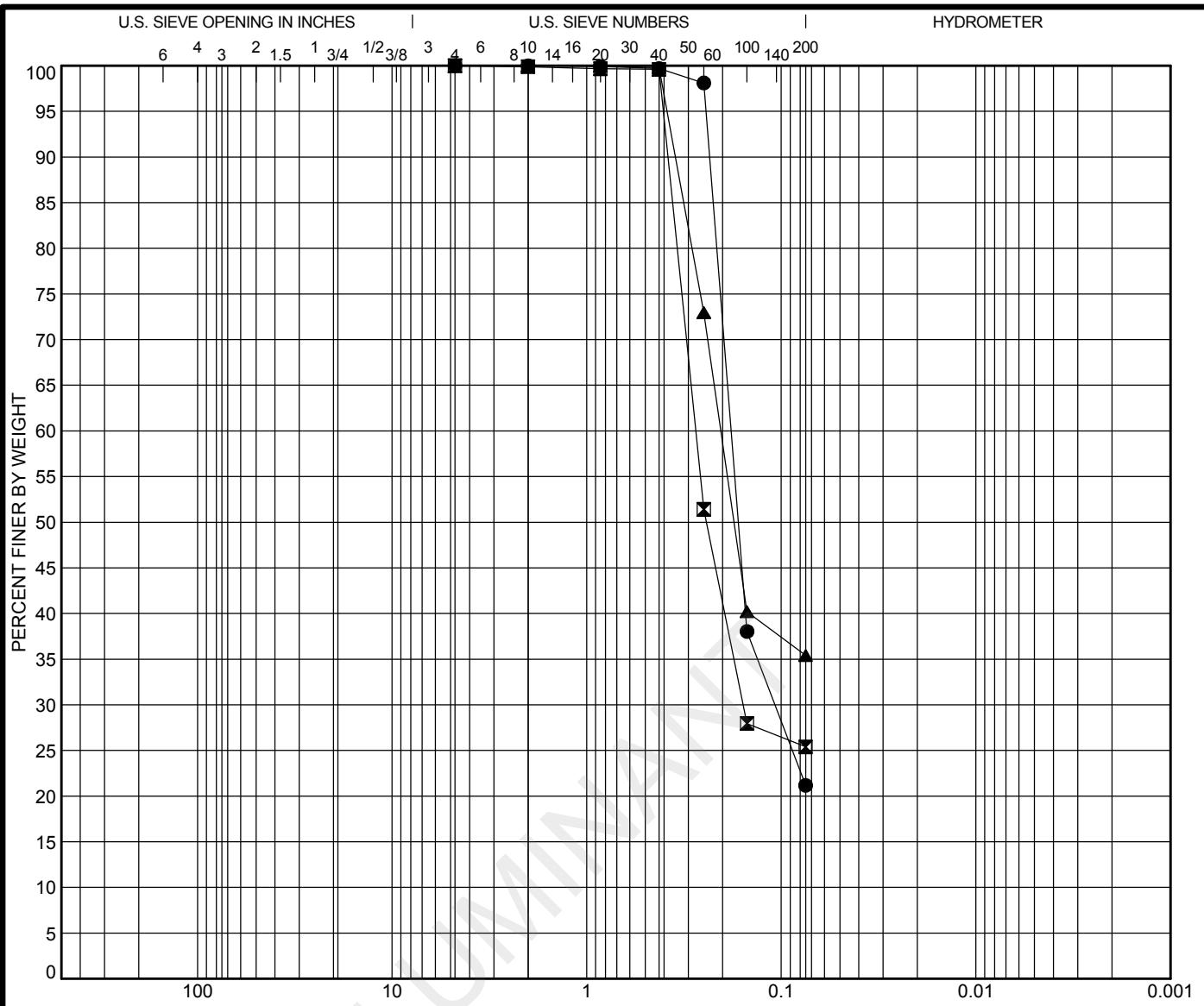
Specimen Identification	Classification					LL	PL	PI	Cc	Cu
● BH-FGD-102 28.00ft										
☒ BH-FGD-103 33.00ft										
▲ BH-FGD-104 23.00ft										
★ BH-FGD-105 8.00ft	FAT CLAY(CH)					51	19	32		
○ BH-FGD-105 38.00ft										
Specimen Identification	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● BH-FGD-102 28.00 ft	4.75	0.206	0.114		0.00	75.23	24.77			
☒ BH-FGD-103 33.00 ft	4.75				0.00	39.73	60.27			
▲ BH-FGD-104 23.00 ft	4.75	0.192	0.139		0.00	83.76	16.24			
★ BH-FGD-105 8.00 ft	4.75				0.00	12.26	87.74			
○ BH-FGD-105 38.00 ft	12.5	0.194			1.23	62.00	36.77			

CAN GRAIN SIZE 94563GINT.GPJ GLDR LDNGDT 4/27/10



GRAIN SIZE DISTRIBUTION

Project: Luminant Pond Stability Geotechnical
Investigation
Location: Oak Grove, Texas



COBBLES	GRAVEL		SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine				
● BH-FGD-105 43.00ft									
☒ BH-FGD-105 48.00ft									
▲ BH-FGD-106 23.00ft									

Specimen Identification	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● BH-FGD-105 43.00 ft	4.75	0.181	0.108		0.00	78.83	21.17	
☒ BH-FGD-105 48.00 ft	4.75	0.275	0.157		0.00	74.61	25.39	
▲ BH-FGD-106 23.00 ft	2	0.204			0.00	64.60	35.40	



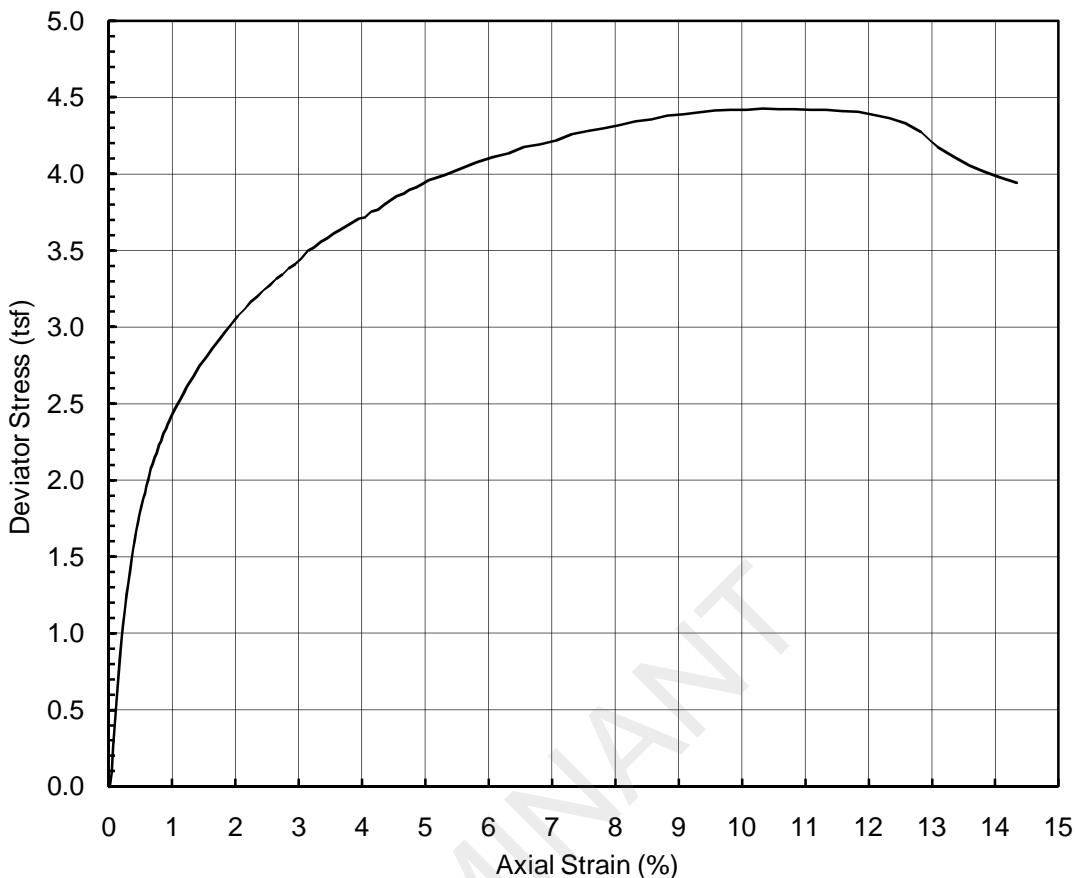
GRAIN SIZE DISTRIBUTION

Project: Luminant Pond Stability Geotechnical

Investigation

Location: Oak Grove, Texas

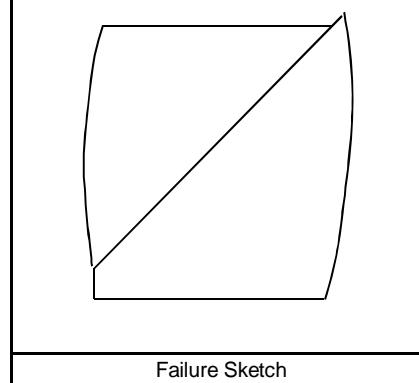
UNCONSOLIDATED / UNDRAINED COMPRESSIVE STRENGTH
ASTM D 2850



Specimen Description	Reddish Brown Sandy Clay						
LL	63	PI	43	LI	0.0	USCS	CH

Depth (ft)	13.0	Confining Pressure (psi)	10.7
Specimen Height (inch)	5.5	Strain Rate (%/min)	1.0
Specimen Diameter (inch)	2.8	Peak Deviator Stress (tsf)	4.4
Initial Specimen Weight (g)	1113.5	Axial Strain at Peak Stress (%)	10.3
Moist Unit Weight (pcf)	125.0		
Initial Water Content (%)	19		
	Initial Dry Unit Weight (pcf)	104.8	

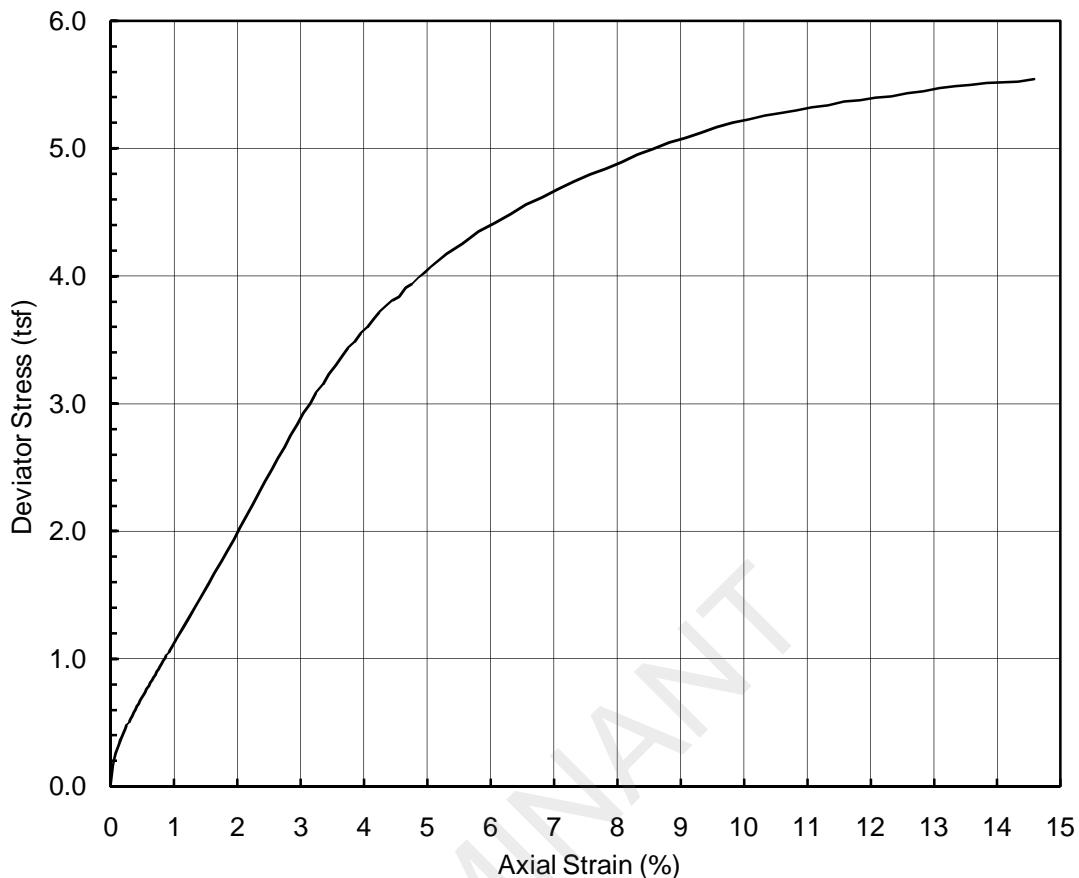
Project Title	Luminant Pond Stability	
Project Number	103-94563	
Sample Type	Shelby Tube	
Sample ID	FGD-103	SA-71
Comments		



Failure Sketch

Performed by	PN
Date	27-Mar-10
Check	DM
Review	PCM

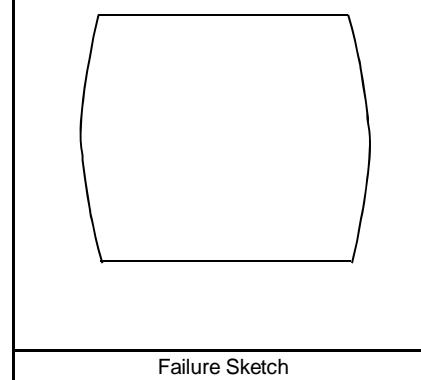
UNCONSOLIDATED / UNDRAINED COMPRESSIVE STRENGTH
ASTM D 2850



Specimen Description	Light brown Sandy Clay						
LL	38	PI	22	LI	0.1	USCS	CL

Depth (ft)	28.0	Confining Pressure (psi)	24.8
Specimen Height (inch)	5.6	Strain Rate (%/min)	1.0
Specimen Diameter (inch)	2.8	Peak Deviator Stress (tsf)	5.5
Initial Specimen Weight (g)	1225.2	Axial Strain at Peak Stress (%)	14.8
Moist Unit Weight (pcf)	132.8		
Initial Water Content (%)	19		
	Initial Dry Unit Weight (pcf)	111.8	

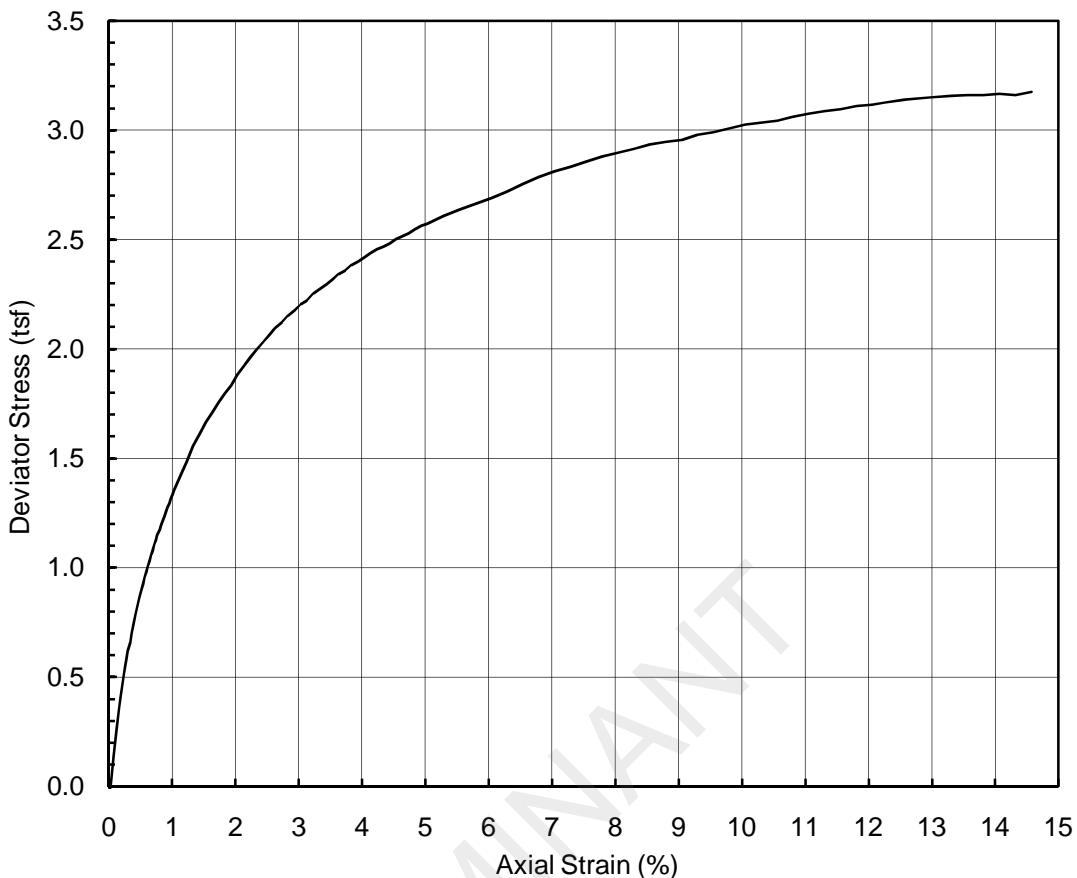
Project Title	Luminant Pond Stability	
Project Number	103-94563	
Sample Type	Shelby Tube	
Sample ID	FGD-103	SA-74
Comments		



Failure Sketch

Performed by	PN
Date	29-Mar-10
Check	DM
Review	PCM

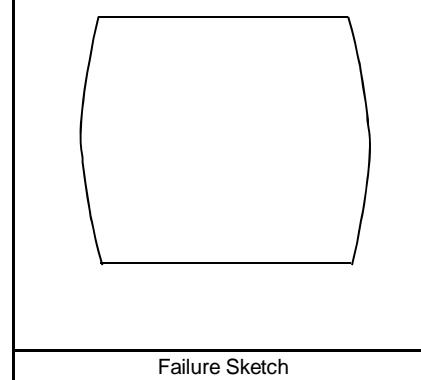
UNCONSOLIDATED / UNDRAINED COMPRESSIVE STRENGTH
ASTM D 2850



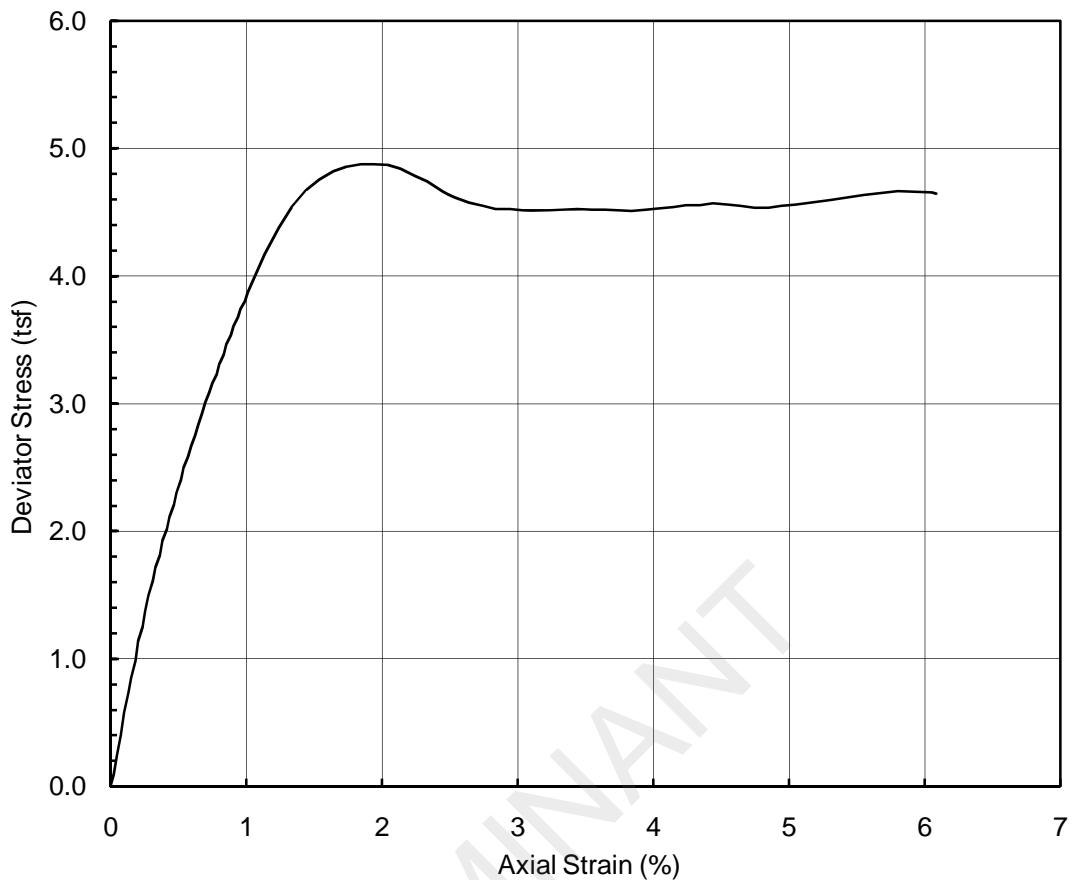
Specimen Description	Light gray Sandy Clay						
LL	35	PI	19	LI	0.0	USCS	CL

Depth (ft)	38.0	Confining Pressure (psi)	30.8
Specimen Height (inch)	5.5	Strain Rate (%/min)	1.0
Specimen Diameter (inch)	2.8	Peak Deviator Stress (tsf)	3.2
Initial Specimen Weight (g)	1131.4	Axial Strain at Peak Stress (%)	15.0
Moist Unit Weight (pcf)	129.7		
Initial Water Content (%)	16		
	Initial Dry Unit Weight (pcf)	111.8	

Project Title	Luminant Pond Stability	
Project Number	103-94563	
Sample Type	Shelby Tube	
Sample ID	FGD-103	SA-76
Comments		



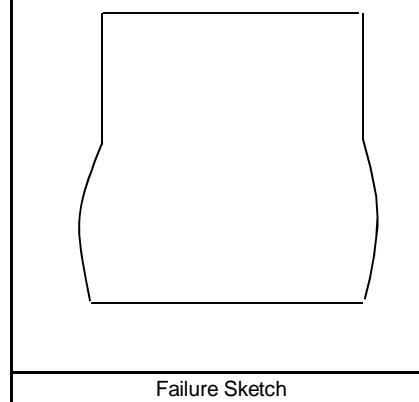
UNCONSOLIDATED / UNDRAINED COMPRESSIVE STRENGTH
ASTM D 2850



Specimen Description	Yellowish Brown Sandy Clay						
LL	53	PI	35	LI	-0.1	USCS	CH

Depth (ft)	8.0	Confining Pressure (psi)	7.8
Specimen Height (inch)	5.6	Strain Rate (%/min)	1.0
Specimen Diameter (inch)	2.8	Peak Deviator Stress (tsf)	4.9
Initial Specimen Weight (g)	1108.3	Axial Strain at Peak Stress (%)	1.9
Moist Unit Weight (pcf)	126.0		
Initial Water Content (%)	15		
	Initial Dry Unit Weight (pcf)	109.2	

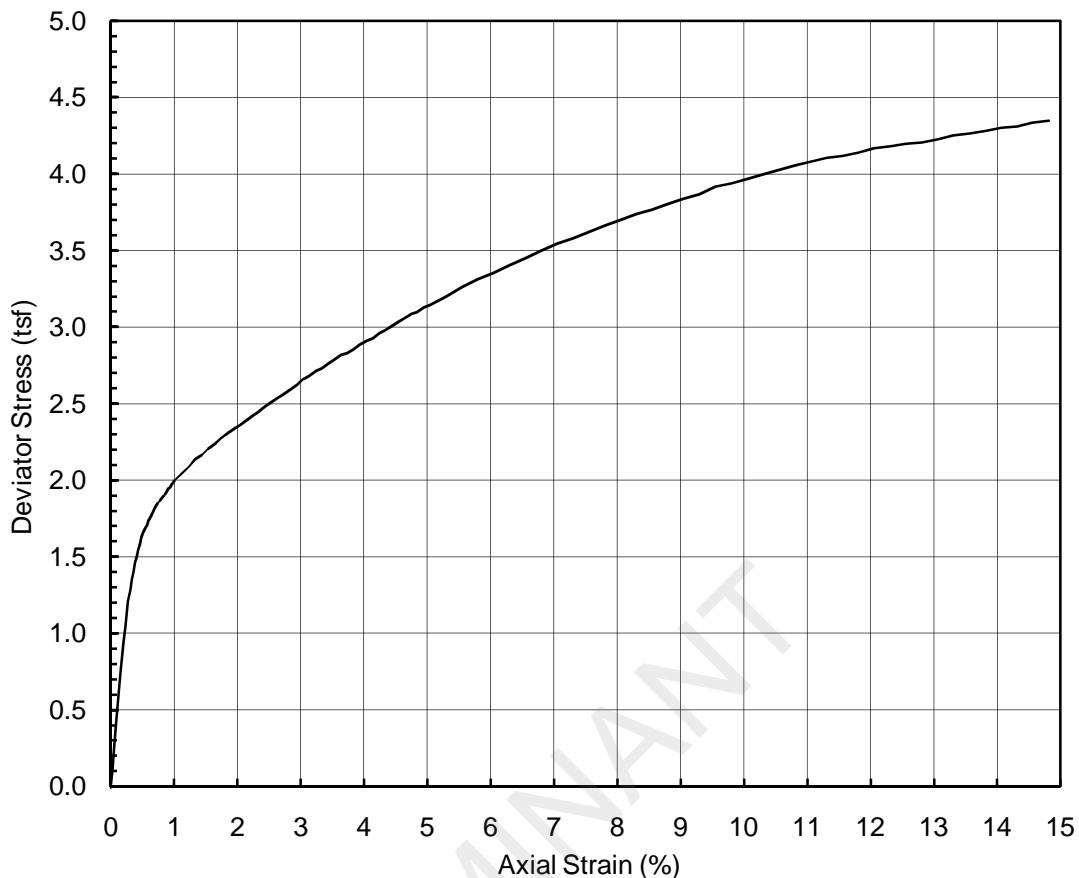
Project Title	Luminant Pond Stability	
Project Number	103-94563	
Sample Type	Shelby Tube	
Sample ID	FGD-103	SA-70
Comments		



Failure Sketch

Performed by	PN
Date	27-Mar-10
Check	DM
Review	PCM

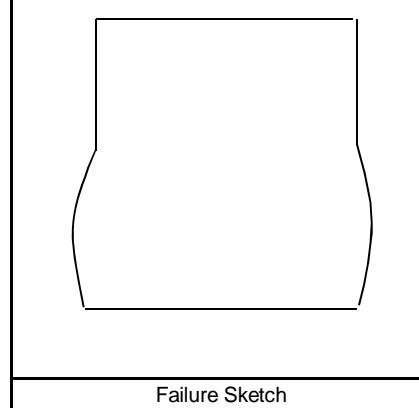
UNCONSOLIDATED / UNDRAINED COMPRESSIVE STRENGTH
ASTM D 2850



Specimen Description	Brown Sandy Clay						
LL	51	PI	32	LI	0.0	USCS	CH

Depth (ft)	18.0	Confining Pressure (psi)	16.9
Specimen Height (inch)	5.0	Strain Rate (%/min)	1.0
Specimen Diameter (inch)	2.8	Peak Deviator Stress (tsf)	4.3
Initial Specimen Weight (g)	1035.2	Axial Strain at Peak Stress (%)	15.0
Moist Unit Weight (pcf)	127.3		
Initial Water Content (%)	18		
	Initial Dry Unit Weight (pcf)	107.9	

Project Title	Luminant Pond Stability	
Project Number	103-94563	
Sample Type	Shelby Tube	
Sample ID	FGD-105	SA-50
Comments		



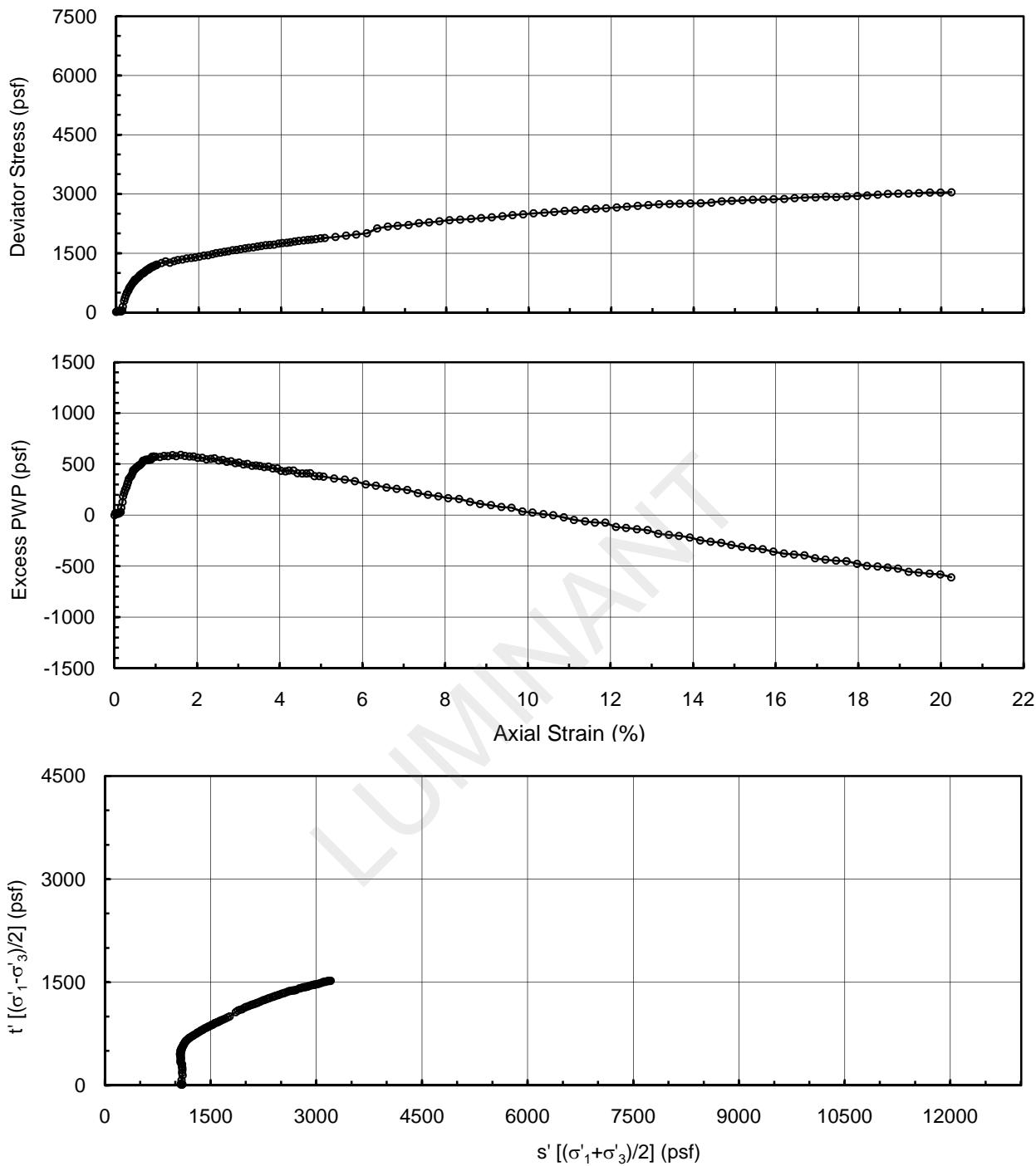
Performed by	PN
Date	27-Mar-10
Check	DM
Review	SBK

Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 08-Apr-10
Depth (ft): 8.9



Specimen Description: Light Brown Fat CLAY

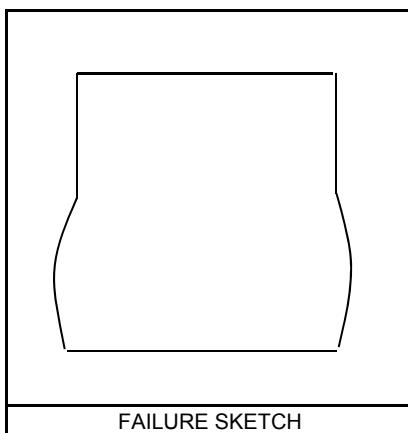
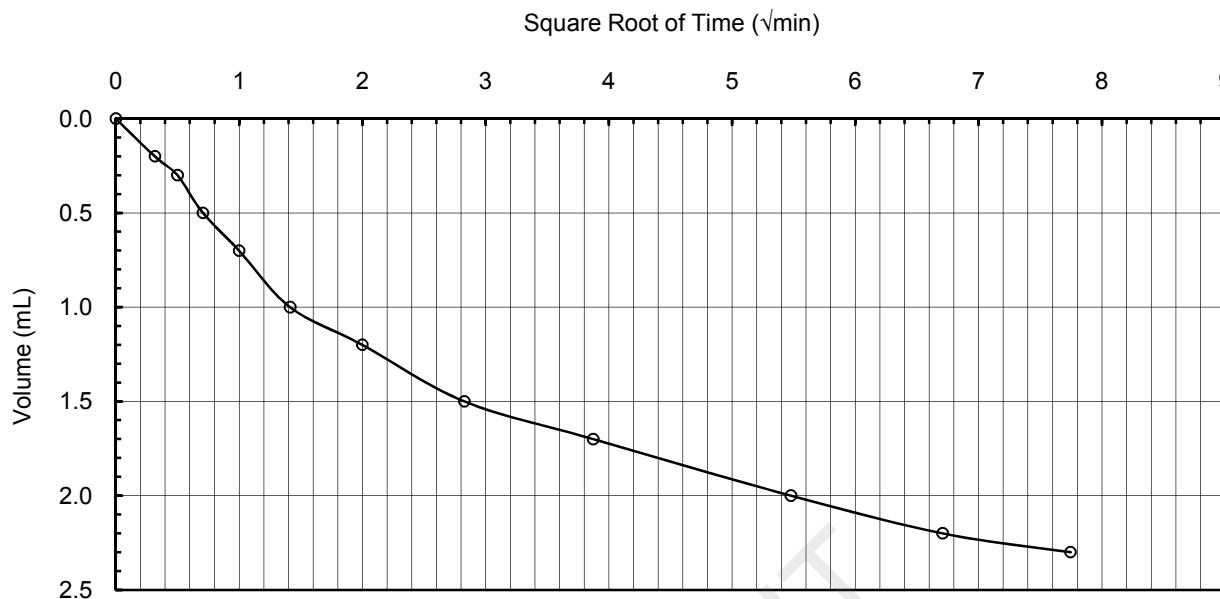
Initial Specimen Diameter (inch) =	2.94	Initial Specimen Height (inch) =	5.29
Initial Water Content (%) =	15.5	Water Content at End of Test (%) =	22.4
Initial Moist Unit Weight (pcf) =	121.8	B-value =	0.95
Back Pressure (BP, psf) =	10800	Consolidation Stress (σ'_3 , psf) =	1088
Initial Lateral Stress (σ'_3 , psf) =	1088	Consolidation t_{50} (min) =	3
Initial Deviator Stress ($\sigma_1 - \sigma_3$, psf) =	16	Rebound Stress (σ'_3 , psf) =	NA
Test Strain Rate (%/hour) =	1.0	Rebound t_{50} (min) =	NA
LL =	51	PI =	32
Comments:	USCS CH		Performed by DM
			Reviewed by PCM

Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 08-Apr-10
Depth (ft): 8.9



Consolidation Stress (σ'_3 , psf) =	1088		
Consolidation t_{50} (min) =	3		
Consolidation Volume Change (mL) =	2.3		
Unloading Stress (psf) =	NA		
Unloading t_{50} (min) =	NA		
Unloading Volume Change (mL) =	NA		
LL =	51	PI =	32
USCS	CH		
Gs =	2.65	assumed	

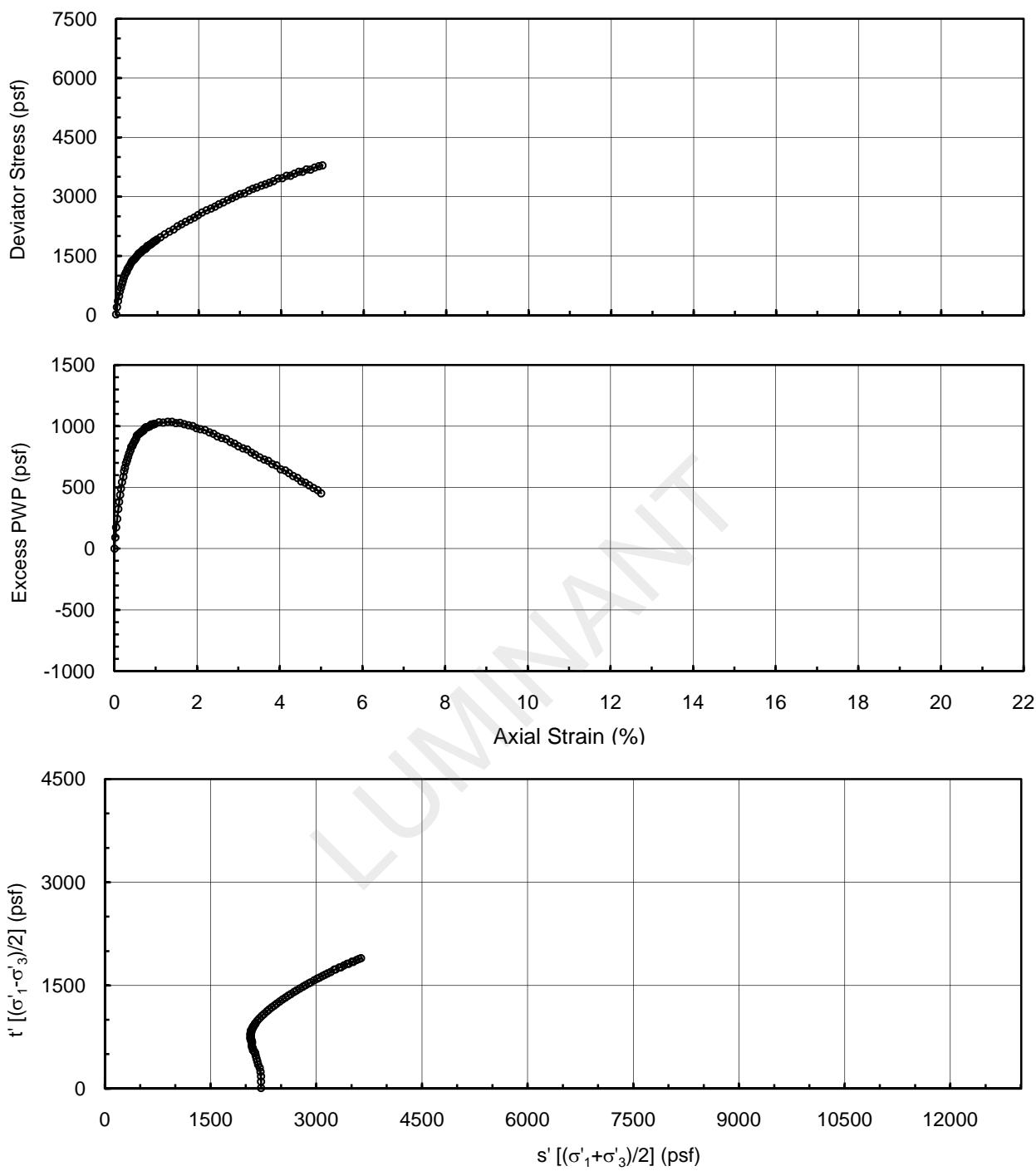
Performed by	DM
Reviewed by	PCM

Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 09-Apr-10
Depth (ft): 8.0



Specimen Description: Light Brown Fat CLAY

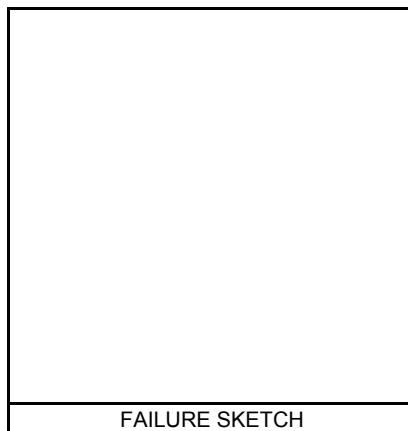
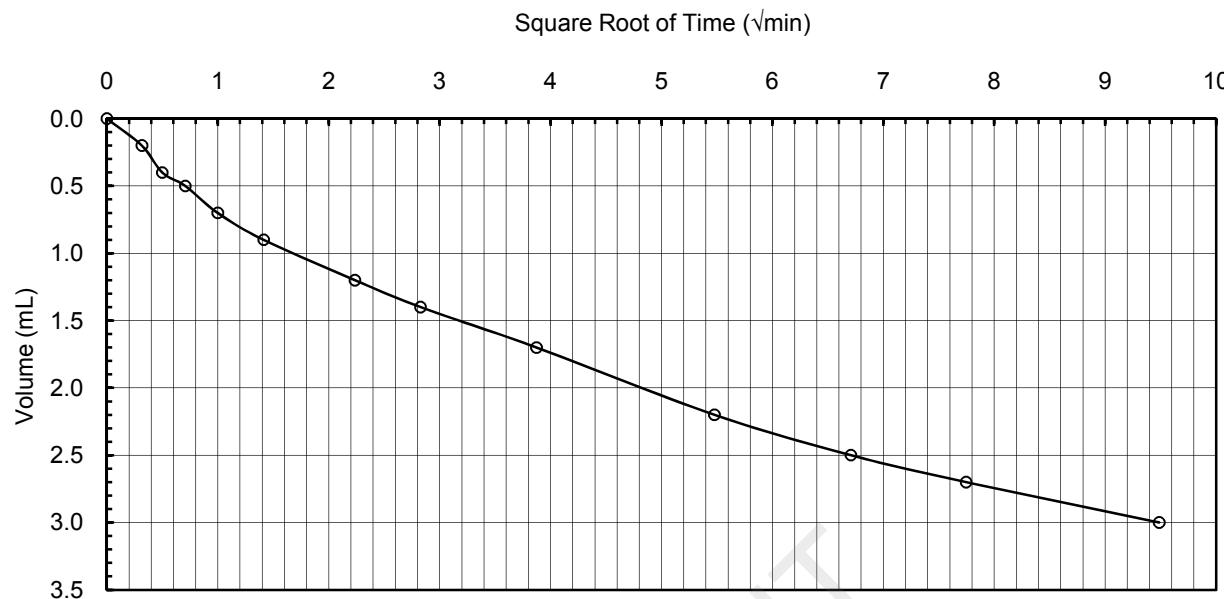
Initial Specimen Diameter (inch) =	2.94	Initial Specimen Height (inch) =	5.56
Initial Water Content (%) =	16.3	Water Content at End of Test (%) =	-
Initial Moist Unit Weight (pcf) =	123.6	B-value =	0.95
Back Pressure (BP, psf) =	9360	Consolidation Stress (σ_3 , psf) =	2209
Initial Lateral Stress (σ_3 , psf) =	2209	Consolidation t_{50} (min) =	17
Initial Deviator Stress ($\sigma_1 - \sigma_3$, psf) =	18	Rebound Stress (σ_3 , psf) =	NA
Test Strain Rate (%/hour) =	1.0	Rebound t_{50} (min) =	NA
LL =	51	PI =	32
Comments: Specimen #2 - Stage 1	USCS		Performed by
	CH		Reviewed by
			PCM

Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 09-Apr-10
Depth (ft): 8.0



Consolidation Stress (σ'_3 , psf) =	2209		
Consolidation t_{50} (min) =	17		
Consolidation Volume Change (mL) =	3.0		
Unloading Stress (psf) =	NA		
Unloading t_{50} (min) =	NA		
Unloading Volume Change (mL) =	NA		
LL =	51	PI =	32
USCS	CH		
Gs =	2.65	assumed	

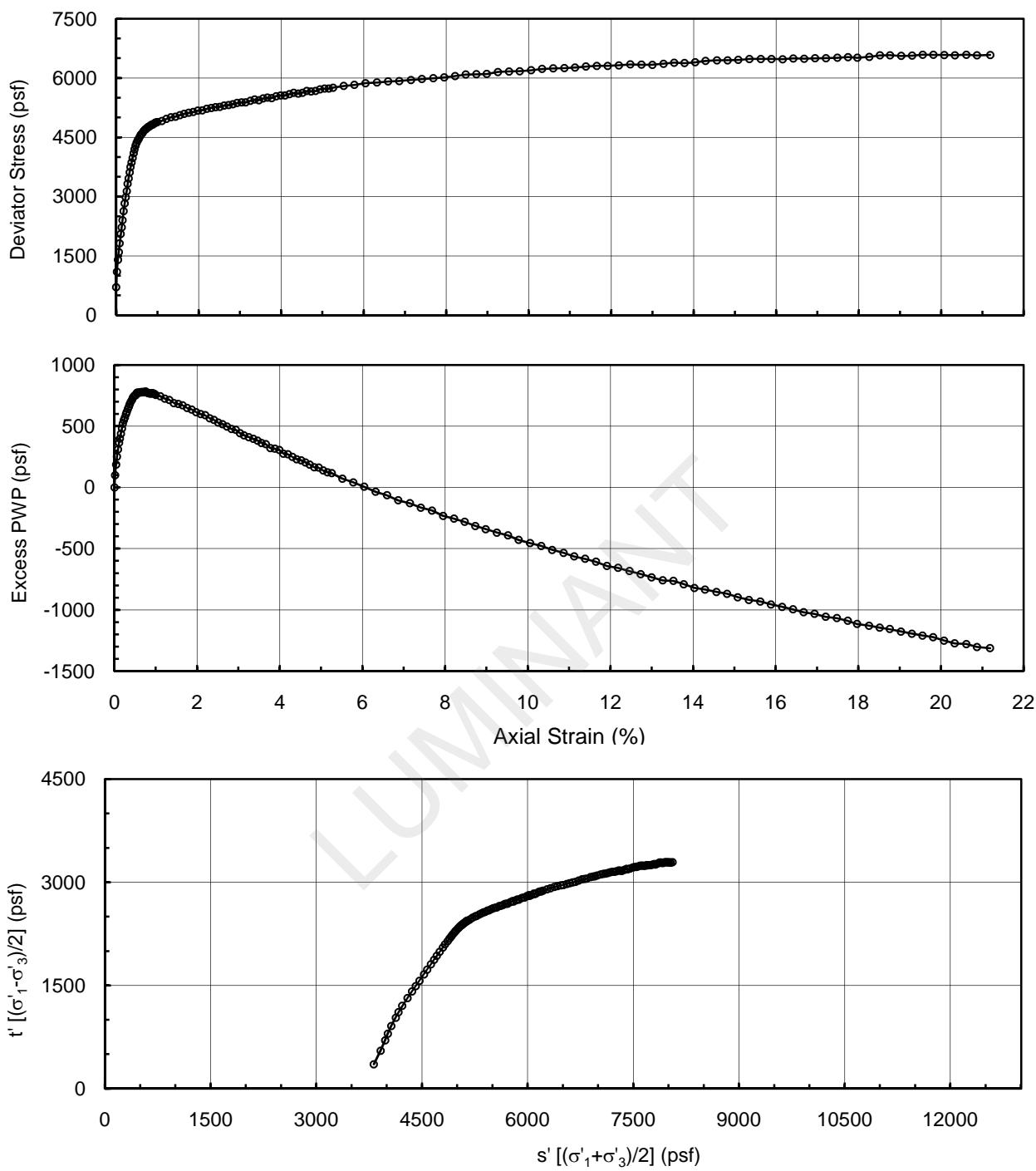
Performed by	DM
Reviewed by	PCM

Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 10-Apr-10
Depth (ft): 8.0



Specimen Description: Light Brown Fat CLAY

Initial Specimen Diameter (inch) =	3.00	Initial Specimen Height (inch) =	5.28
Initial Water Content (%) =	-	Water Content at End of Test (%) =	21.2
Initial Moist Unit Weight (pcf) =	-	B-value =	-
Back Pressure (BP, psf) =	9360	Consolidation Stress (σ_3' , psf) =	3463
Initial Lateral Stress (σ_3' , psf) =	3463	Consolidation t_{50} (min) =	6
Initial Deviator Stress ($\sigma_1 - \sigma_3$, psf) =	708	Rebound Stress (σ_3' , psf) =	NA
Test Strain Rate (%/hour) =	1.0	Rebound t_{50} (min) =	NA
LL =	51	PI =	32
Comments: Specimen #2 - Stage 2		USCS	CH
			Performed by
			Reviewed by

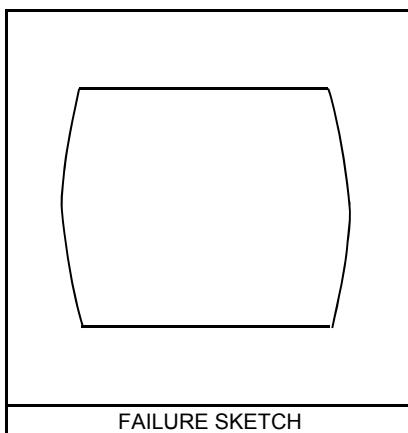
Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 10-Apr-10
Depth (ft): 8.0

Square Root of Time ($\sqrt{\text{min}}$)



Consolidation Stress (σ'_3 , psf) =	3463		
Consolidation t_{50} (min) =	6		
Consolidation Volume Change (mL) =	5.4		
Unloading Stress (psf) =	NA		
Unloading t_{50} (min) =	NA		
Unloading Volume Change (mL) =	NA		
LL =	51	PI =	32
USCS	CH		
Gs =	2.65	assumed	

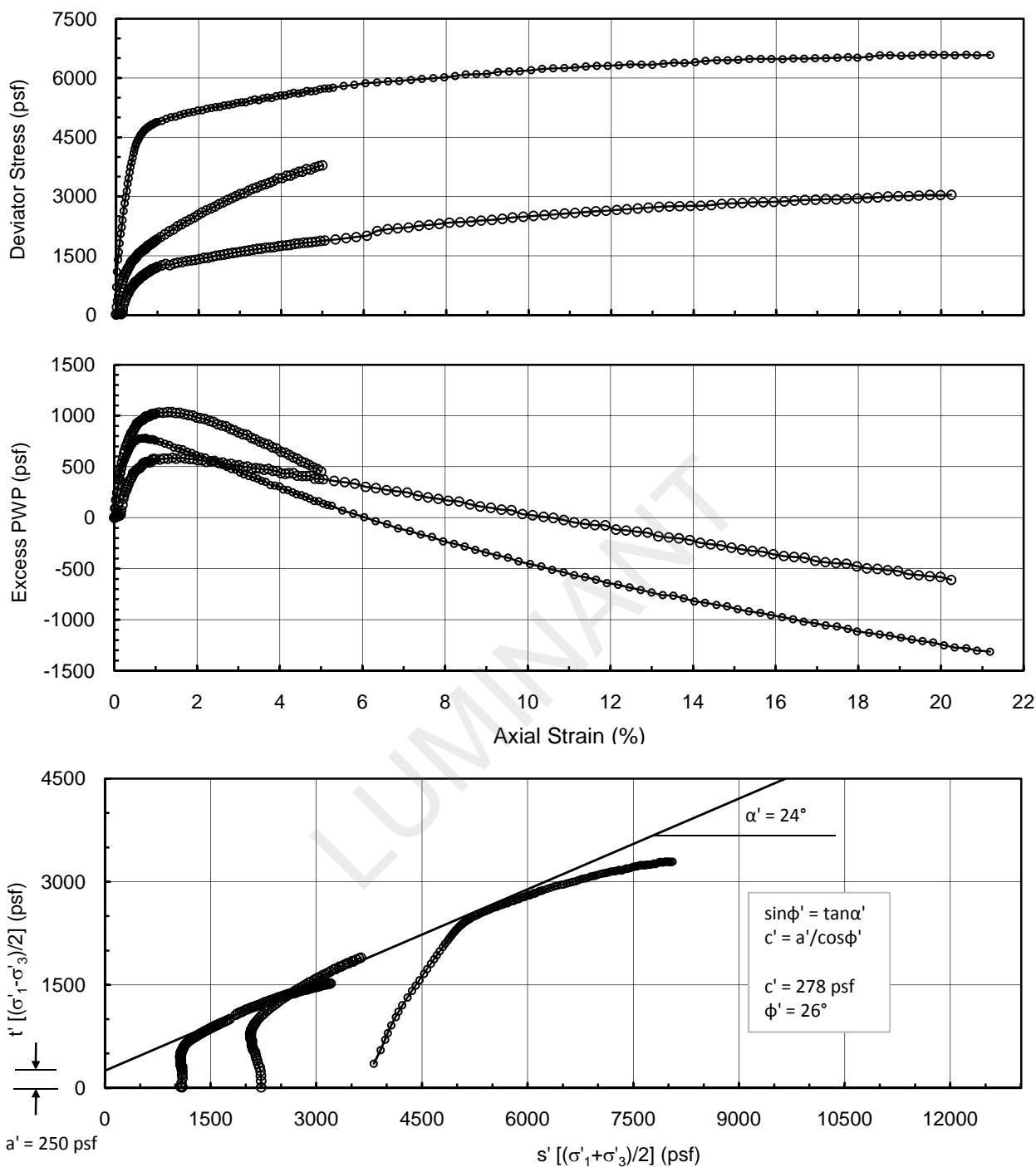
Performed by	DM
Reviewed by	PCM

Isotropically Consolidated Undrained Triaxial Test (ICU)

Project Title: Luminant Pond
Boring Number: FGD-105

Project Number: 103-94563
Specimen Name: SA-48

Date: 10-Apr-10
Depth (ft):



Specimen Description: Light Brown Fat CLAY

Initial Specimen Diameter (inch) =		Initial Specimen Height (inch) =	
Initial Water Content (%) =		Water Content at End of Test (%) =	
Initial Moist Unit Weight (pcf) =		B-value =	
Back Pressure (BP, psf) =		Consolidation Stress (σ'_3 , psf) =	
Initial Lateral Stress (σ'_3 , psf) =		Consolidation t_{50} (min) =	
Initial Deviator Stress ($\sigma_1 - \sigma_3$, psf) =		Rebound Stress (σ'_3 , psf) =	
Test Strain Rate (%/hour) =		Rebound t_{50} (min) =	
LL =	51	PI =	32 USCS CH
Comments:	3 Stages on 2 Specimens	Performed by	DM
		Reviewed by	PCM



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Fax: (281) 821-6870

SUMMARY OF LABORATORY RESULTS

PAGE 1 OF 1

CLIENT Luminant Power

PROJECT NAME Luminant

PROJECT NUMBER 1406296

PROJECT LOCATION Oak Grove SES

Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)	Saturation (%)	Specific Gravity
CELL 4 SF-01	0.0	45	14	31	9.5	58	CL	17.8			
FGD-10	4.0				4.75	82		14.8			
FGD-10	26.0				4.75	33		28.0			
FGD-10	32.0	46	20	26	4.75	77	CL	21.5			
FGD-11	4.0	52	17	35	4.75	93	CH	20.6			
FGD-11	22.0				4.75	15		8.2			
FGD-11	40.0				4.75	24		34.5			
FGD-12	28.0				4.75	20		22.8			
FGD-C-01	4.0	52	17	35	4.75	78	CH	11.5			
FGD-C-01	12.0	39	20	19	4.75	77	CL	8.6			
FGD-C-02	10.0	51	17	34	9.5	90	CH	15.1			
FGD-C-02	36.0				4.75	60		28.3			
FGD-C-03	4.0	39	20	19	4.75	67	CL	8.5			
FGD-C-03	8.0	41	21	20	4.75	89	CL	9.0			
FGD-C-03	36.0	36	24	12	4.75	51	CL	26.1			
FGD-C-04	4.0	46	15	31	4.75	49	SC	6.6			
FGD-C-04	10.0	68	21	47	4.75	61	CH	16.2			
FGD-C-04	40.0	36	16	20	4.75	68	CL	18.5			
FGD-C-05	2.0	56	17	39	4.75	84	CH	22.5			
FGD-C-05	32.0	34	19	15	9.5	28	SC	29.9			
FGD-C-06	16.0	41	15	26	9.5	66	CL	11.4			
FGD-C-06	24.0				4.75	29		5.1			
FGD-C-07	14.0	45	15	30	9.5	74	CL	12.3			
FGD-C-07	36.0	NP	NP	NP	4.75	30	SM	24.1			
FGD-C-08	4.0	37	17	20	9.5	59	CL	13.4			
FGD-C-08	16.0	31	16	15	9.5	45	SC	8.3			
FGD-C-09	12.0	39	15	24	4.75	62	CL	11.6			
FGD-C-10	0.0	41	19	22	9.5	79	CL	19.8			
FGD-C-10	2.0	42	18	24	9.5	73	CL	13.4			
FGD-C-10	4.0	41	17	24	4.75	67	CL	13.9			

APPENDIX C
SLOPE STABILITY ANALYSIS RESULTS

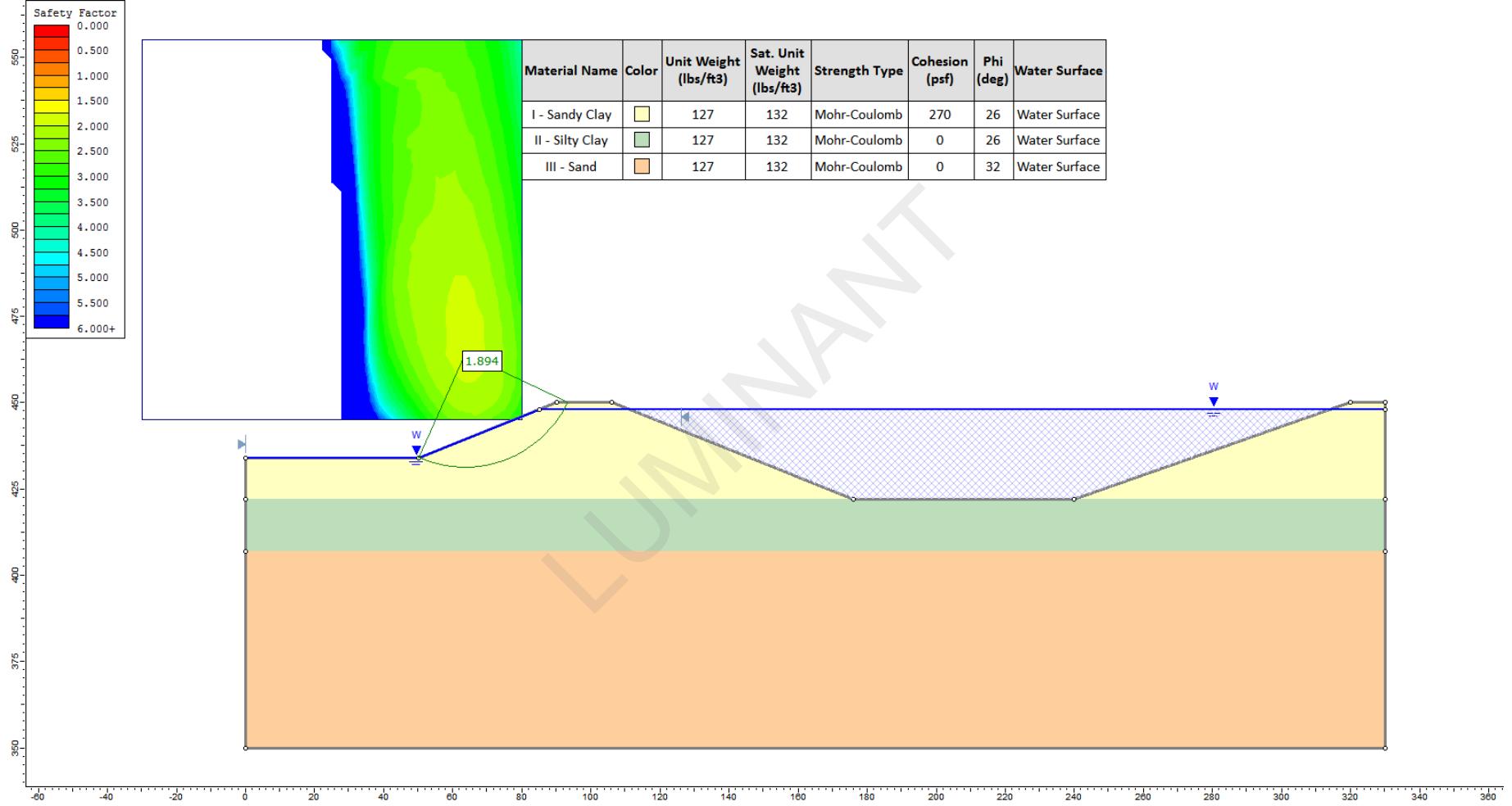


FIGURE C.1
Results of Stability Analysis – FGD-A: A-A' – Case 1a
 Stability and Safety Factor Assessment, Oak Grove SES

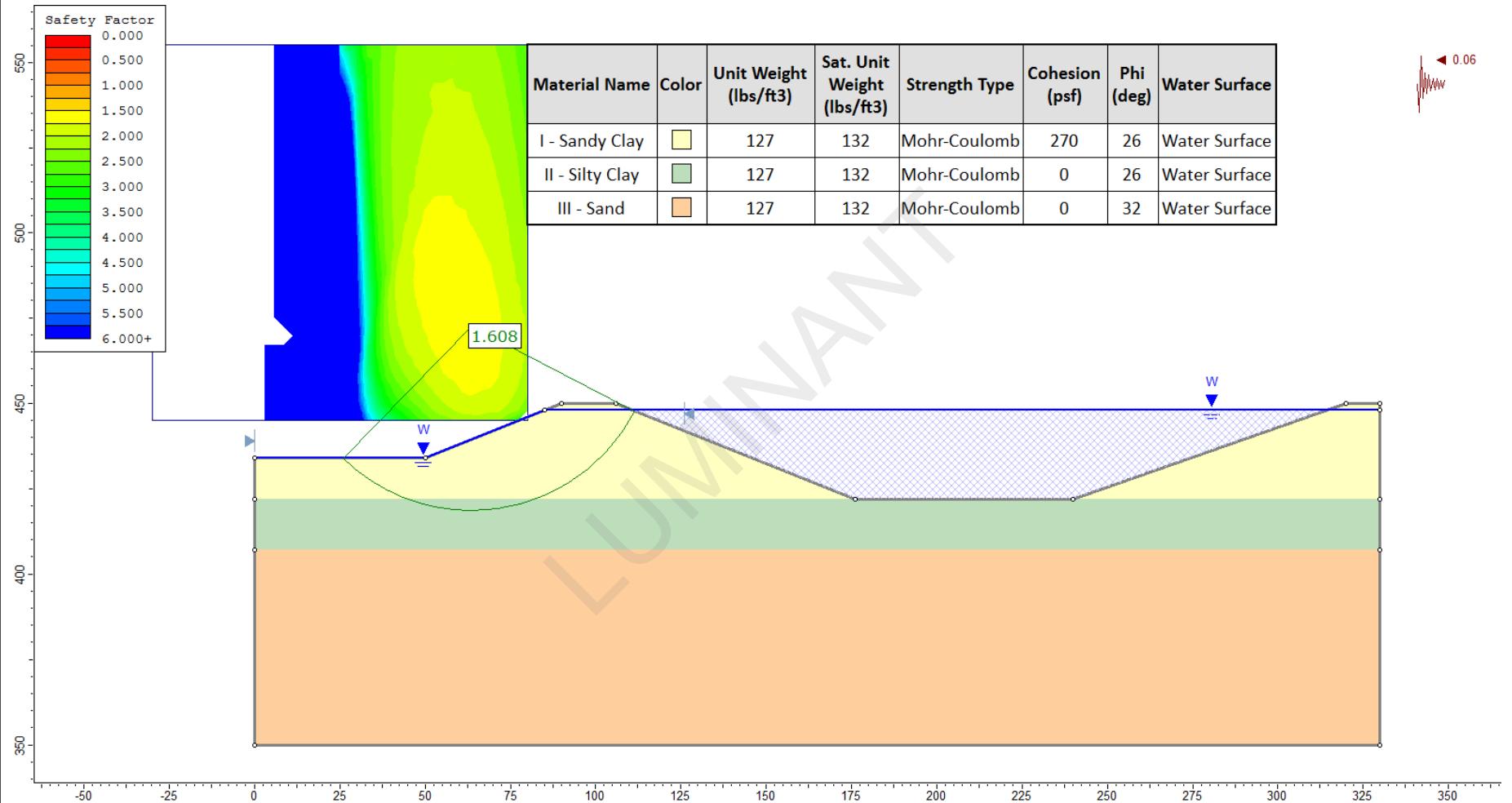


FIGURE C.2
Results of Stability Analysis – FGD-A: A-A' – Case 1b
 Stability and Safety Factor Assessment, Oak Grove SES

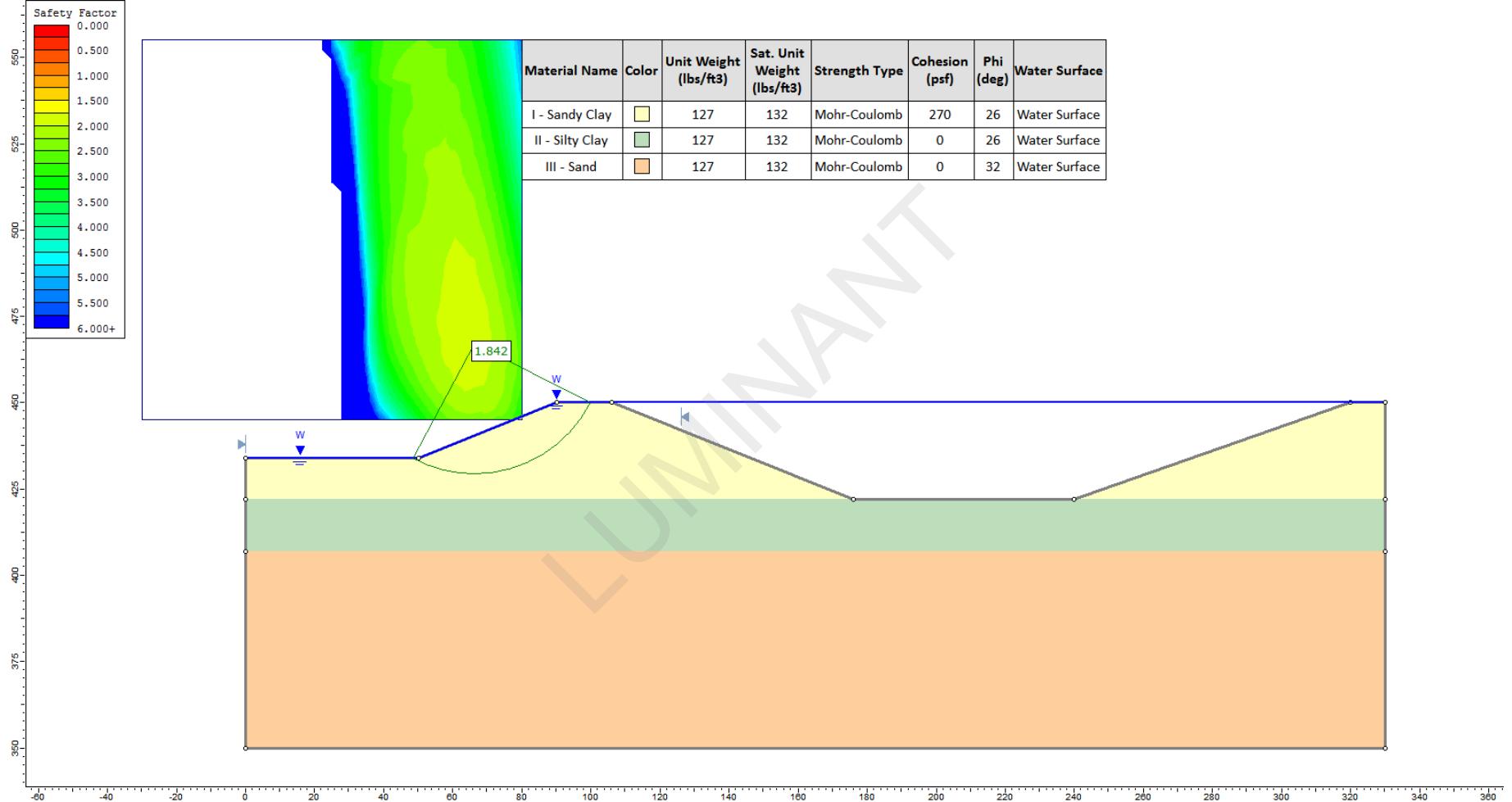


FIGURE C.3
Results of Stability Analysis – FGD-A: A-A' – Case 2a
Stability and Safety Factor Assessment, Oak Grove SES

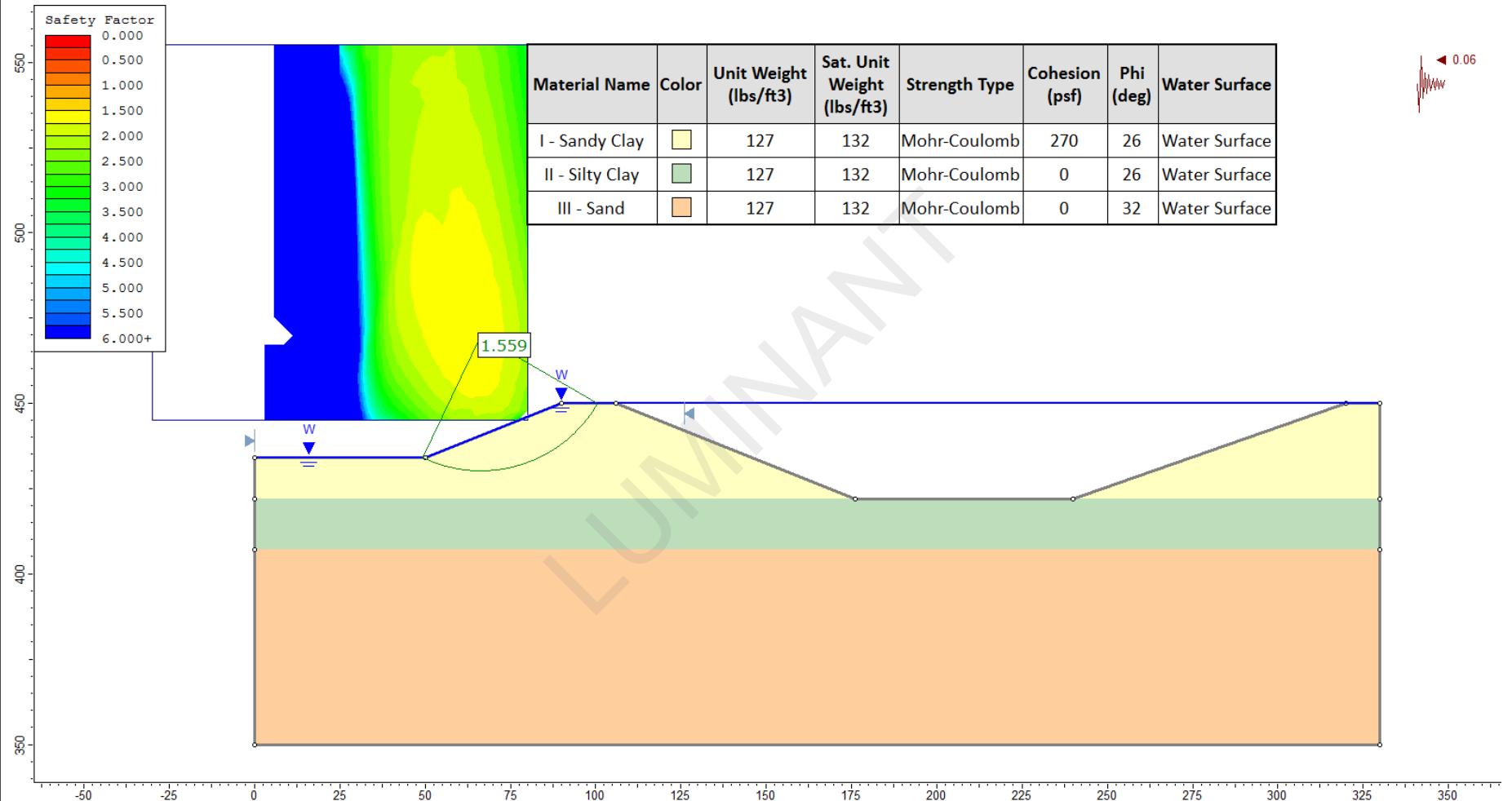


FIGURE C.4
Results of Stability Analysis – FGD-A: A-A' – Case 2b
 Stability and Safety Factor Assessment, Oak Grove SES

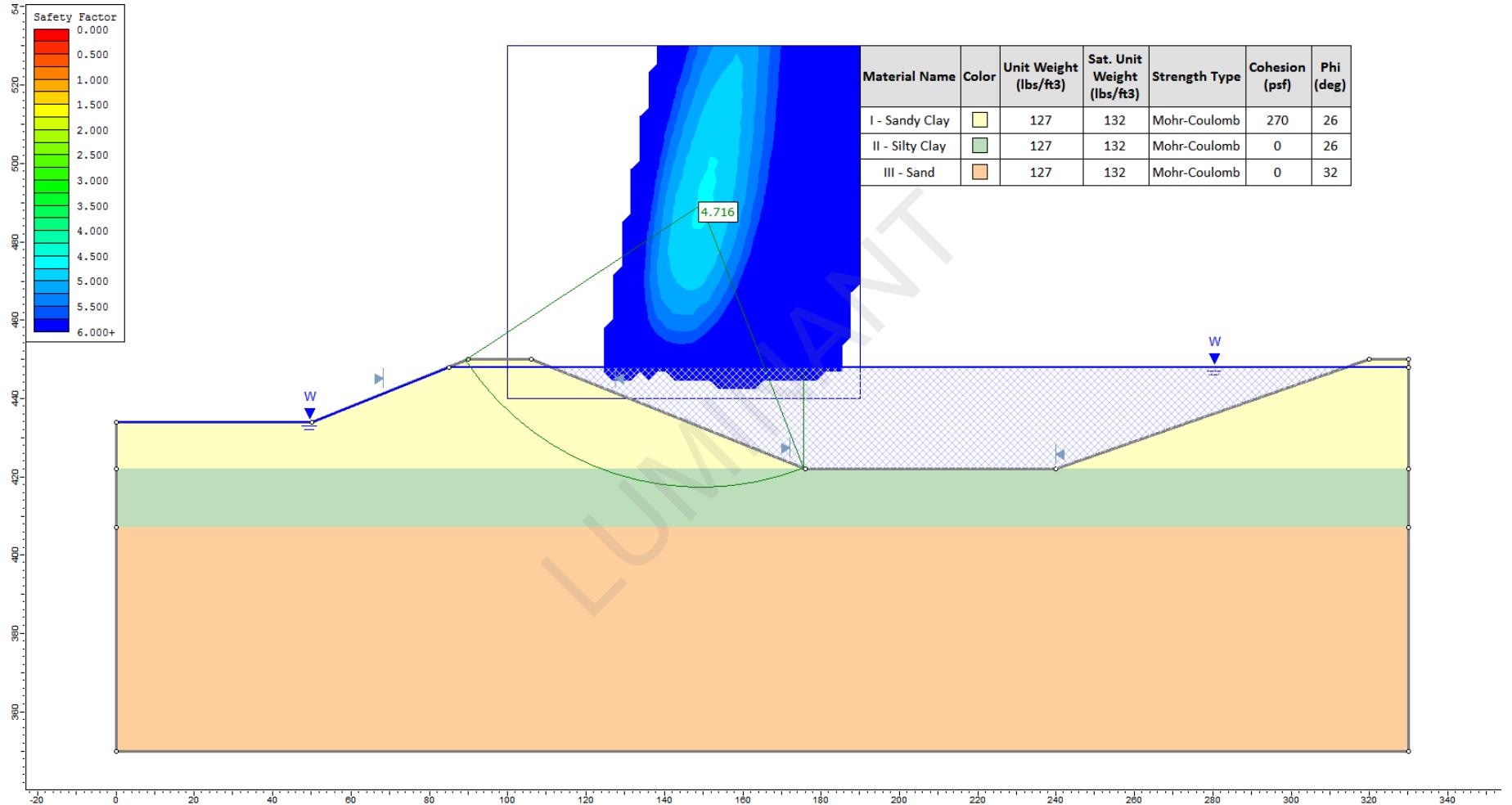


FIGURE C.5
Results of Stability Analysis – FGD-A: A-A' – Case 3a
 Stability and Safety Factor Assessment, Oak Grove SES

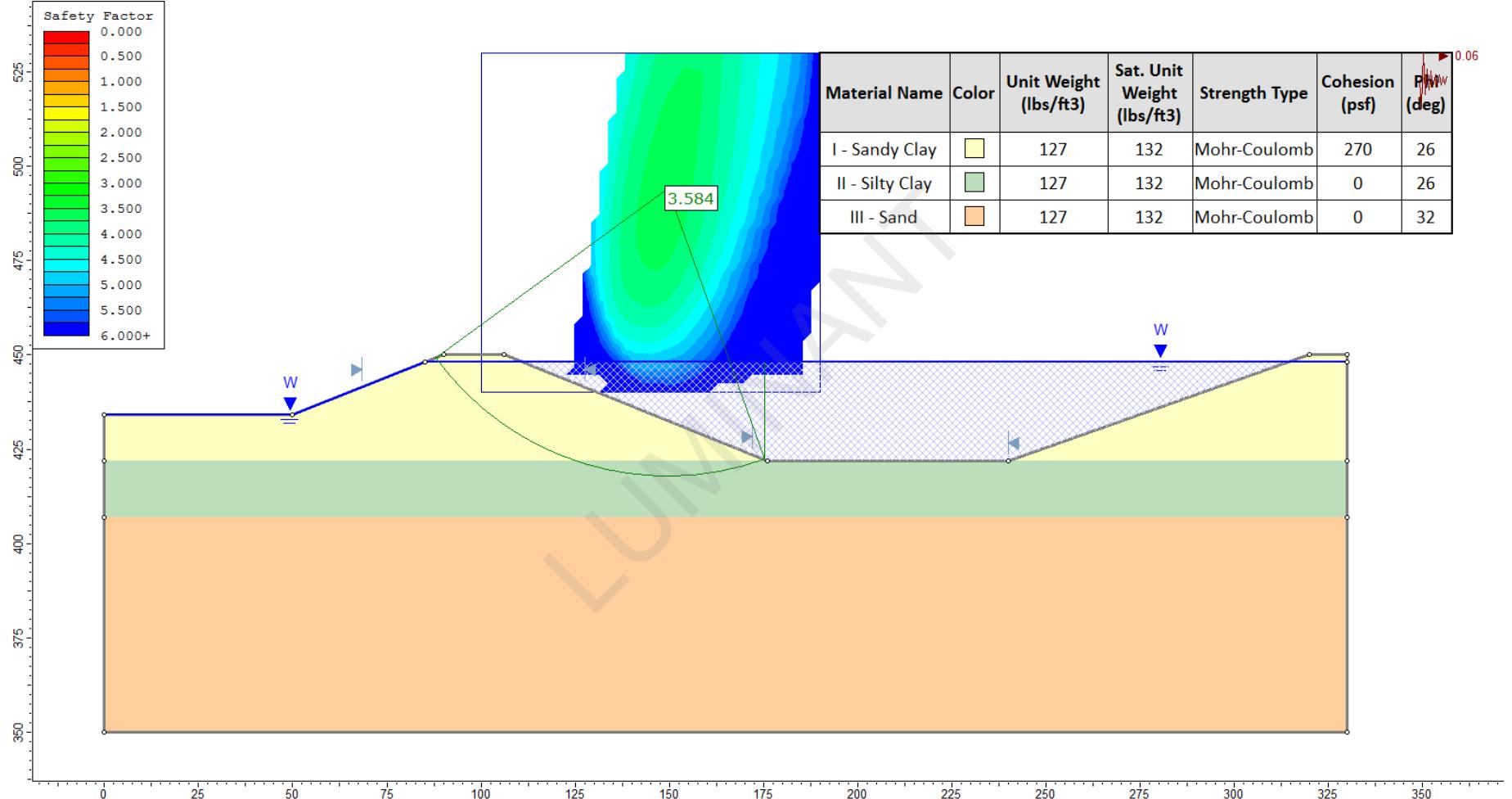


FIGURE C.6
Results of Stability Analysis – FGD-A: A-A' – Case 3b
 Stability and Safety Factor Assessment, Oak Grove SES

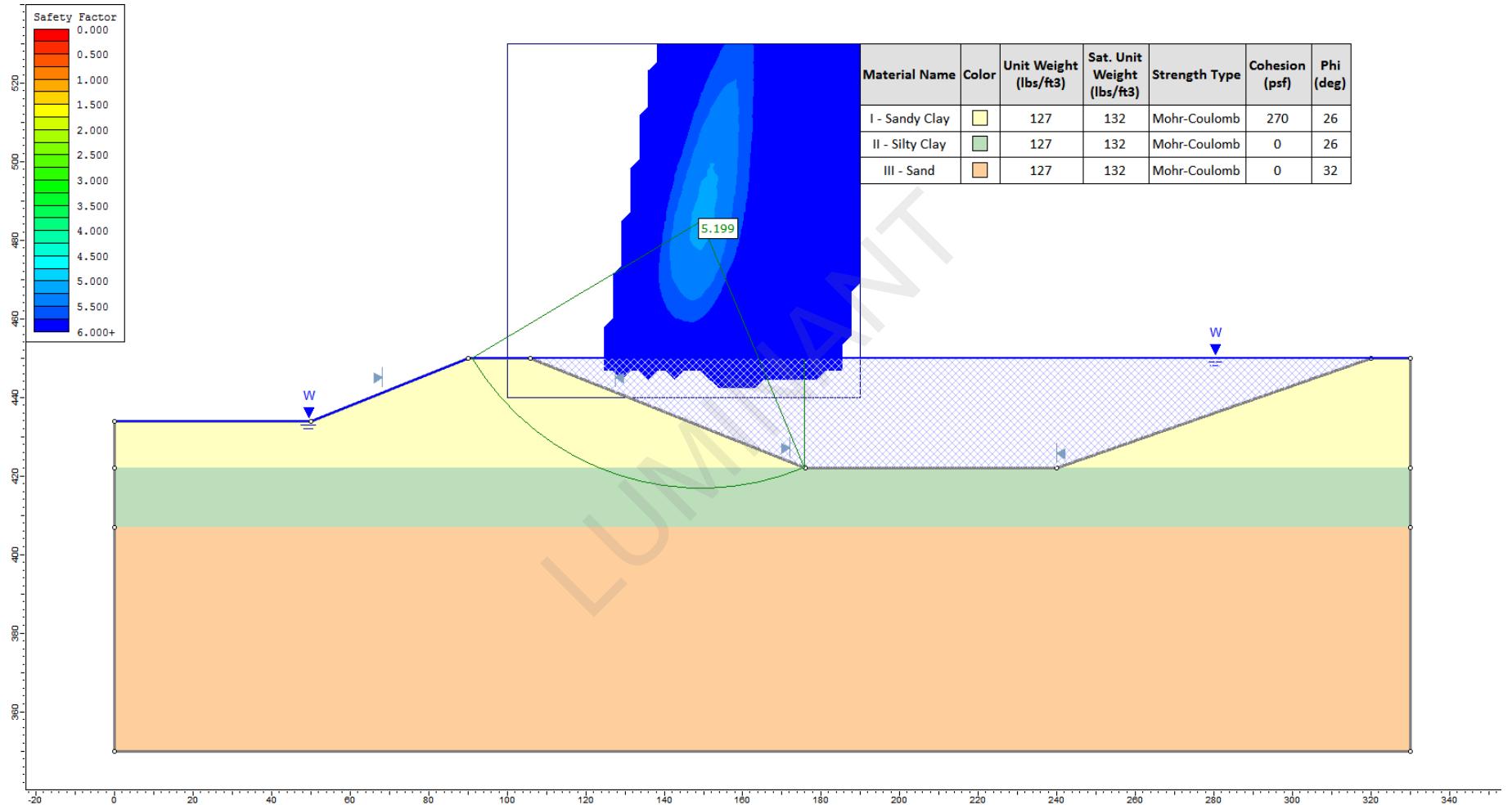


FIGURE C.7
Results of Stability Analysis – FGD-A: A-A' – Case 4a
 Stability and Safety Factor Assessment, Oak Grove SES

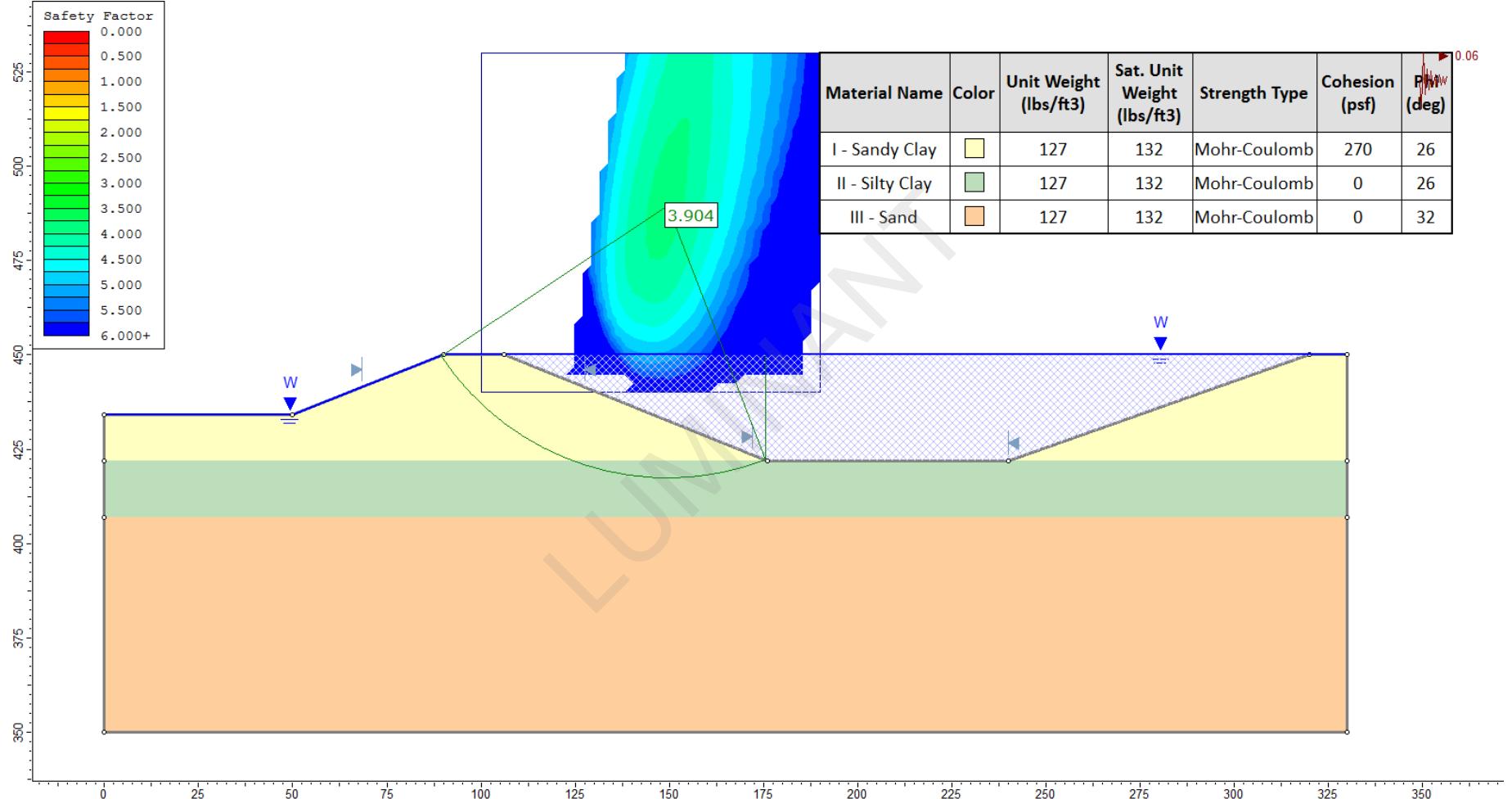


FIGURE C.8
Results of Stability Analysis – FGD-A: A-A' – Case 4b
 Stability and Safety Factor Assessment, Oak Grove SES

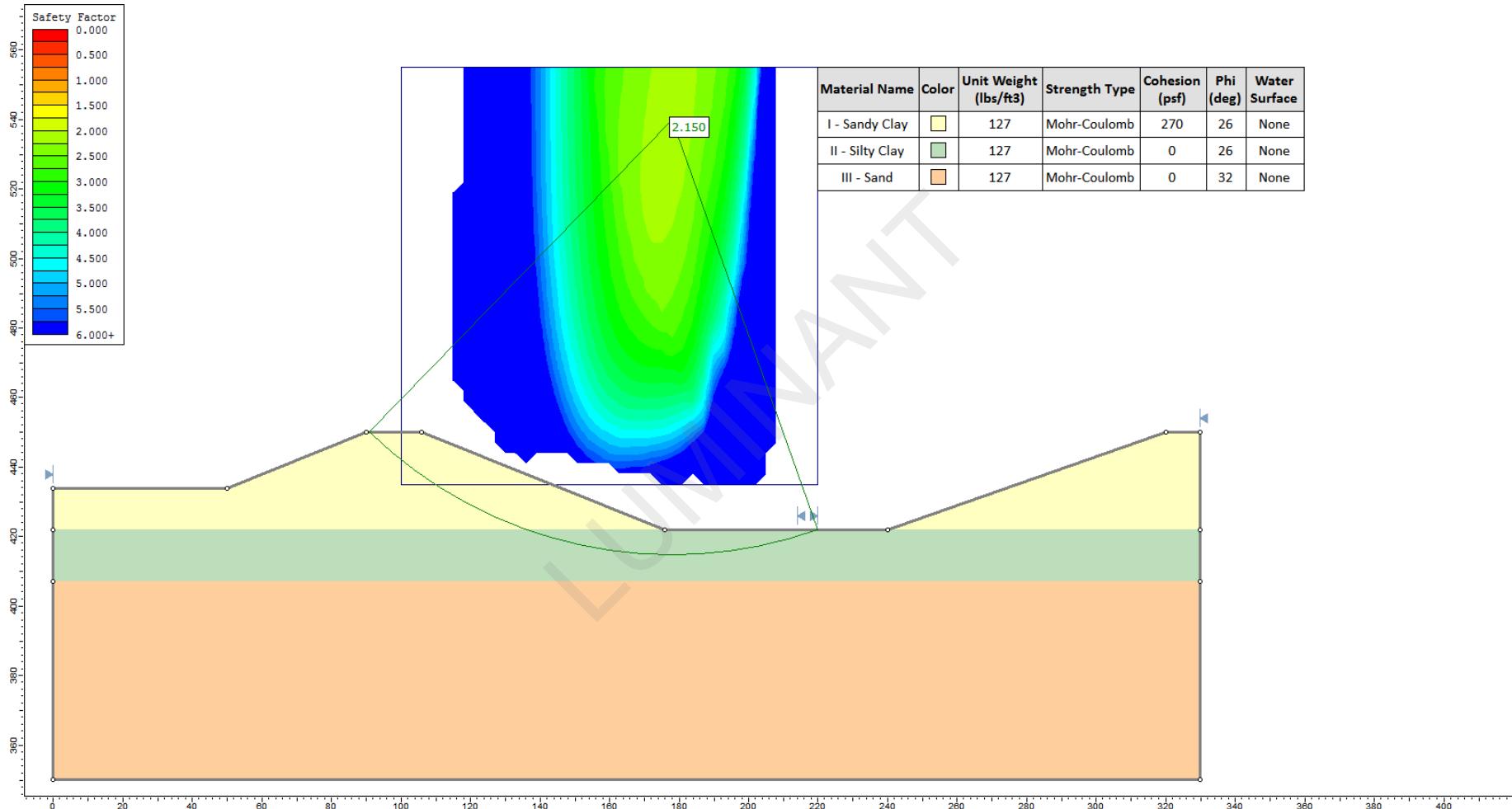


FIGURE C.9
Results of Stability Analysis – FGD-A: A-A' – Case 5a
 Stability and Safety Factor Assessment, Oak Grove SES

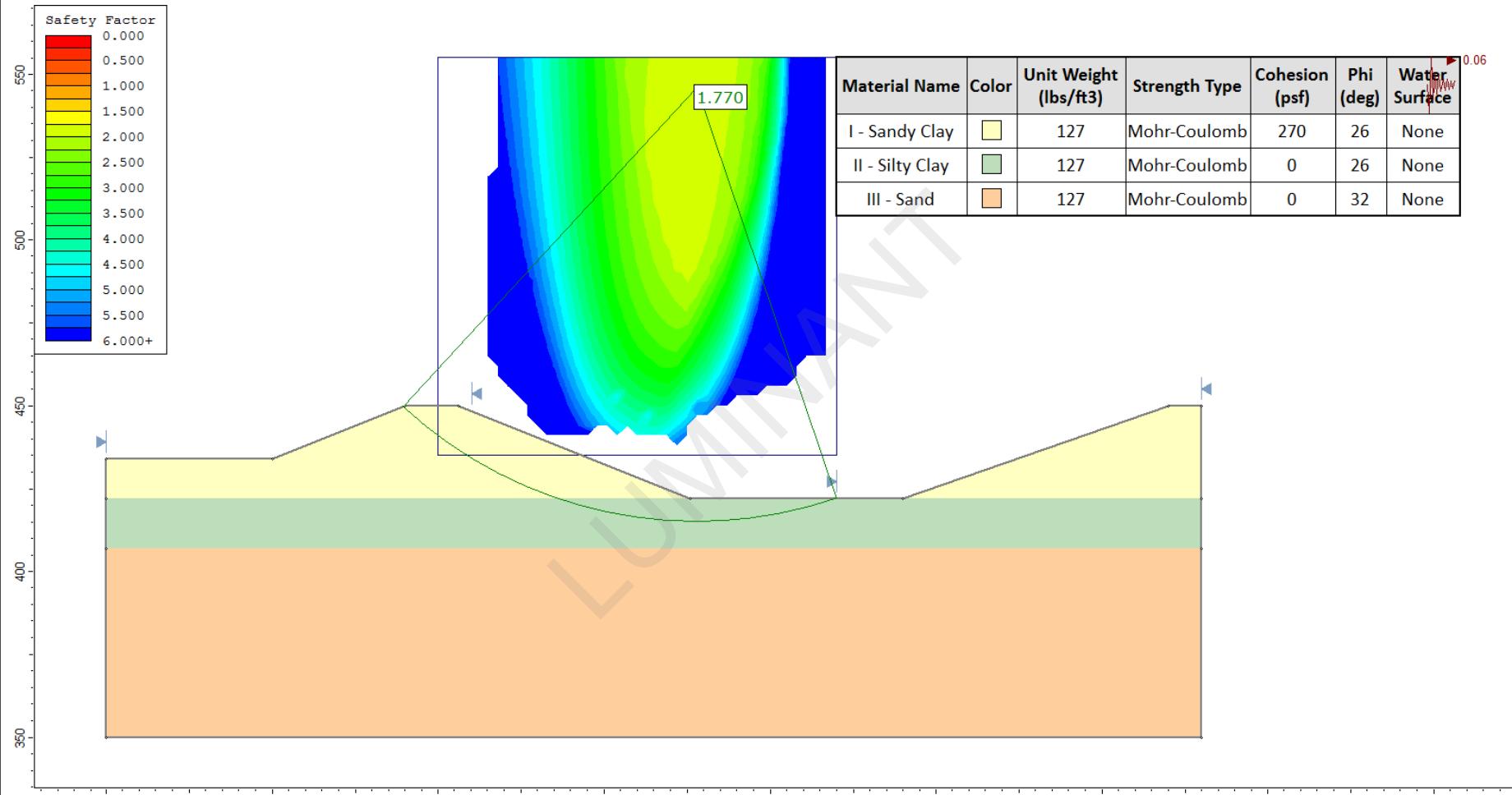


FIGURE C.10
Results of Stability Analysis – FGD-A: A-A' – Case 5b
 Stability and Safety Factor Assessment, Oak Grove SES

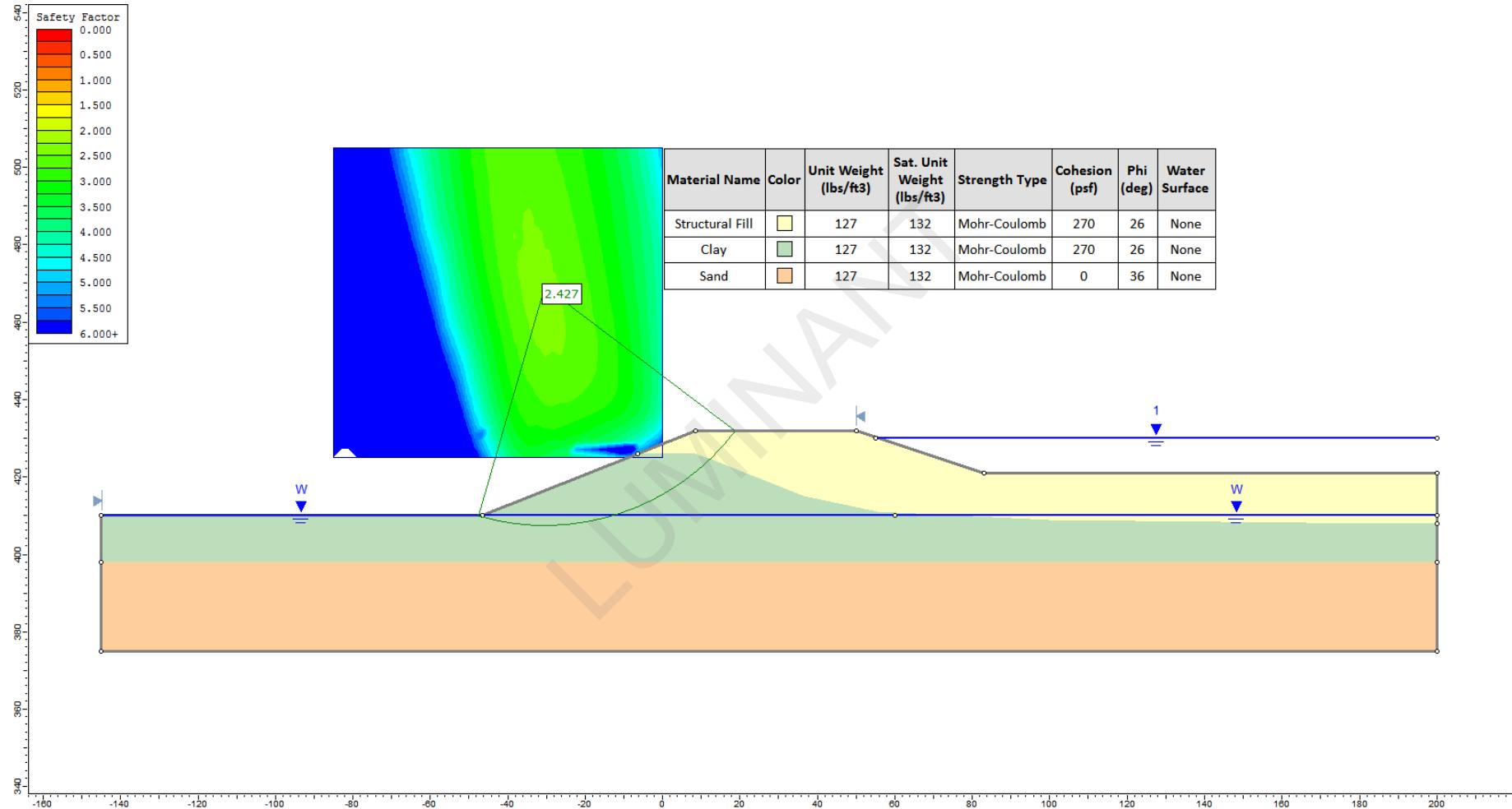


FIGURE C.11
Results of Stability Analysis – FGD-B: B-B' – Case 1a
 Stability and Safety Factor Assessment, Oak Grove SES

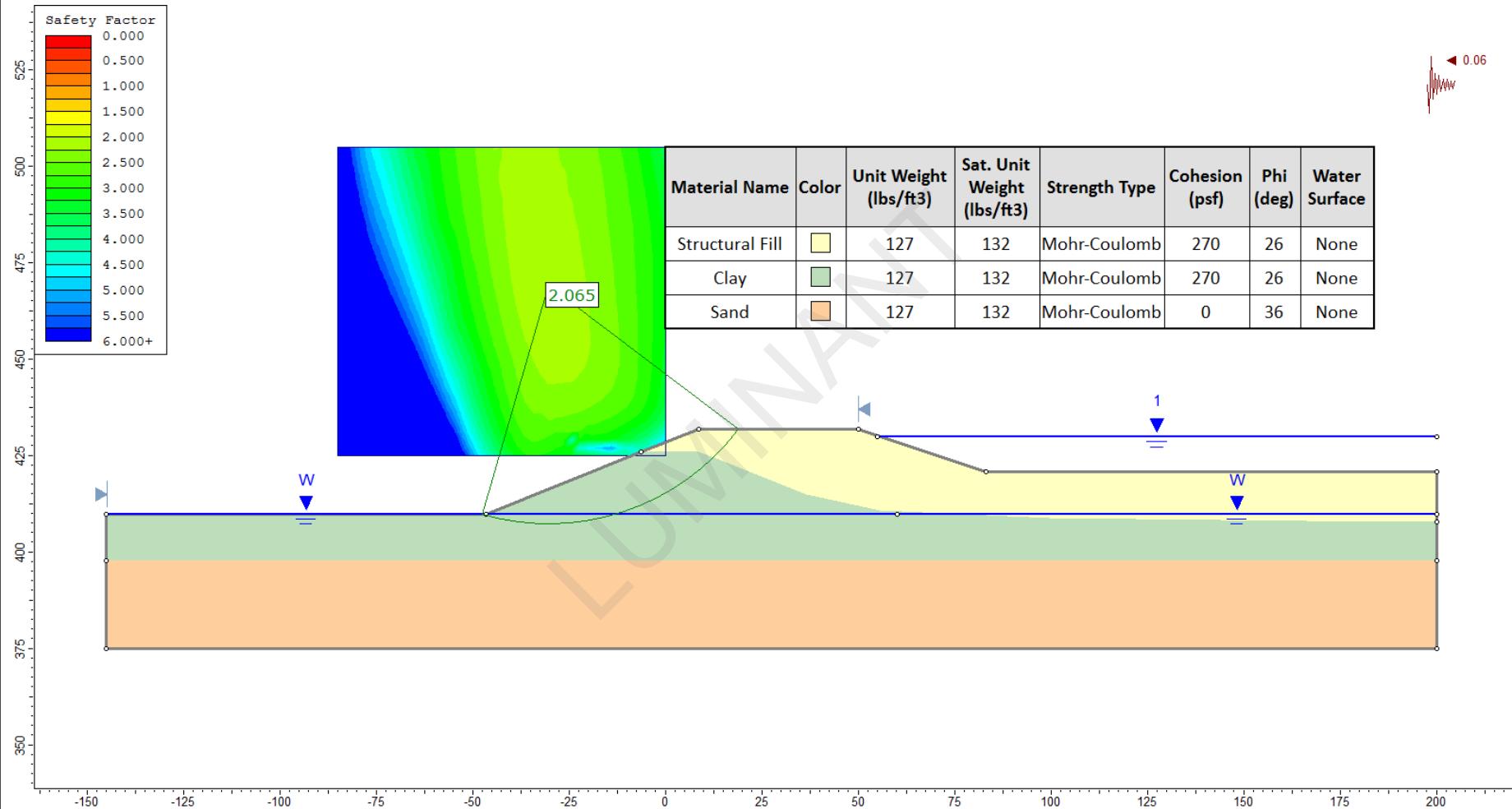


FIGURE C.12
Results of Stability Analysis – FGD-B: B-B' – Case 1b
 Stability and Safety Factor Assessment, Oak Grove SES

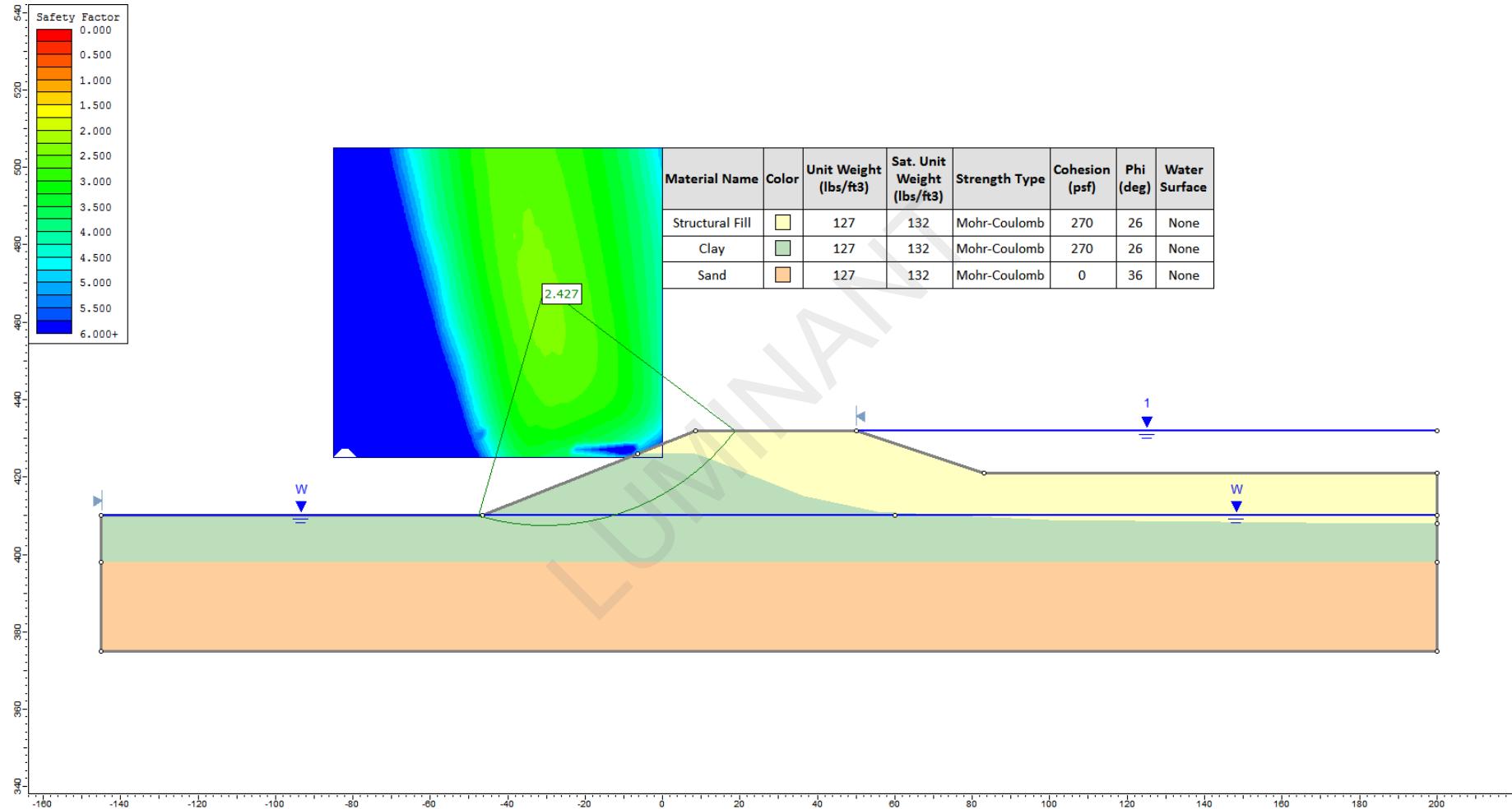


FIGURE C.13
Results of Stability Analysis – FGD-B: B-B' – Case 2a
 Stability and Safety Factor Assessment, Oak Grove SES

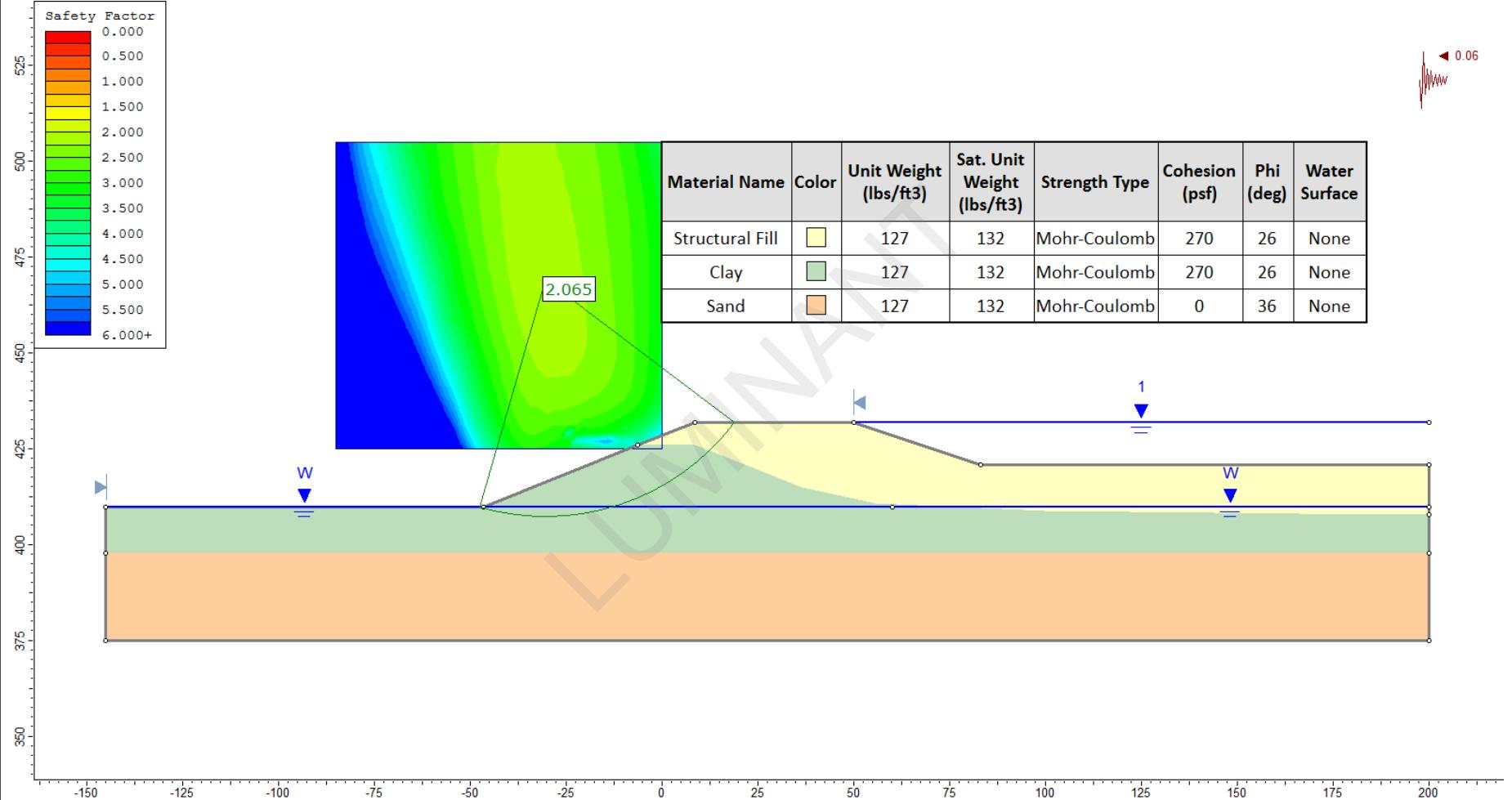


FIGURE C.14
Results of Stability Analysis – FGD-B: B–B' – Case 2b
 Stability and Safety Factor Assessment, Oak Grove SES

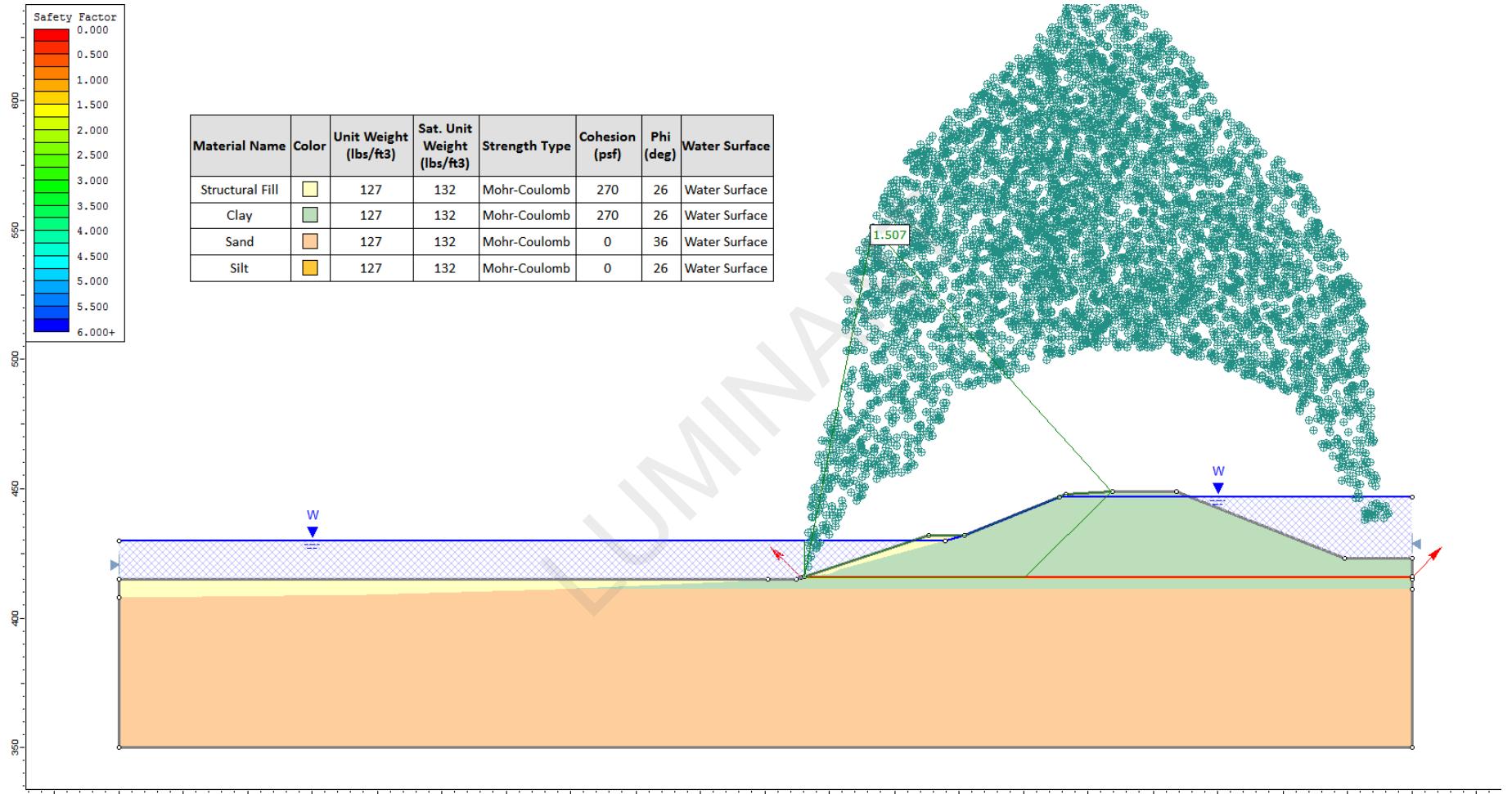


FIGURE C.15
Results of Stability Analysis – FGD-B: B1-B1' – Case 3a
 Stability and Safety Factor Assessment, Oak Grove SES

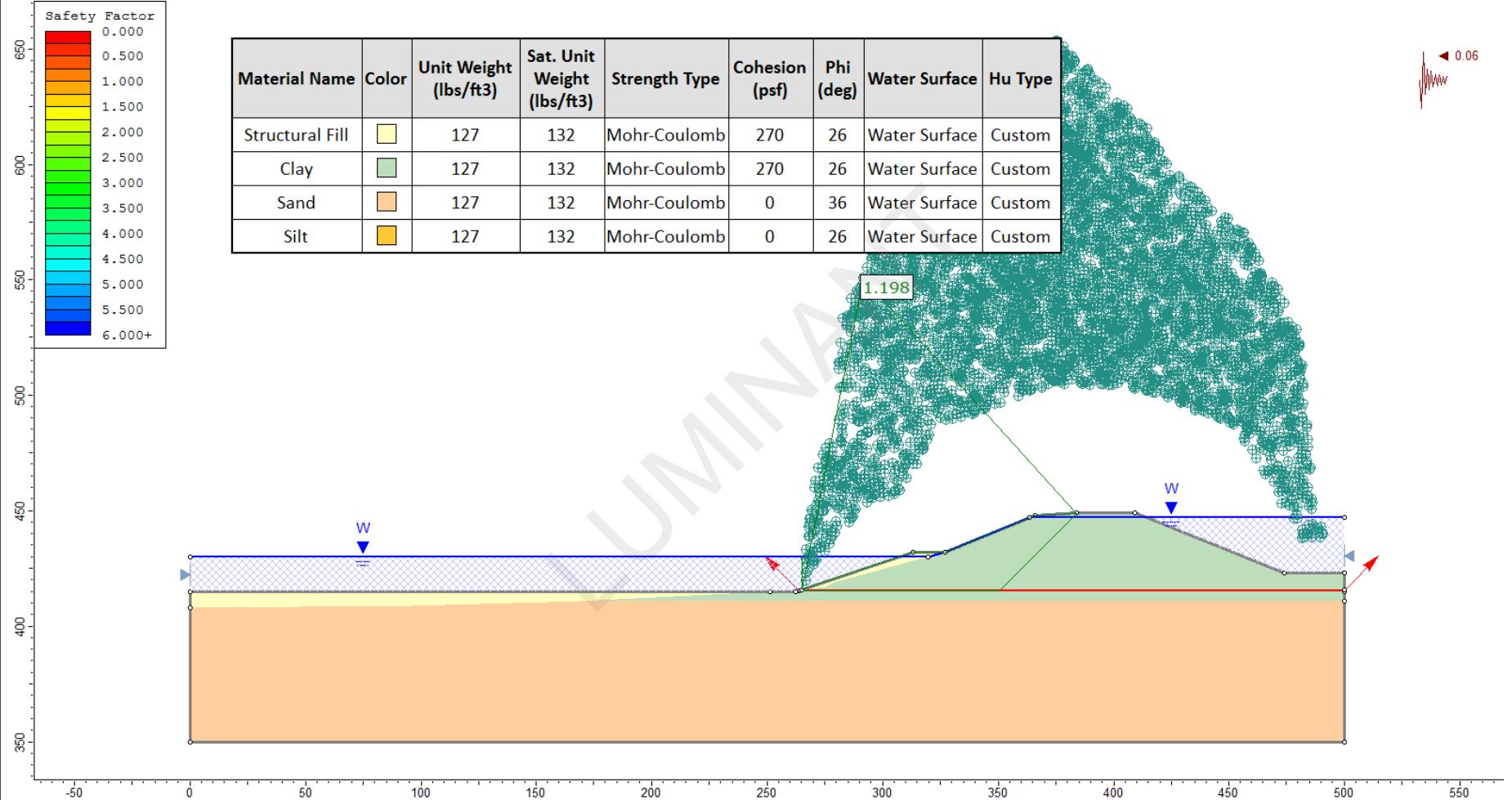
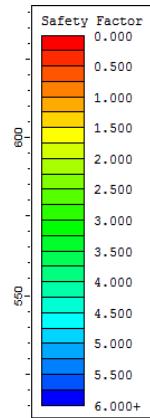


FIGURE C.16
Results of Stability Analysis – FGD-B: B1–B1' – Case 3b
 Stability and Safety Factor Assessment, Oak Grove SES



Material Name	Color	Unit Weight (lbs/ft³)	Sat. Unit Weight (lbs/ft³)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface
Structural Fill	Light Yellow	127	132	Mohr-Coulomb	270	26	Water Surface
Clay	Light Green	127	132	Mohr-Coulomb	270	26	Water Surface
Sand	Light Orange	127	132	Mohr-Coulomb	0	36	Water Surface
Silt	Yellow	127	132	Mohr-Coulomb	0	26	Water Surface

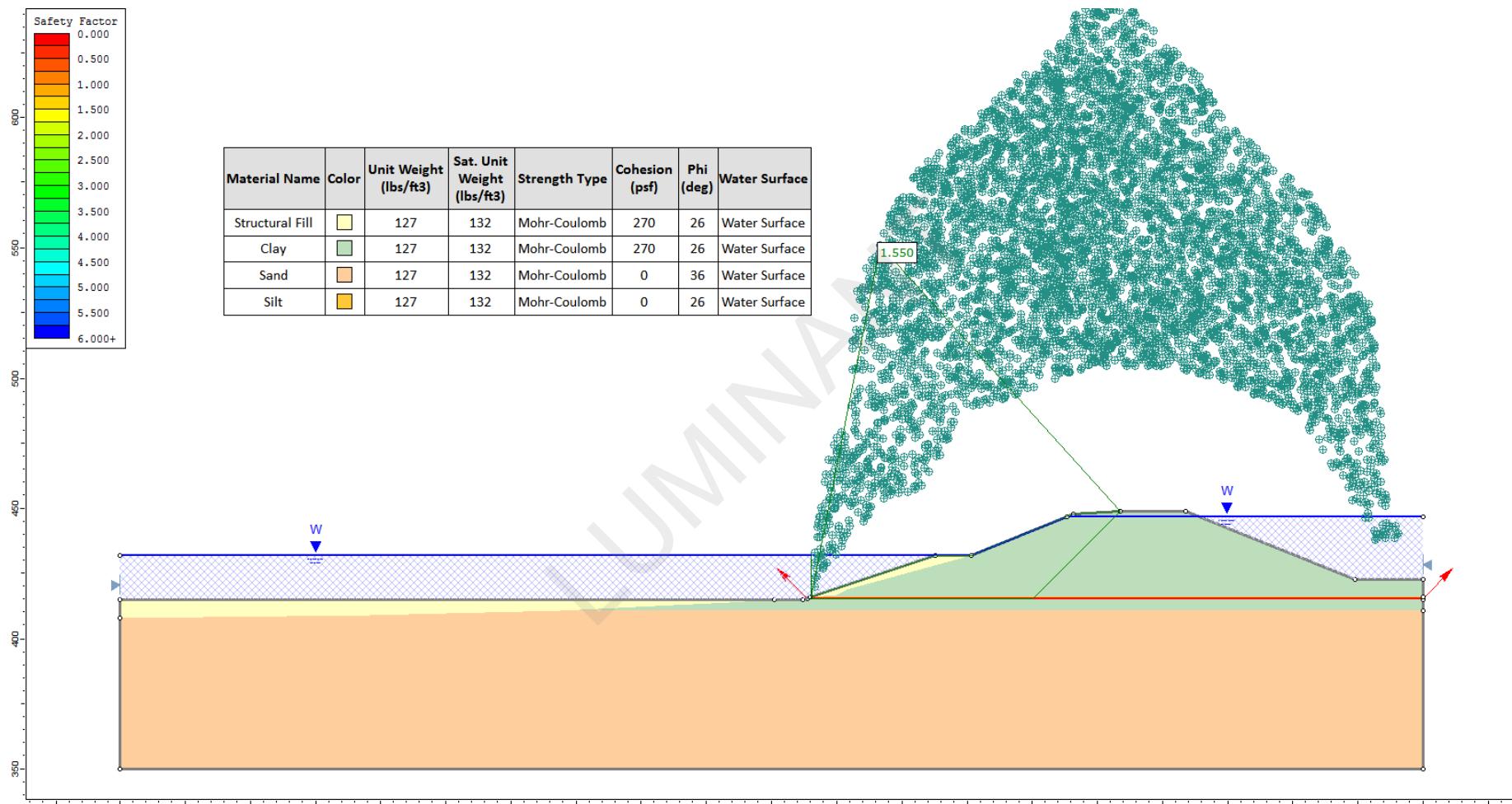


FIGURE C.17
Results of Stability Analysis – FGD-B: B1–B1' – Case 4a
Stability and Safety Factor Assessment, Oak Grove SES

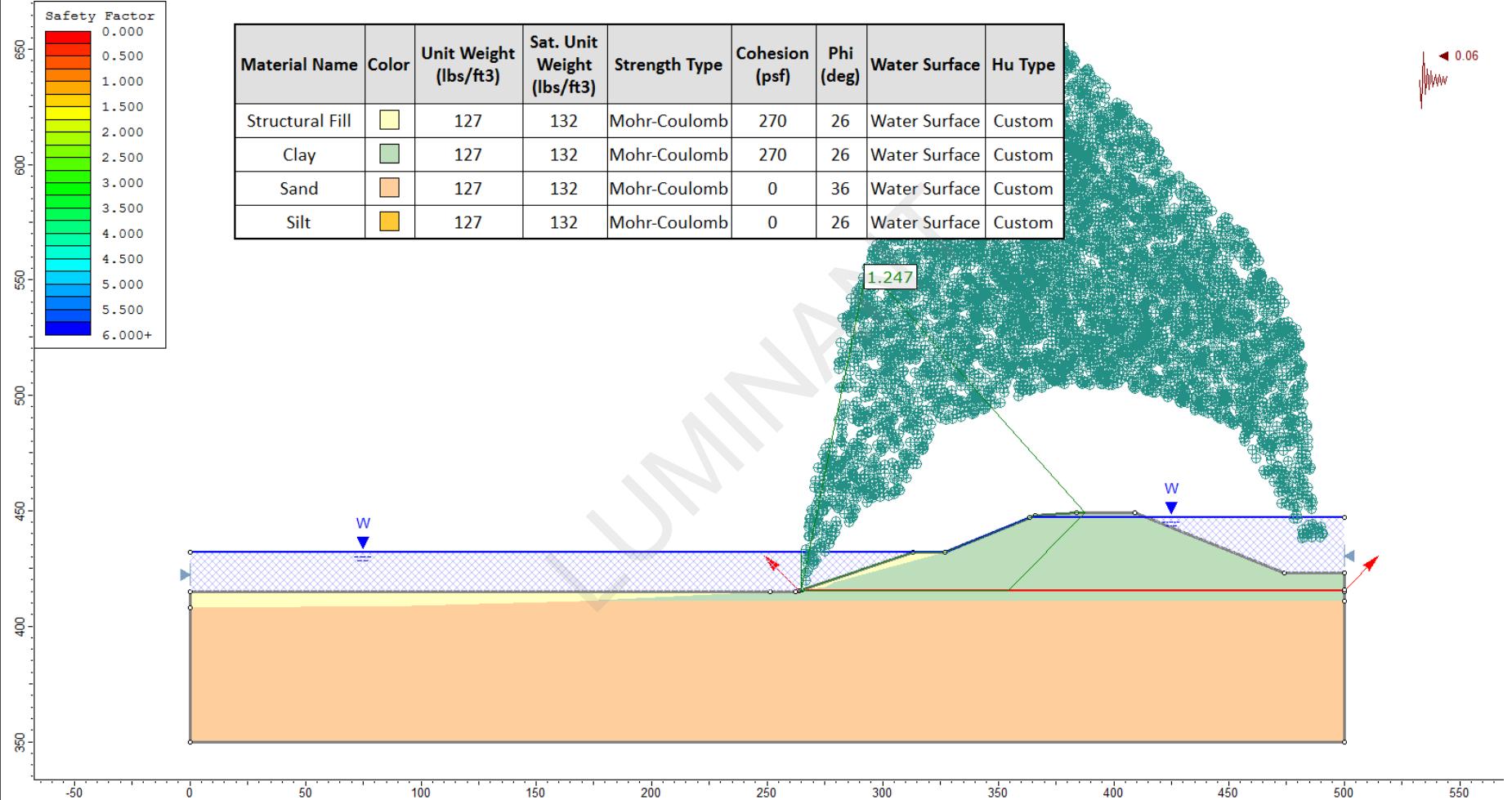
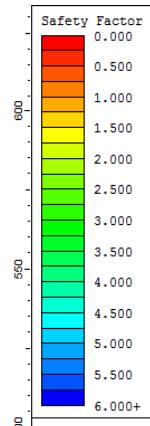


FIGURE C.18
Results of Stability Analysis – FGD-B: B1–B1' – Case 4b
 Stability and Safety Factor Assessment, Oak Grove SES



Material Name	Color	Unit Weight (lbs/ft³)	Sat. Unit Weight (lbs/ft³)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface
Structural Fill	Light Yellow	127	132	Mohr-Coulomb	270	26	Water Surface
Clay	Light Green	127	132	Mohr-Coulomb	270	26	Water Surface
Sand	Light Orange	127	132	Mohr-Coulomb	0	36	Water Surface
Silt	Yellow	127	132	Mohr-Coulomb	0	26	Water Surface

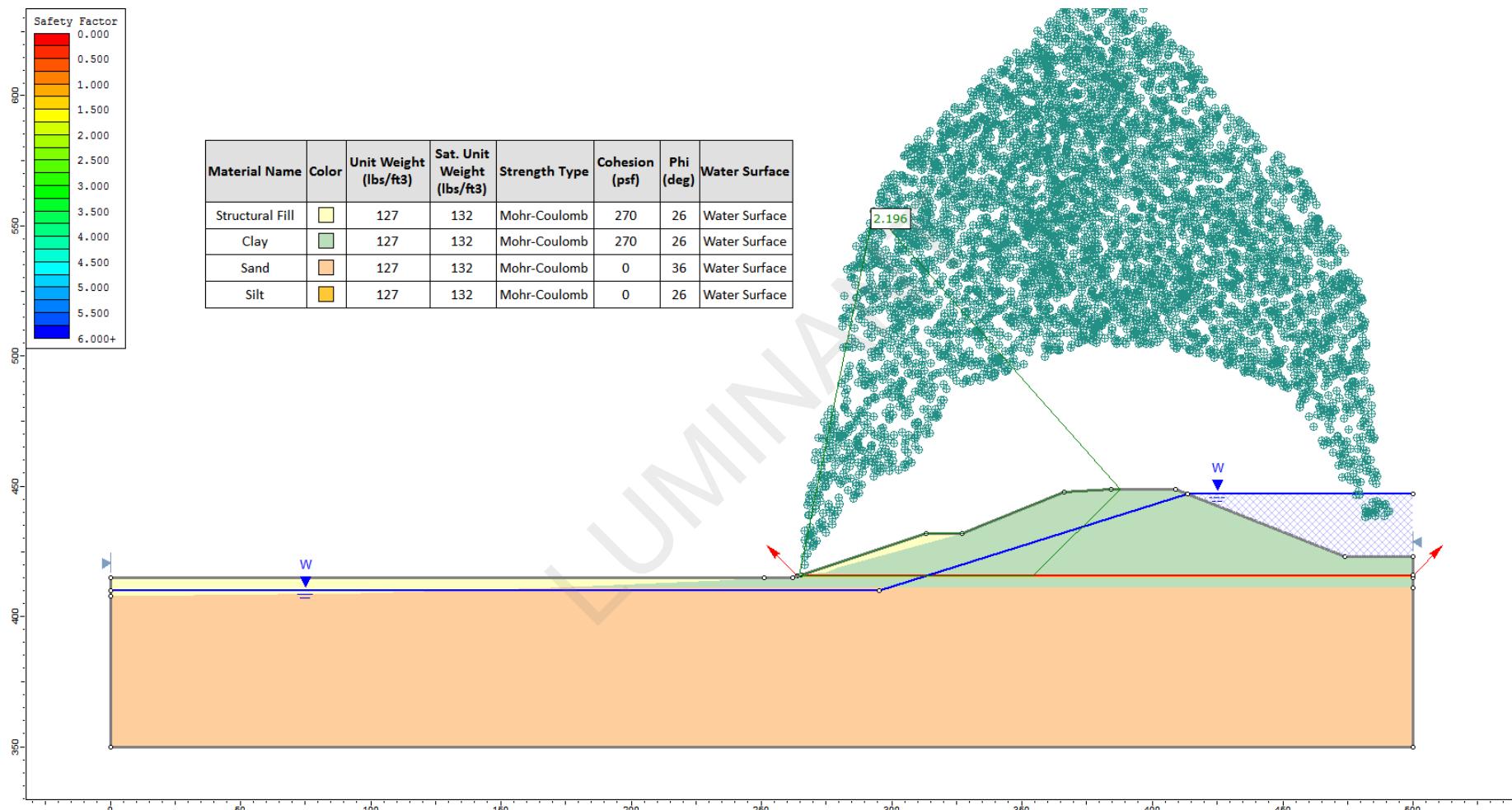
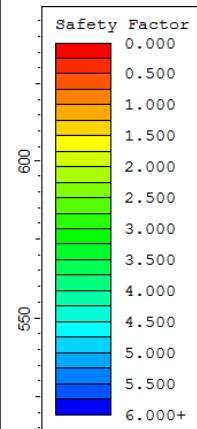


FIGURE C.19
Results of Stability Analysis – FGD-B: B1–B1' – Case 5a
 Stability and Safety Factor Assessment, Oak Grove SES



Material Name	Color	Unit Weight (lbs/ft ³)	Sat. Unit Weight (lbs/ft ³)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface
Structural Fill	Yellow	127	132	Mohr-Coulomb	270	26	Water Surface
Clay	Green	127	132	Mohr-Coulomb	270	26	Water Surface
Sand	Orange	127	132	Mohr-Coulomb	0	36	Water Surface
Silt	Yellow	127	132	Mohr-Coulomb	0	26	Water Surface

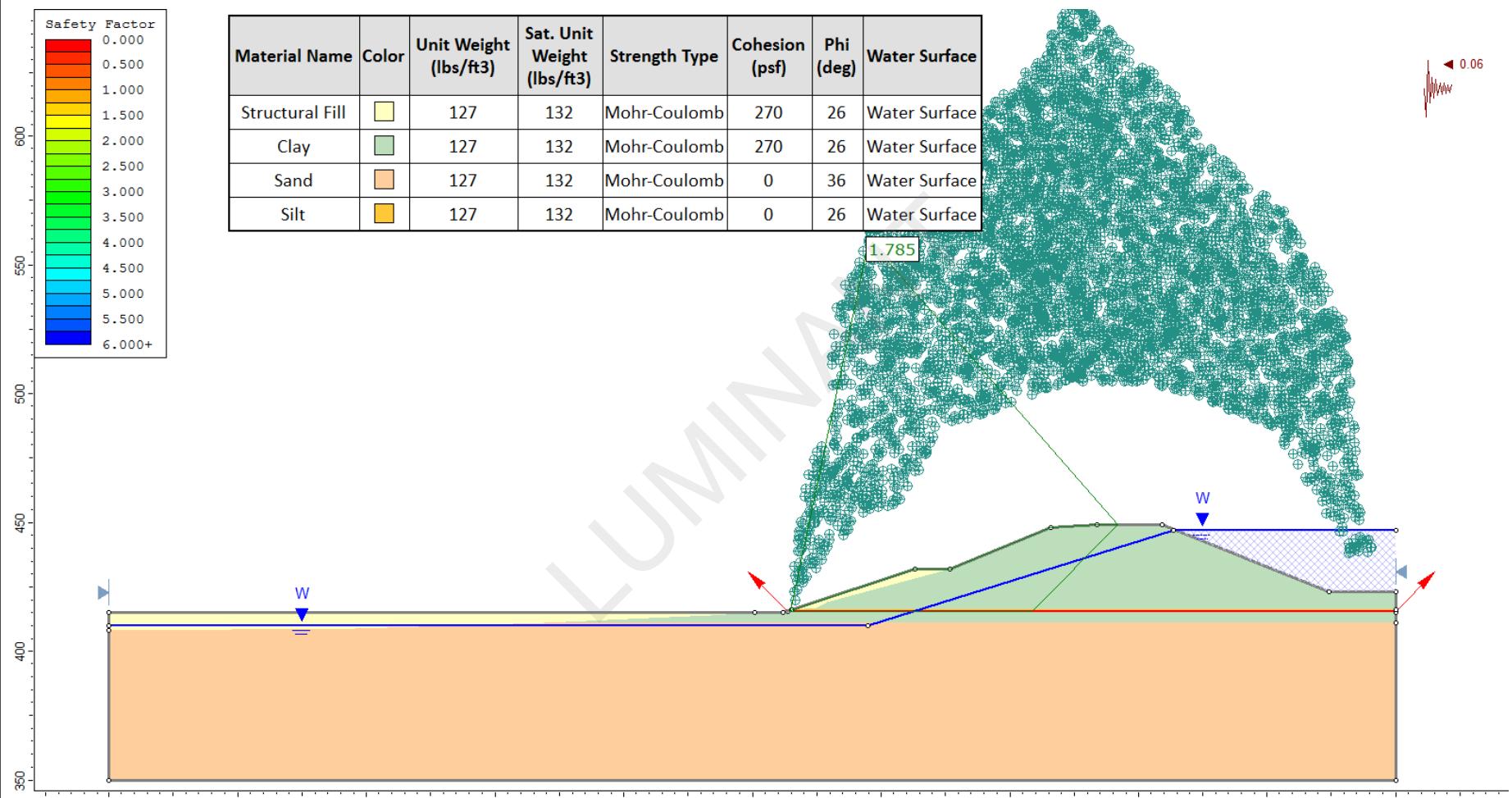


FIGURE C.20
Results of Stability Analysis – FGD-B: B1–B1' – Case 5b
 Stability and Safety Factor Assessment, Oak Grove SES

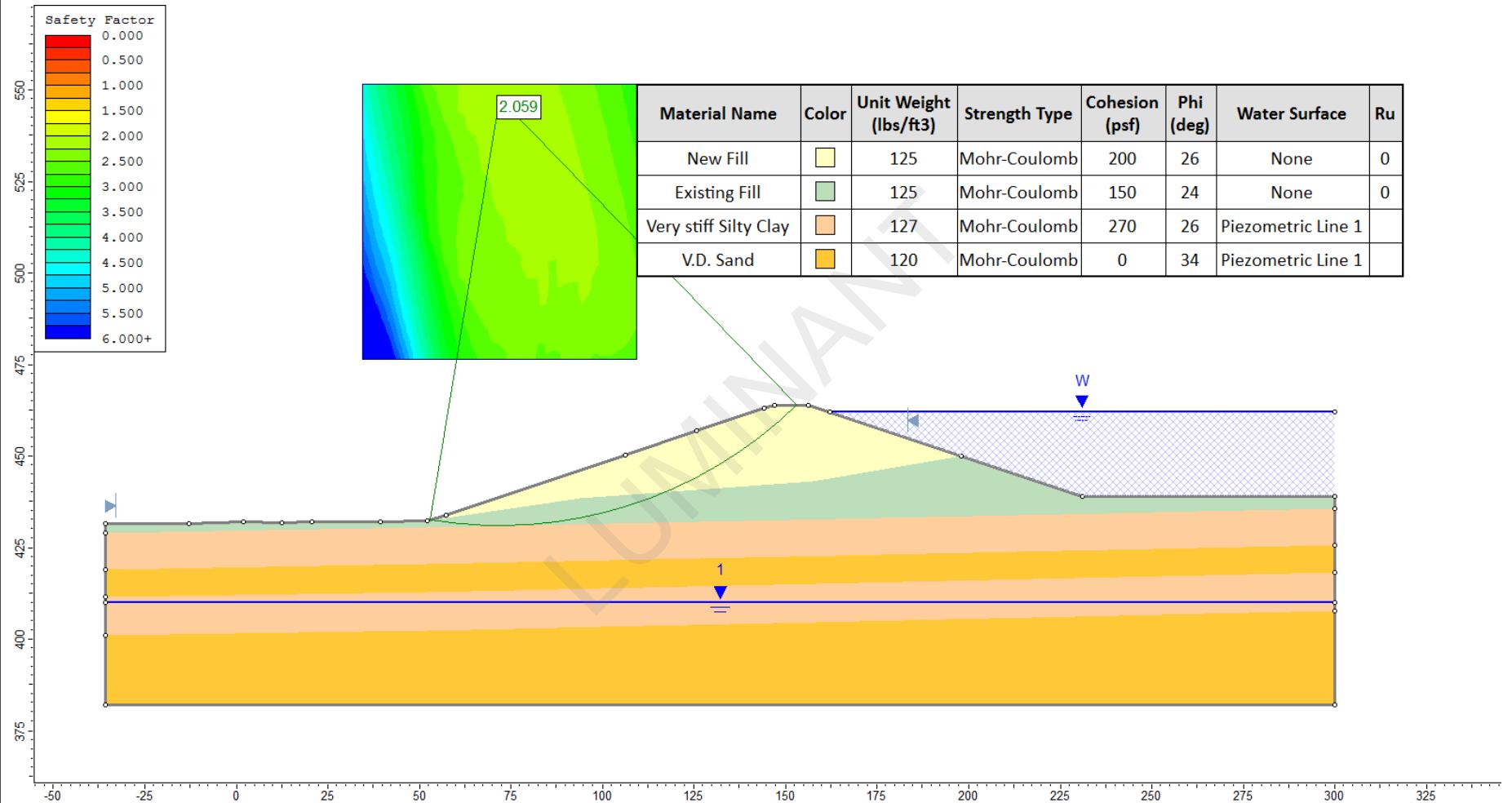


FIGURE C.21
Results of Stability Analysis – FGD-C: C–C' – Case 1a
 Stability and Safety Factor Assessment, Oak Grove SES

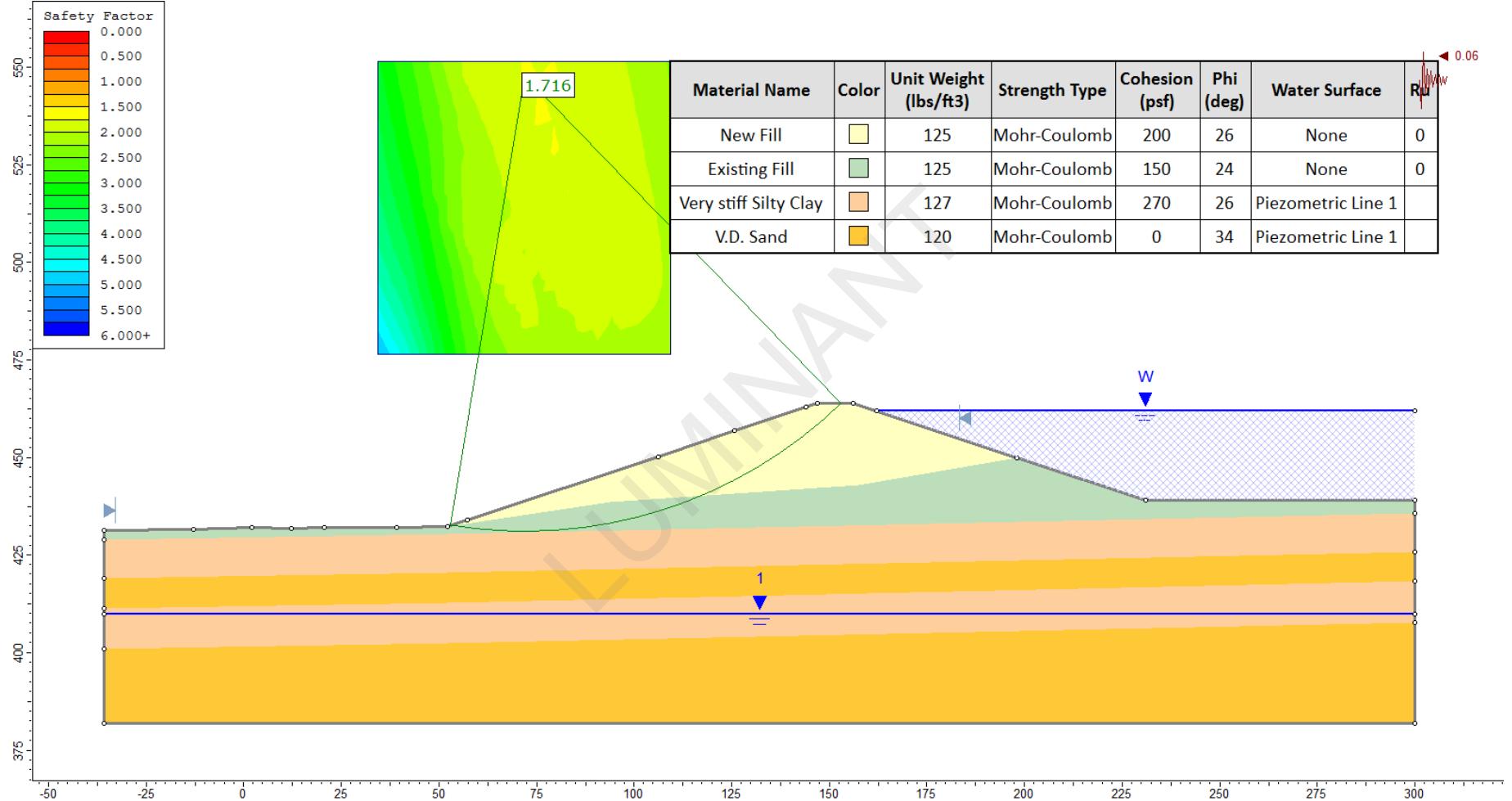


FIGURE C.22
Results of Stability Analysis – FGD-C: C-C' – Case 1b
 Stability and Safety Factor Assessment, Oak Grove SES

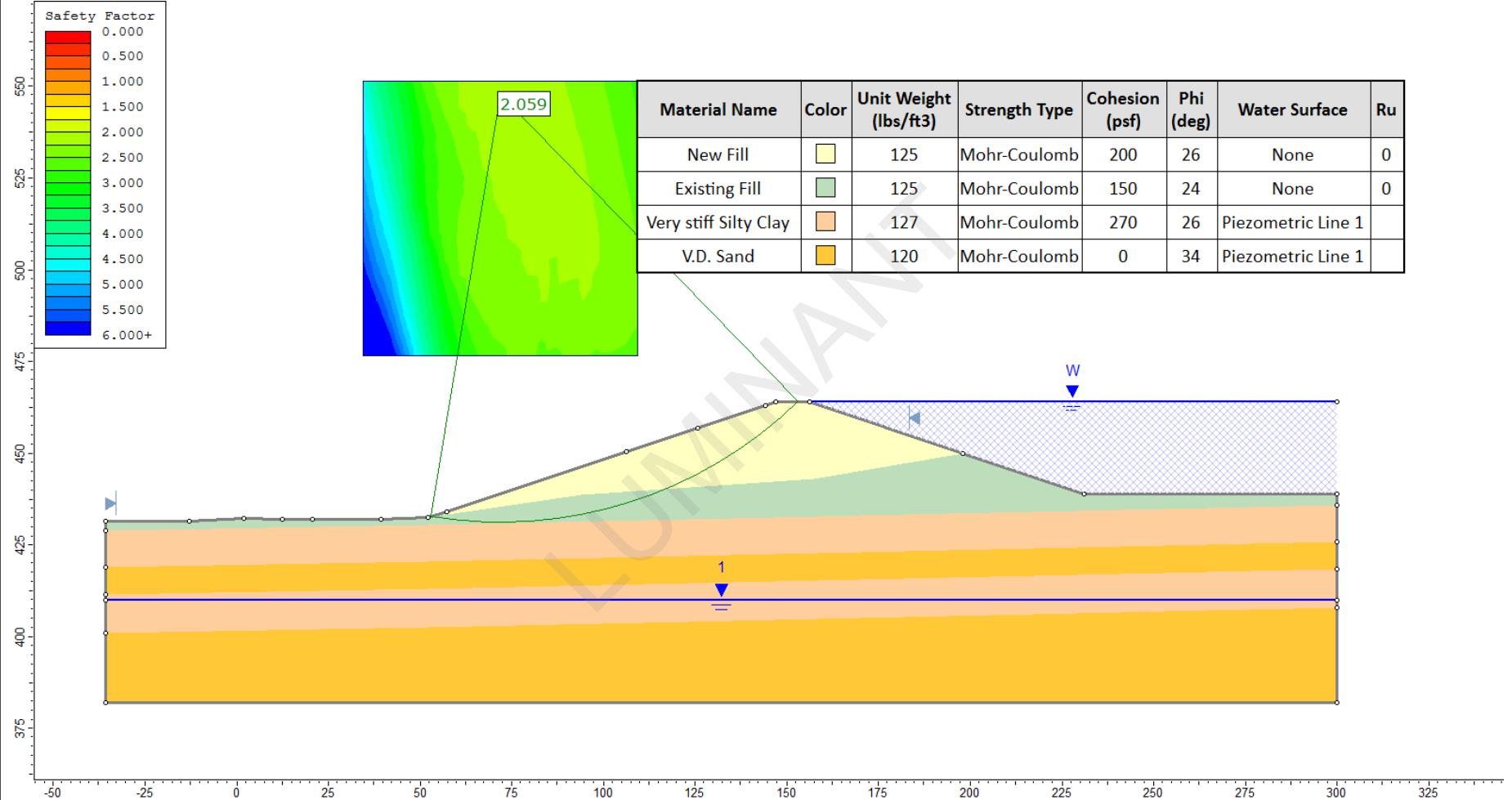


FIGURE C.23
Results of Stability Analysis – FGD-C: C–C' – Case 2a
 Stability and Safety Factor Assessment, Oak Grove SES

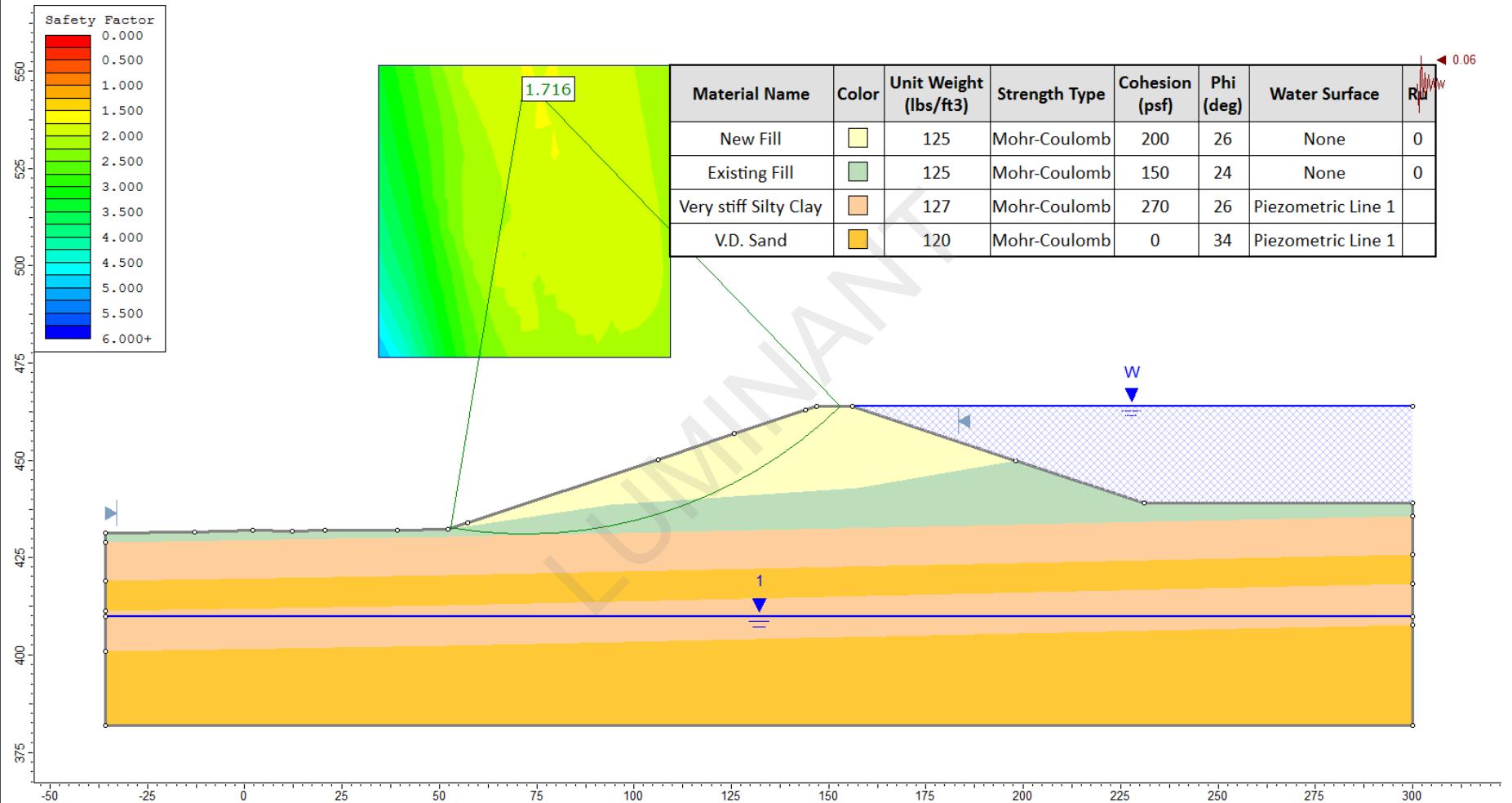


FIGURE C.24
Results of Stability Analysis – FGD-C: C–C' – Case 2b
 Stability and Safety Factor Assessment, Oak Grove SES

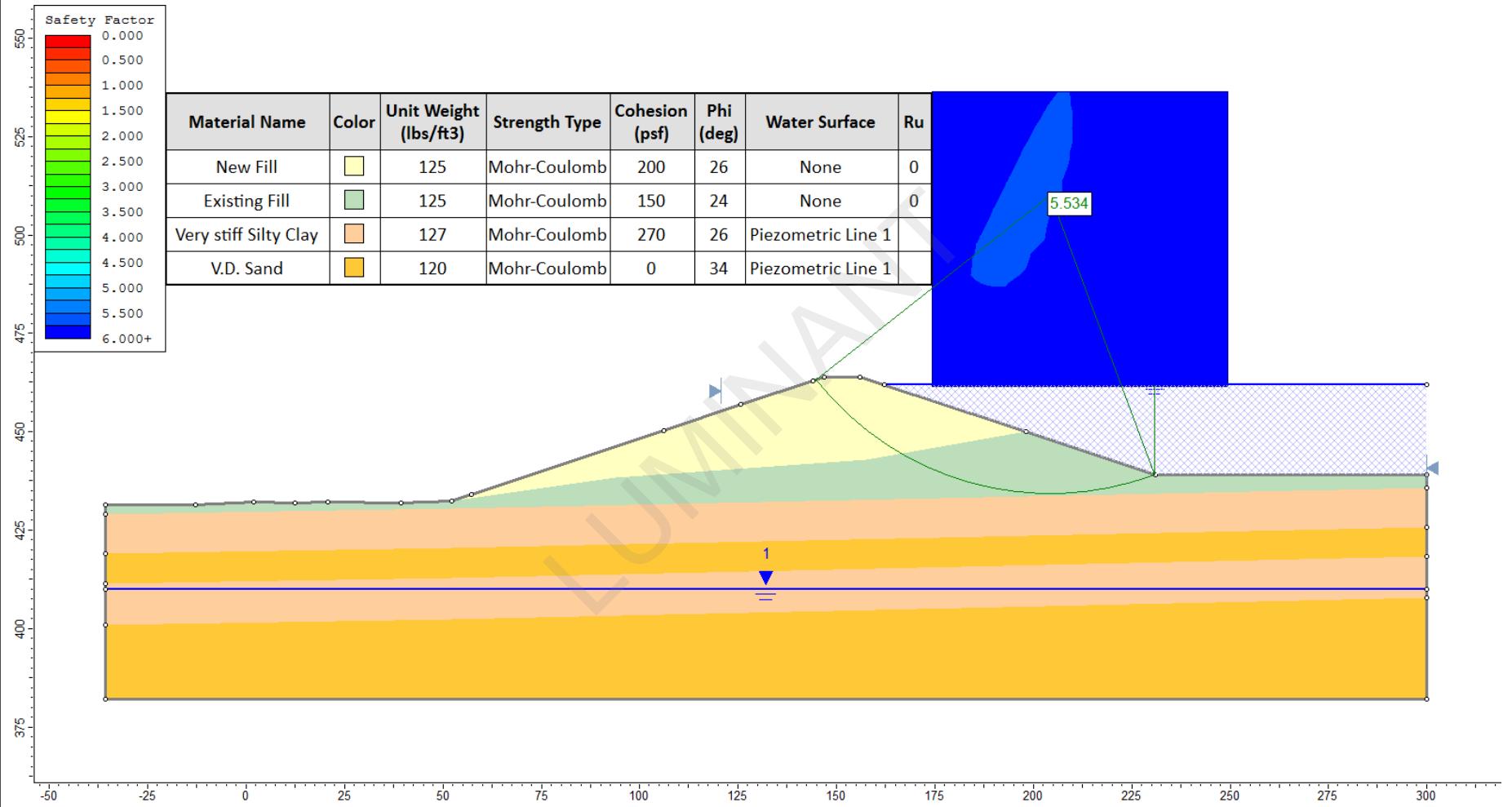


FIGURE C.25
Results of Stability Analysis – FGD-C: C–C' – Case 3a
 Stability and Safety Factor Assessment, Oak Grove SES

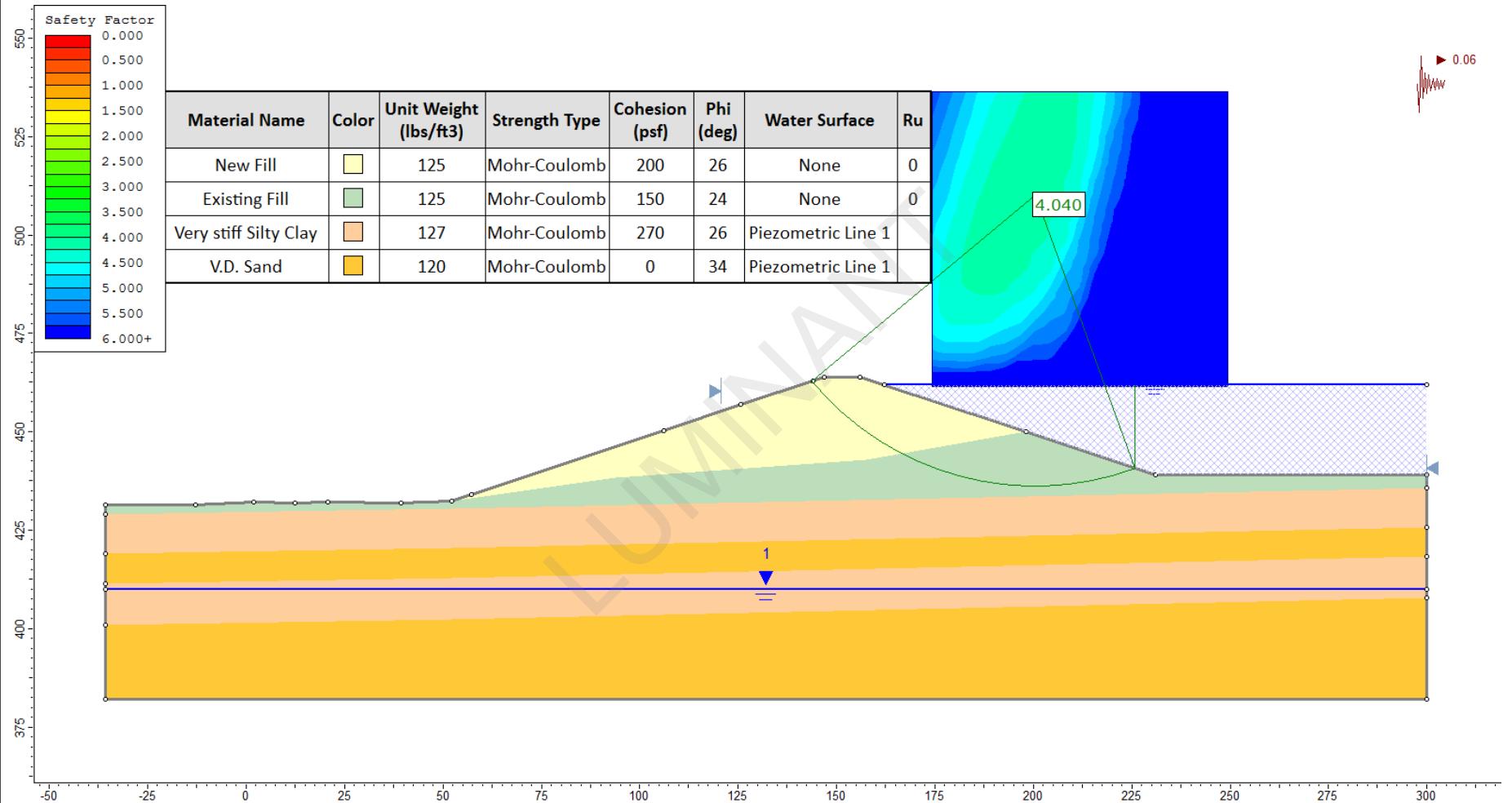


FIGURE C.26
Results of Stability Analysis – FGD-C: C–C' – Case 3b
 Stability and Safety Factor Assessment, Oak Grove SES

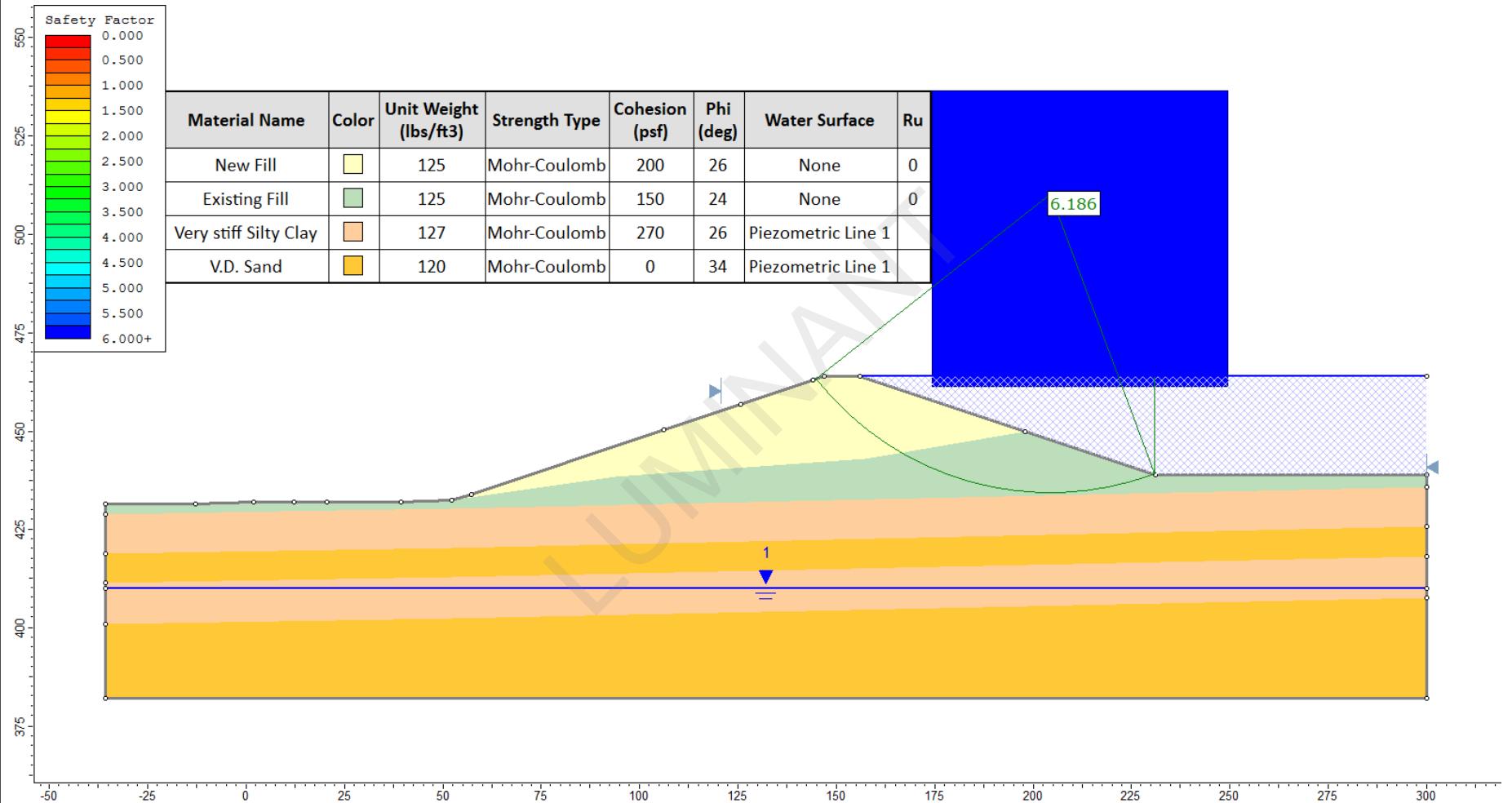


FIGURE C.27
Results of Stability Analysis – FGD-C: C–C' – Case 4a
 Stability and Safety Factor Assessment, Oak Grove SES

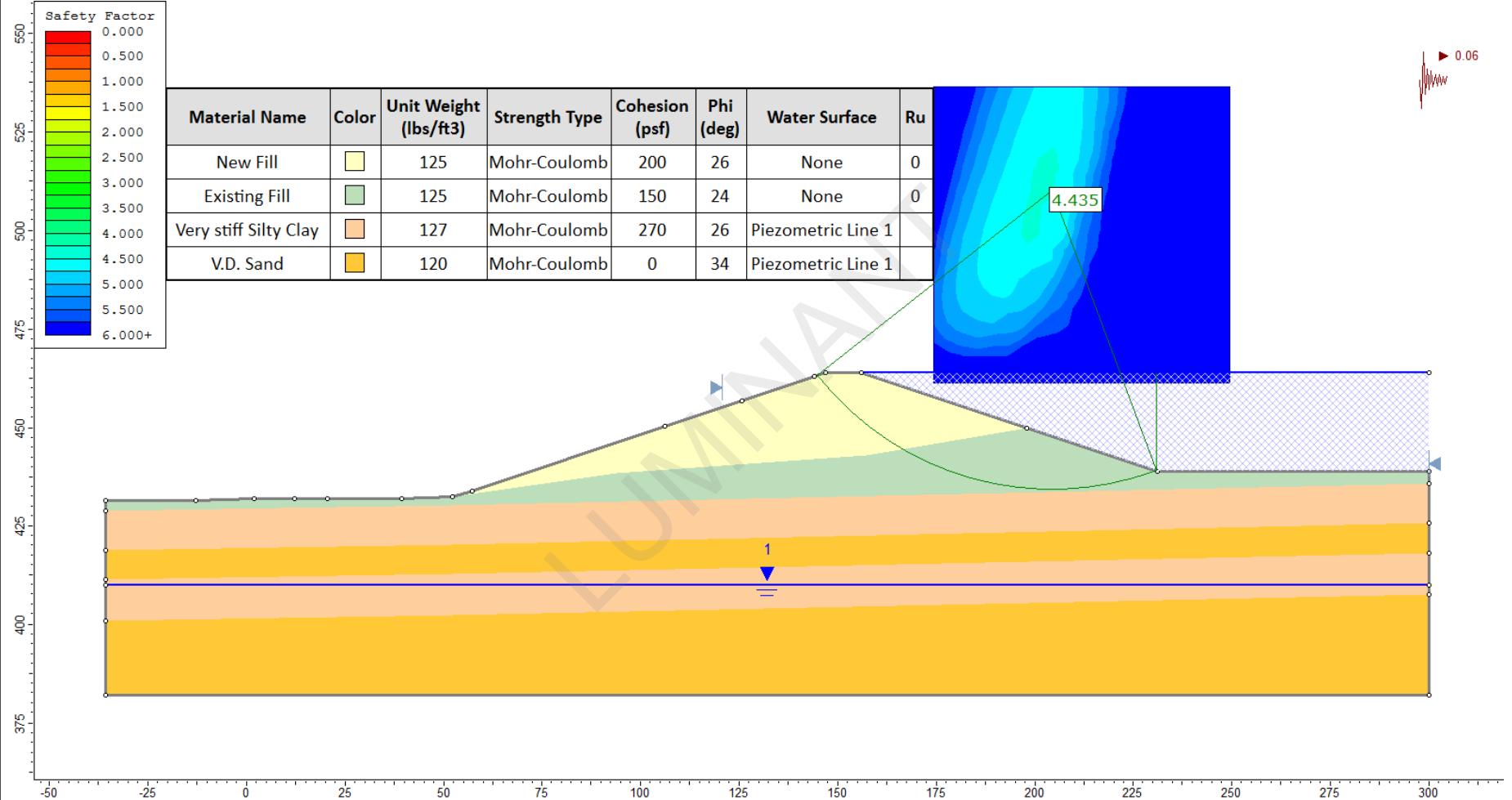


FIGURE C.28
Results of Stability Analysis – FGD-C: C-C' – Case 4b
 Stability and Safety Factor Assessment, Oak Grove SES

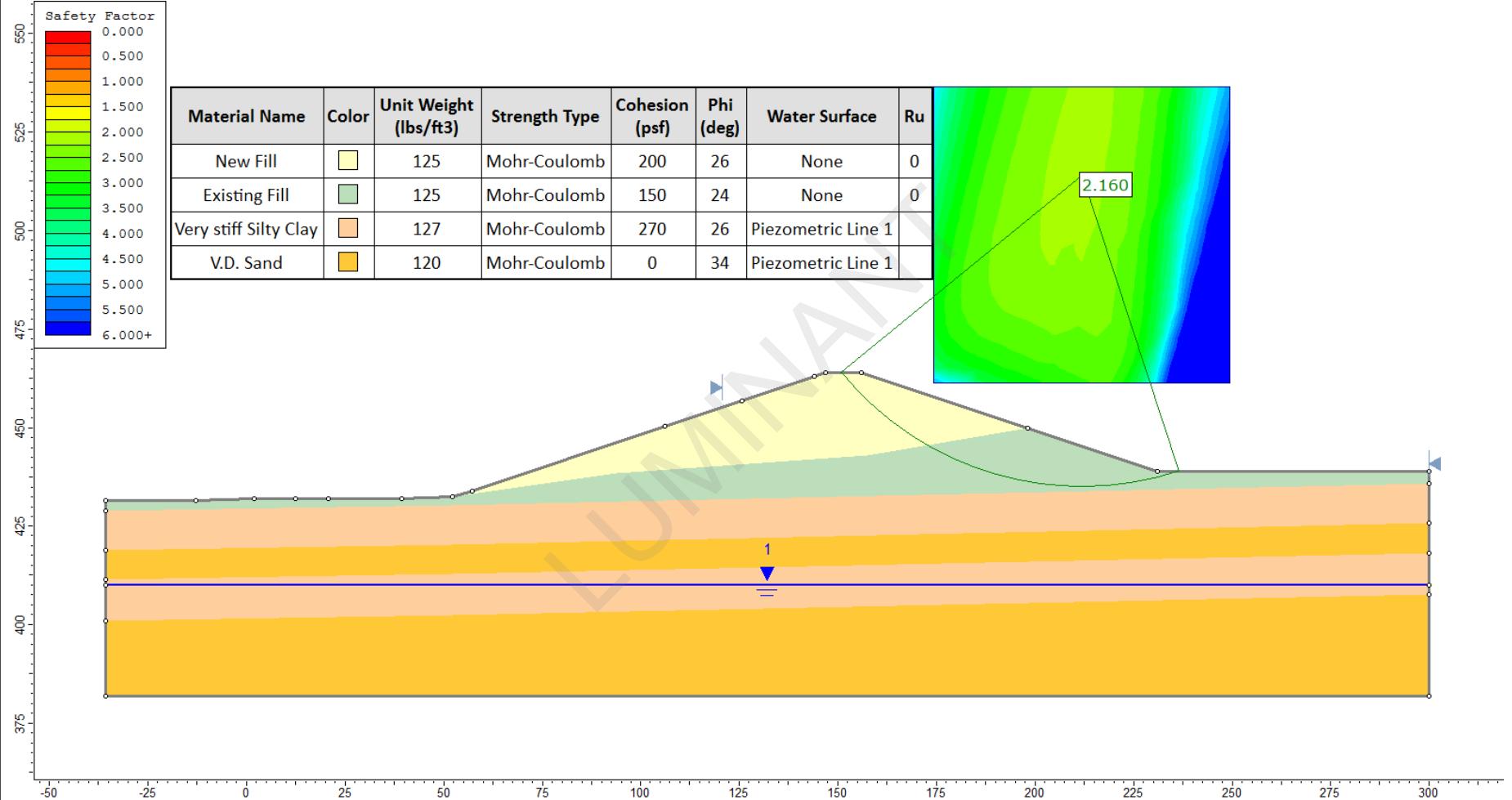


FIGURE C.29
Results of Stability Analysis – FGD-C: C–C' – Case 5a
 Stability and Safety Factor Assessment, Oak Grove SES

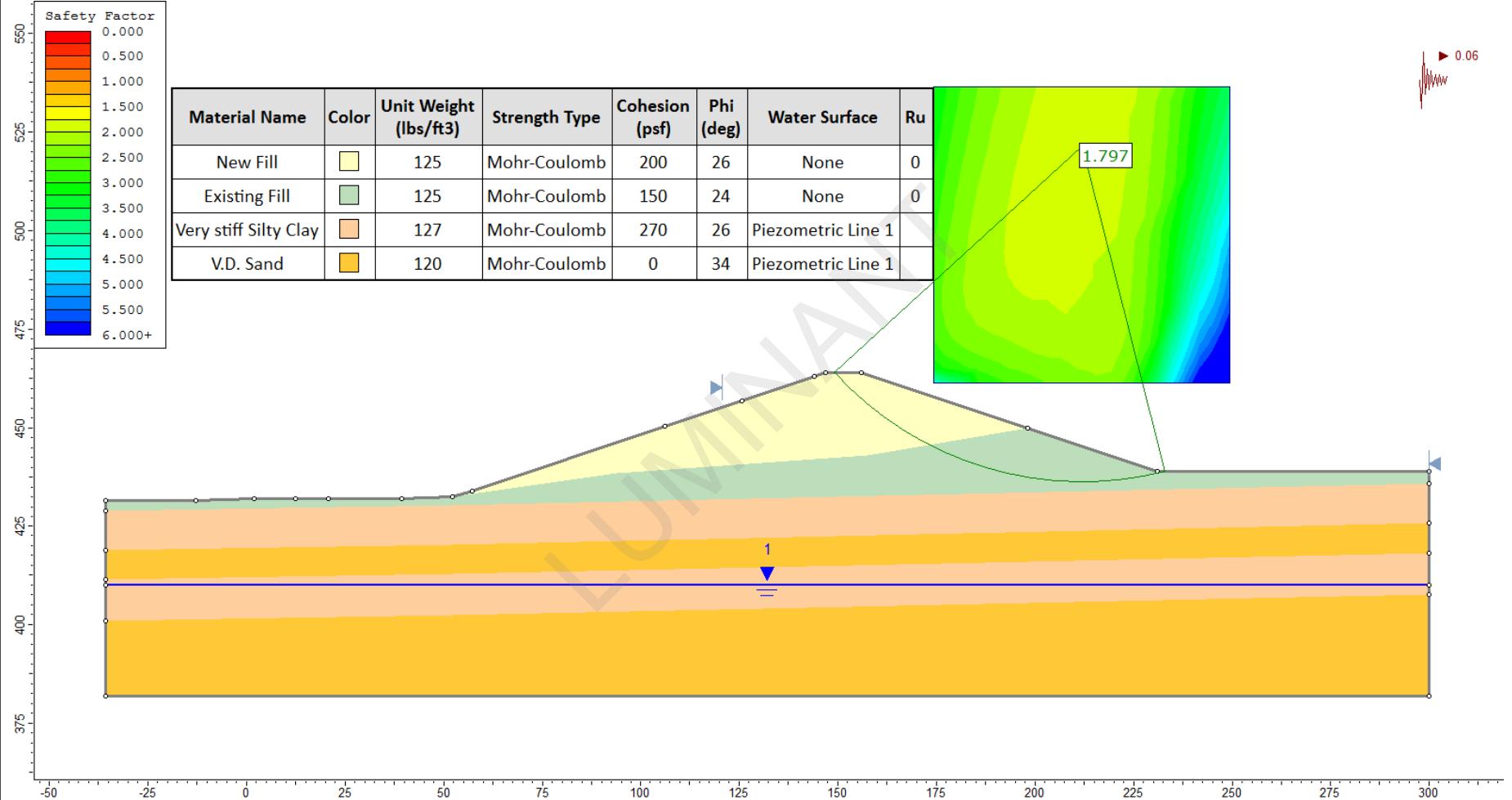


FIGURE C.30
Results of Stability Analysis – FGD-C: C–C' – Case 5b
 Stability and Safety Factor Assessment, Oak Grove SES

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